CCR RULE GROUNDWATER MONITORING CERTIFICATION

COAL ASH PONDS ELMER SMITH STATION DAVIESS COUNTY OWENSBORO, KENTUCKY

Prepared For:

OWENSBORO MUNICIPAL UTILITIES OWENSBORO, KENTUCKY



Prepared By:

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. PITTSBURGH, PENNSYLVANIA

CEC Project 164-014

OCTOBER 17, 2017 (AMENDED MARCH 2019)



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1.0 INTRODUCTION

1.1 PURPOSE

The United States Environmental Protection Agency (USEPA) issued 40 CFR §257, Subpart D, *Disposal of Coal Combustion Residuals from Electric Utilities* (CCR Rule) on April 17, 2015. The CCR Rule regulates disposal of CCR in new and active landfills and impoundments.

The CCR Rule states the following criteria for a groundwater monitoring system (GMS) (40 CFR §257.91):

- (a) *Performance standard*. The owner or operator of a CCR unit must install a GMS that consists of a sufficient number of wells, installed at appropriate locations and depths, to yield groundwater samples from the uppermost aquifer that:
 - (1) Accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit. A determination of background quality may include sampling of wells that are not hydraulically upgradient of the CCR management area where:
 - (i) Hydrogeologic conditions do not allow the owner or operator of the CCR unit to determine what wells are hydraulically upgradient; or
 - (ii) Sampling at other wells will provide an indication of background groundwater quality that is as representative or more representative than that provided by the upgradient wells; and
 - (2) Accurately represent the quality of groundwater passing the waste boundary of the CCR unit. The downgradient monitoring system must be installed at the waste boundary that ensures detection of groundwater contamination in the uppermost aquifer. All potential contaminants must be monitored.
- (b) The number, spacing, and depths of monitoring systems shall be determined based upon site-specific technical information that must include thorough characterization of:
 - (1) Aquifer thickness, groundwater flow rate, groundwater flow direction including seasonal and temporal fluctuations in groundwater flow; and
 - (2) Saturated and unsaturated geologic units and fill materials overlying the uppermost aquifer, materials comprising the uppermost aquifer, and materials comprising the confining unit defining the lower boundary of the uppermost aquifer, including, but not limited to, thicknesses, stratigraphy, lithology, hydraulic conductivities, porosities and effective porosities.

- (c) The GMS must include the minimum number of monitoring wells necessary to meet the performance standards specified in paragraph (a) of this section, based on the sitespecific information specified in paragraph (b) of this section. The GMS must contain:
 - (1) A minimum of one upgradient and three downgradient monitoring wells; and
 - (2) Additional monitoring wells as necessary to accurately represent the quality of background groundwater that has not been affected by leakage from the CCR unit and the quality of groundwater passing the waste boundary of the CCR unit.

The CCR Rule continues to outline well installation, development, sampling, and decommissioning requirements. The CCR Rule requires the owner or operator to obtain a certification from a qualified professional engineer stating that the GMS has been designed and constructed as outlined here. A record of the certification must be placed in the facility's operating record and the publicly accessible internet site and the state must be notified that the information is available.

Owensboro Municipal Utilities (OMU) installed a GMS at their CCR unit to comply with the CCR Rule. OMU retained Civil & Environmental Consultants (CEC) to assist with the design, installation and sampling of the GMS, and the preparation of this report. This report has been amended to provide documentation regarding installation of an additional GMS monitoring well (MW-8) in accordance with the requirements of the CCR Rule.

2.0 SITE OVERVIEW

2.1 BACKGROUND

The Ash Pond area associated with the Elmer Smith Station (ESS) is less than 10 acres in size and consists of three separate unlined ash settling basins (Ponds 1, 2, and 3). A site location map and a site and vicinity aerial map showing the location of the Ash Ponds are provided as Figures 1 and 2, respectively. The basins are not used for the disposal of CCR but for the temporary storage of CCR material prior to being excavated and transported off-site for disposal or beneficial re-use. Pond 1 is used for Unit 1 boiler slag; Pond 2 receives all other ash as well as water plant blowdown (lime softening sludge); and, Pond 3 receives no ash directly and is used for final settling prior to discharge. Other plant discharges, including coal pile runoff, Flue Gas Desulfurization (FGD) blowdown, roof and floor drains, etc. are also conveyed through the ponds. Based on a review of aerial images, contour data from the USGS National Map, Owensboro East Quadrangle, and a site map prepared by others labeled "Structural Fill Finish Grading" dated August 28, 1962¹, the Ash Ponds appear to be incised in the native soils to a depth of approximately 8 feet below ground surface (bgs). This was confirmed through knowledge of site personnel.

Permanent groundwater monitoring wells were not previously installed at the ESS Ash Pond area and no prior groundwater monitoring had been conducted prior to the GMS installation. To comply with the Federal CCR Rule (Section §257.91) published April 17, 2015, permanent groundwater monitoring wells were installed to meet the GMS performance standard.

2.2 HYDROGEOLOGIC SETTING

Subsurface conditions encountered at the site, as evidenced by the soil borings advanced in association with a preliminary Hydrogeologic investigation and the permanent GMS wells, are consistent with Quaternary-aged alluvium, and buried outwash (Tazewell age) typically found within the Ohio River Valley². Variable thicknesses of fine-grained silt and clay lenses are

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¹ Drawing No. S-7 "Structural Finish Grading", prepared by Black & Veatch, dated August 28, 1962.

interbedded with deposits of coarser-grained, poorly-graded sand beneath a thin veneer of topsoil, crushed stone fill, or other fill material. The near-surface fine-grained deposits are thicker near the Ohio River, and decrease in thickness away from the river towards the southeast, where sand becomes the predominant soil type. A low permeability clay layer was encountered at depths ranging from 26 to 43 feet bgs, varying in thickness from approximately 1 foot to over 16 feet, with an increasing trend in the thickness of this layer towards the south/southeast. The clay layer is underlain by saturated, coarse-grained deposits that constitute the uppermost aquifer at the site. Aquifer saturated thickness in the vicinity of the site ranges from approximately 60 to 100 feet². Based on the depth to groundwater and the depth of the Ash Ponds, it does not appear that groundwater is in direct communication with the Ash Ponds. Lithology encountered in the borings advanced for the monitoring wells that comprise the GMS is documented in the boring logs included in Appendix A.

2.2.1 Hydrogeologic Characteristics

Groundwater elevation data collected to date have ranged from 346.80 feet above mean sea level (amsl) at MW-7 to 370.29 feet amsl at MW-3. The normal pool elevation of the adjacent Ohio River in the vicinity of ESS is approximately 358 feet AMSL³. Potentiometric data are summarized on Table 1 and shown on Figure 3.

Groundwater elevation measurements indicate that the groundwater flow direction is to the southeast at an approximate average hydraulic gradient of 0.006. This flow direction is contrary what is typically observed in this type of hydrogeologic setting, where groundwater flow is towards the surface water body. The southeasterly flow direction is interpreted to be a result of the pumping influence from the 11 nearby water production wells (Figure 2) associated with municipal water production operations at OMU's Cavin Water Treatment Plant, which has a capacity of up to 10 million gallons per day. Between the Cavin Plant and Water Plant A, which is located west of the Cavin Plant and draws from the same well field, OMU's total withdrawal capacity is 28 million

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² Geohydrology and Simulation of Ground-Water Flow for the Ohio River Alluvial Aquifer near Owensboro, Northwestern Kentucky. U.S. Geological Survey Water-Resources Investigation Report 96-4274. 1997. Figure 7.

³Ohio River Navigation Charts from Cairo, Illinois to Foster, Kentucky (June 2010). U.S. Army Corps of Engineers, Louisville District. Chart No. 53.

gallons per day. Absent operation of the production wells, groundwater flow direction is likely to the northwest towards the Ohio River; however, some combination of pumping wells is always in operation and all of the observed groundwater levels measured since the installation of the GMS (Table 1) indicate a southeasterly groundwater flow direction.

Hydraulic conductivity of the uppermost aquifer was not evaluated as part of the GMS installation process; however, based on published scientific reports, the site is located in an area where horizontal hydraulic conductivity values are estimated to range from 126 to 157 feet per day⁴.

⁴Geohydrology and Simulation of Ground-Water Flow for the Ohio River Alluvial Aquifer near Owensboro, Northwestern Kentucky. U.S. Geological Survey Water-Resources Investigation Report 96-4274. 1997. Figure 11.

3.0 GROUNDWATER MONITORING SYSTEM

3.1 MONITORING WELL SELECTION

The GMS consists of eight monitoring wells. Monitoring wells MW-1 and MW-3 are used to monitor groundwater elevation, and monitoring wells MW-2, MW-4, MW-5, MW-6, MW-7, and MW-8 are utilized to monitor both groundwater elevation and quality. As noted above in Section 2.2.1, the well field pumping influence and proximity of the Ash Ponds to the Ohio River create a unique hydrogeologic setting where there is not an ideal location to establish background groundwater quality conditions (i.e., groundwater that does not have the potential to be affected by leakage from a CCR unit). Two monitoring wells (MW-2 and MW-7) will be used to establish and monitor background groundwater conditions.

While MW-2 is currently hydraulically upgradient, this is an artificial condition created by the operation of the production wells. Prior to the operation of the production wells (ca. 1998) this well was in a downgradient location. Also, should the production wells cease to operate in the future, groundwater flow direction would likely be reversed toward the river and MW-2 would be in a downgradient location. Because of this unique and artificial condition, the MW-7 location was also selected to accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit. MW-7, while located hydraulically downgradient from the ash ponds, is placed in a location so as not to be on a direct flow path from the ponds. MW-7 is also at a sufficient distance from the ponds to be representative of background conditions for the well field aquifer.

Downgradient monitoring wells MW-4, MW-5 and MW-6 will be used to monitor water quality of groundwater passing the waste boundary of the CCR unit. These wells were placed as close as possible to the waste boundary to provide for detection of groundwater contamination in the uppermost aquifer. Additionally, in the event that the well field should cease pumping operations for an extended period of time and the groundwater flow direction reverts back toward the river, monitoring wells MW-1 and MW-3 (currently used only for water level monitoring) can serve as future downgradient wells along with MW-2.

Monitoring well MW-8 was installed in December 2018 after one constituent (molybdenum) was quantified at a statistically significant level (SSL) in downgradient monitoring wells MW-5 and MW-6 in an effort to characterize the nature and extent of the release, as required by §257.95(g)(1).

A summary of the GMS wells is provided in the table below.

CCR RULE GROUNDWATER MONITORING SYSTEM

Location	Relative Location	Well Diameter (in.)	Total Depth (ft-bgs)	Screen Length (ft)
MW 1	Upgradient	4	57	10
MW-2	Upgradient (Background)	4	57	10
MW-3	Upgradient	4	57	10
MW-4	Downgradient	4	59	10
MW-5	Downgradient	4	59	10
MW-6	Downgradient	4	59	10
MW-7	Downgradient (Background)	4	72	10
MW-8	Downgradient	4	63	15

3.2 WELL CONSTRUCTION

The wells are completed in unconsolidated sand and gravel deposits associated with the Ohio River Valley alluvium and outwash complex. Each of the GMS wells was advanced using hollow-stem augers and constructed of 4-inch diameter schedule 40 polyvinyl chloride (PVC) casing with 10 to 15 feet of 0.010-inch slotted well screen and solid riser extended to a height of approximately 2.5 feet above the ground surface (reference Appendix A). Well screens were placed to monitor the uppermost aquifer. Each of the well screens was constructed using U-Pack® double-walled screens instead of traditional single-walled screens to assist with the collection of low turbidity groundwater samples. The U-Pack® screens were filled with sand filter media (silica sand) along the length of the screen prior to lowering it into the borehole to prevent installation of the filter sand through a turbid water column, which can entrain sediment in the filter pack. Global Drilling Suppliers, Inc. #7 filter sand was utilized within the U Pack® screens. As the augers were extracted at each monitoring well location, the annular space between the borehole and the U-Pack® well

screen was backfilled with Global Drilling Suppliers, Inc. #5 filter sand from the base of the screen to approximately 2 feet above the screen. Coated bentonite pellets were then placed in the annulus and hydrated with potable water to construct an approximate 5-foot thick seal above the filter pack. Bentonite grout was then placed via tremie pipe from the top of the seal to ground surface elevation. Each well is completed with a locking steel protective cover, concrete pad, and protective bollards. The Kentucky Attach Well Identification Number (AKGWA) Well Identification label is affixed to the underside of each protective cover lid. After construction, the wells were developed via a combination of surging, bailing and pumping techniques to clean the screens, reduce turbidity, and establish communication with the aquifer.

4.0 GROUNDWATER MONITORING CERTIFICATION

CCR Impoundment Information

Name:

Elmer Smith Station Ash Ponds Owensboro Municipal Utilities

Operator: Address:

4301 E 4th Street Owensboro, Kentucky 42303

Qualified Professional Engineer:

Name:

James E. Zentmeyer

Company:

Civil & Environmental Consultants

I, James E. Zentmeyer, certify that this Groundwater Monitoring System for the Elmer Smith Station Ash Ponds has been designed and constructed to meet the requirements of the Coal Combustion Residual (CCR) rule 40 CFR §257.91. I am a duly licensed Professional Engineer under the laws of Kentucky.

Print Name: __James E. Zentmeyer

Signature:

Date:

License Number: 18953

My license renewal date is: June 30, 2020



Qualified Professional Geologist:

Name:

Matthew G. Nemecek

Company:

Civil & Environmental Consultants

I, Matthew G. Nemecek, certify that this Groundwater Monitoring System for the Elmer Smith Station Ash Ponds has been designed and constructed to meet the requirements of the Coal Combustion Residual (CCR) rule 40 CFR §257.91. I am a duly licensed Professional Geologist under the laws of Kentucky.

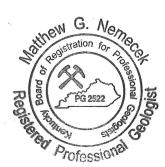
Print Name: Matthew G. Nemecek

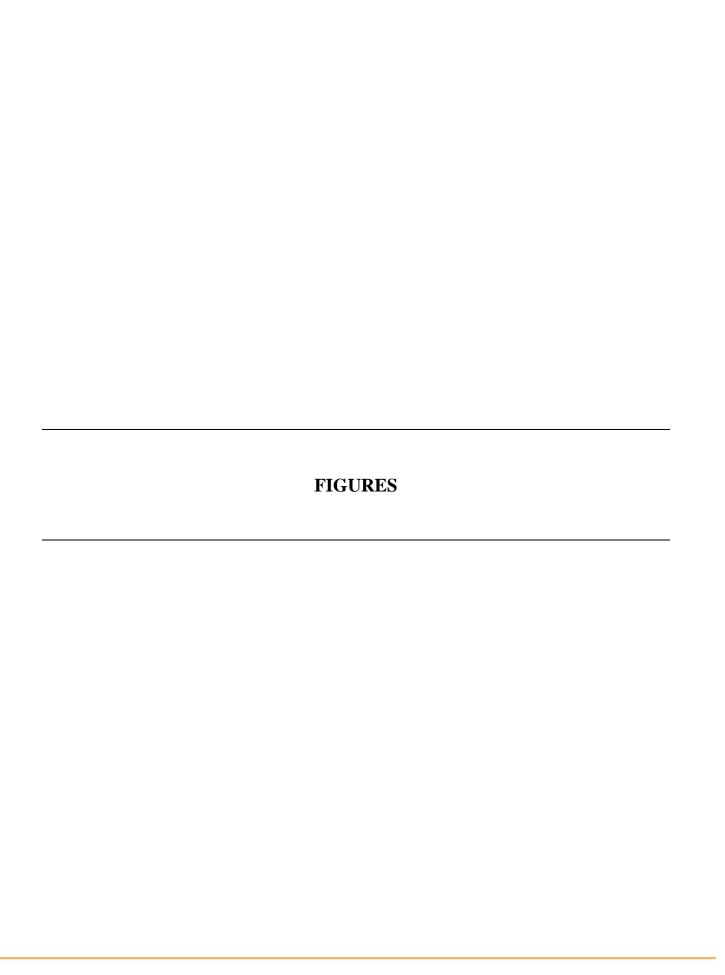
Signature: Matthew Change

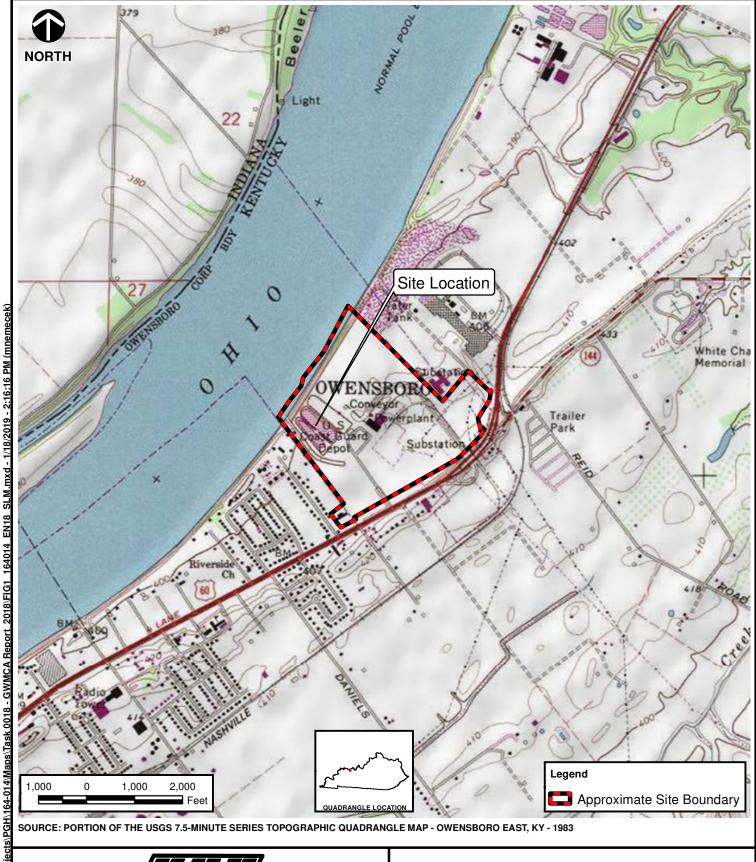
Date: March 29, 2019

License Number: KY-2522

My license renewal date is September: 30, 2019









Civil & Environmental Consultants, Inc.

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OWENSBORO MUNICIPAL UTILITIES ELMER SMITH STATION ASH PONDS OWENSBORO, DAVIESS COUNTY, KY

SITE LOCATION MAP

DRAWN BY: MGN CHECKED BY: HTW APPROVED BY: HTW* FIGURE NO:

DATE: JANUARY 18, 2019 DWG SCALE: 1 " = 2,000 ' PROJECT NO: 164-014.0018





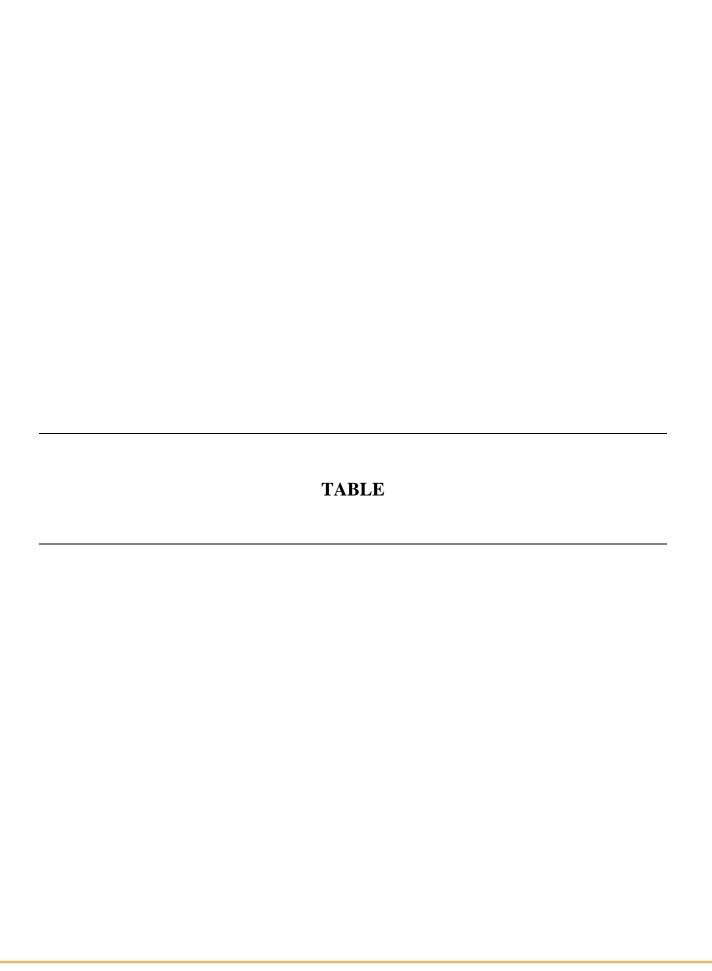


TABLE 1 Groundwater Elevation Summary OMU Elmer Smith Station Ash Ponds Owensboro, KY (all measurements are in feet)

Well ID (AKGWA#)	Location Relative to Ash Ponds	Ground Surface Elevation (AMSL)	TOC Elevation (AMSL)	Measurement Date	Depth to Water Measurement (ft BTOC)	Groundwater Elevation (AMSL)
				12/8/2016	48.51	356.02
				12/13/2016	48.07	356.46
				2/8/2017	45.69	358.84
				3/8/2017	40.68	363.85
				4/6/2017	43.51	361.02
				5/3/2017	45.91	358.62
		402.00		5/15/2017	43.46	361.07
				6/16/2017	49.94	354.59
NANY 1			404.53	6/29/2017 7/13/2017	46.72 49.81	357.81 354.72
MW-1 (8006-9522)	Upgradient			7/27/2017	49.81	354.72
(8000-7322)				8/9/2017	49.15	355.38
				8/23/2017	50.38	354.15
				9/6/2017	50.31	354.22
				9/20/2017	50.04	354.49
				10/10/2017	49.55	354.98
				4/5/2018	34.75	369.78
				6/5/2018	46.61	357.92
				12/12/2018	43.97	360.56
				12/27/2018	35.66	368.87
				12/8/2016	49.21	356.34
				12/13/2016	48.74	356.81
				2/8/2017	46.29	359.26
				3/8/2017	41.24	364.31
				4/6/2017	44.16	361.39
				5/3/2017	45.48	360.07
				5/15/2017	44.02	361.53
			405.55	6/16/2017	50.02	355.53
MW	TT 1' ,			6/29/2017	47.17	358.38
MW-2 (8006-9523)	Upgradient (Background)	402.75		7/13/2017 7/27/2017	50.16 50.23	355.39 355.32
(8000-9323)	(Dackground)			8/9/2017	50.75	354.80
				8/23/2017	50.97	354.58
				9/6/2017	50.95	354.60
				9/20/2017	50.69	354.86
				10/10/2017	50.20	355.35
				4/5/2018	35.70	369.85
				6/5/2018	47.22	358.33
				12/12/2018	44.51	361.04
				12/27/2018	36.85	368.70
	Upgradient			12/8/2016	49.88	356.51
				12/13/2016	49.43	356.96
				2/8/2017	46.95	359.44
				3/8/2017	41.64	364.75
				4/6/2017	44.56	361.83
				5/3/2017	45.90	360.49
				5/15/2017	44.51	361.88
				6/16/2017	50.06 47.29	356.33 359.10
MW-3				7/13/2017	50.64	355.75
(8006-9524)		403.78	406.39	7/27/2017	50.69	355.70
				8/9/2017	51.35	355.04
				8/23/2017	51.65	354.74
				9/6/2017	51.43	354.96
				9/20/2017	51.25	355.14
				10/10/2017	50.82	355.57
				4/5/2018	36.10	370.29
				6/5/2018	47.84	358.55
				12/12/2018	45.16	361.23
				12/27/2018	37.61	368.78

Notes: AMSL = Above Mean Sea Level

TOC = Top of Casing

Ft BTOC = Feet Below Top of Casing

TABLE 1

Groundwater Elevation Summary OMU Elmer Smith Station Ash Ponds Owensboro, KY

(all measurements are in feet)

Г				12/0/2017	51 11	252 50
				12/8/2016	54.44	353.58
				12/13/2016	54.06	353.96
				2/8/2017	51.22	356.80
				3/8/2017	52.97	355.05
				4/6/2017	54.99	353.03
				5/3/2017	55.75	352.27
				5/15/2017	53.95	354.07
		406.44		6/16/2017	58.65	349.37
				6/29/2017	57.60	350.42
MW-4	Daven and diant		409.02	7/13/2017	58.20	349.82
(8006-9525)	Downgradient		408.02	7/27/2017	58.73	349.29
				8/9/2017	58.97	349.05
				8/23/2017	59.48	348.54
				9/6/2017	58.73	349.29
				9/20/2017	57.75	350.27
				10/10/2017	57.15	350.87
				4/5/2018	48.85	359.17
			-	6/5/2018	51.97	
						356.05
				12/12/2018	50.92	357.10
				12/27/2018	48.87	359.15
				6/16/2017	56.37	349.79
				6/29/2017	56.66	349.50
				7/13/2017	56.62	349.54
				7/27/2017	57.03	349.13
				8/9/2017	57.05	349.11
				8/23/2017	57.45	348.71
MW-5	Downgradient	403.56	406.16	9/6/2017	57.11	349.05
(8005-9530)	8			9/20/2017	56.12	350.04
				10/10/2017	55.51	350.65
				4/5/2018	45.14	361.02
				6/5/2018	50.11	356.05
			-	12/12/2018	49.16	357.00
				12/27/2018	46.58	359.58
				6/16/2017	57.96	349.39
				6/29/2017	57.40	349.95
				7/13/2017	57.96	349.39
				7/27/2017	58.16	349.19
				8/9/2017	58.55	348.80
MW-6		405.23		8/23/2017	58.82	348.53
(8006-9531)	Downgradient		407.35	9/6/2017	58.65	348.70
(8000-9331)				9/20/2017	57.41	349.94
				10/10/2017	56.84	350.51
				4/5/2018	46.53	360.82
				6/5/2018	51.56	355.79
				12/12/2018	50.53	356.82
				12/27/2018	48.35	359.00
				6/16/2017	72.90	348.21
	Downgradient (Background)	418.26				
				6/29/2017	73.25	347.86
				7/13/2017	72.87	348.24
				7/27/2017	73.81	347.30
			421.11	8/9/2017	74.31	346.80
NASS C				8/23/2017	74.31	346.80
MW-7				9/6/2017	73.71	347.40
(8006-9532)				9/20/2017	73.79	347.32
				10/10/2017	73.70	347.41
						+
				4/5/2018	67.61	353.50
				6/5/2018	69.37	351.74
				12/12/2018	66.12	354.99
				12/27/2018	65.11	356.00
				12/2//2010	03.11	330.00
MW-8	Downgradient	402.97	405.82	12/27/2018	49.51	356.31

Notes: AMSL = Above Mean Sea Level

TOC = Top of Casing

Ft BTOC = Feet Below Top of Casing



WELL NUMBER MW-1 PAGE 1 OF 1 (mdd) WELL DIAGRAM 딢 Pro-Cover & Top Plug \<u>401.</u>7/ NA NA NA 4-inch PVC well casing NA 393.5 NA 391.5 NA 390.0 ■Benseal grout NA NA NA NA NA 380.3 NA NA 376.0 NA NA NA NA NA NA NA

333 Baldwin Road Pittsburgh, PA 15205 PROJECT NAME Elmer Smith Ash Pond **CLIENT** Owensboro Municipal Utilities CEC PROJECT NUMBER 164-014 PROJECT LOCATION Owensboro, Kentucky **COMPLETED** 12/5/16 GROUND ELEVATION 402.00 ft HOLE SIZE 12 inches DATE STARTED 12/5/16 DRILLING CONTRACTOR Richardville Drilling **GROUND WATER LEVELS:** DRILLING METHOD Hydraulic Push/6.25" HSA $\sqrt{2}$ AT TIME OF DRILLING 47.0 ft / Elev 355.0 ft LOGGED BY JEL CHECKED BY MGN AT END OF DRILLING _---▼ 72 hours AFTER DRILLING 46.0 ft / Elev 356.0 ft **LOCATION** N 3815477, E 4541324; AKGWA #8006-9522 SAMPLE TYPE NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) MATERIAL DESCRIPTION TOPSOIL, moist DF 0.3 / 95 Brown sandy SILT, medium stiff, moist DP 95 DP 100 3 100 DP 4 100 Olive gray silty SAND, moist DP 10 10.5 5 100 Olive gray SILT, medium stiff, moist 12.0 DP Light brown to reddish brown silty CLAY, some sand, medium stiff to very 6 90 DP stiff, moist 90 DP 100 8 DΡ 100 20 9 DP 90 10 Brown SAND, loose, moist DP 90 11 DP 75 $\frac{1}{26.5}$ 12 Brown silty CLAY, soft, very moist 75 DP Brown **SAND**, loose, poorly graded, moist, as above 13 70 30 DP 14 70 DP 15 80 DP 80 16 DP 100 17 DP 100 40 18 DP 70 NA 19 Hvdrated DP 70 bentonite seal NA 20 DP 75 NA Filter pack 21 75 NA DP .saturated, as above, becoming more well-graded 22 90 NA DP 0.010-slot 23 UPack PVC 90 NA DP well screen 75 NA DP 75 NA 25 DP 150 NA 57.0 345.0 Unslotted 26 Bottom of hole at 57.0 feet threaded end DP сар 27 DP 28 DP

Civil & Environmental Consultants, Inc.

GENERAL BH / TP / WELL 164-014 BORING LOGS.GPJ GOOD TEMPLATE.GDT 10/2/17

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GENERAL BH / TP / WELL 164-014 BORING LOGS.GPJ GOOD TEMPLATE.GDT 10/2/17

WELL NUMBER MW-3 Civil & Environmental Consultants, Inc. PAGE 1 OF 1 333 Baldwin Road Pittsburgh, PA 152050 PROJECT NAME Elmer Smith Ash Pond **CLIENT** Owensboro Municipal Utilities PROJECT LOCATION Owensboro, Kentucky CEC PROJECT NUMBER 164-014 **COMPLETED** 12/5/16 **GROUND ELEVATION** 403.77 ft HOLE SIZE 12 inches DATE STARTED 12/5/16 DRILLING CONTRACTOR Richardville Drilling **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING 47.0 ft / Elev 356.8 ft DRILLING METHOD Hydraulic Push/6.25" HSA LOGGED BY JEL **CHECKED BY** MGN AT END OF DRILLING _---**Y** 60 hours AFTER DRILLING 47.3 ft / Elev 356.5 ft **LOCATION** N 3815758, E 4541533; , AKGWA #8006-9524 SAMPLE TYPE NUMBER GRAPHIC LOG (mdd) RECOVERY DEPTH (ft) MATERIAL DESCRIPTION WELL DIAGRAM 딢 Pro-Cover & Top Plug 0.3 TOPSOIL, moist DF \403.5/ 75 NA 401.8 **GRAVEL** (FILL) DP 75 NA 399.8 4.0 Brown SILT, some sand, some gravel, medium stiff, moist DP 90 Brown to olive gray silty SAND, loose, moist NA 4-inch PVC well casing 3 90 NA DP 4 8.8 395.0 100 NA DP Olive gray to reddish brown clayey SILT, medium stiff, moist 10 5 100 NA DP 6 70 NA 390.0 DP Reddish brown SAND, loose, poorly graded, moist 70 NA DP 75 NA 8 DP 19.0 Reddish brown clayey SILT, medium stiff, moist NA 20 9 Brown SAND, loose, poorly graded, moist DP 70 NA 10 DP 70 NA 11 25.5 | | | 26.5 DP NA ■Benseal grout 12 Brown sandy SILT, soft, moist 70 NA DP Brown **SAND**, loose, poorly graded, moist, as above 13 70 NA 30 DP 14 70 NA DP 15 70 NA DP 70 NA 16 DP 70 NA 17 DP 70 NA 18 DP 70 NA 19 ■Hydrated DP 70 NA bentonite seal 20 DP 75 NA Filter pack 21 75 NA DP ...<u>saturated</u>, as above, becoming more well-graded 22 90 NA DP 0.010-slot 23 UPack PVC NA DP well screen 67 NA DP NA 25 DP 133 NA 57.0 346.8 Unslotted 26 Bottom of hole at 57.0 feet threaded end DP сар 27 DP 28 DP

GENERAL BH / TP / WELL 164-014 BORING LOGS.GPJ GOOD TEMPLATE.GDT 10/2/17

	Civ 333 Pitt	il & Environmental Consultants, Inc. 3 Baldwin Road sburgh, PA 15205	WI	ELLN	NUMBER MW-4 PAGE 1 OF 1
CLIENT Owe	ensboro Muni	cipal Utilities	PROJECT NAME Elmer Smith Ash Po	nd	
CEC PROJEC	T NUMBER		PROJECT LOCATION Owensboro, Ke	ntucky	
DATE START	ED 12/5/16	COMPLETED 12/7/16	GROUND ELEVATION 406.442 ft	HOLE S	SIZE 12 inches
DRILLING CO	NTRACTOR	Richardville Drilling	GROUND WATER LEVELS:		
DRILLING ME	THOD Hydr	aulic Push/6.25" HSA	$\sqrt{2}$ AT TIME OF DRILLING $\sqrt{49.0}$ ft /	Elev 357.	4 ft
LOGGED BY	JEL	CHECKED BY MGN			
LOCATION_	N 3815041, E	E 4542187; AKGWA #8006-9525	48 hours AFTER DRILLING 52.9	ft / Elev	353.6 ft
O DEPTH (ft) SAMPLE TYPE NUMBER	RECOVERY % GRAPHIC LOG	MATERIAI	L DESCRIPTION	PID (ppm)	WELL DIAGRAM Pro-Cover & Top Plug
DP	75	GRAVEL (FILL)	40	NA NA	
DP DP		Brown silty CLAY , some gravel, so		NIA	
2 DP	90	Brown sandy SILT grading to silty		NA	4-inch PVC
3 DP	90	8.0	39	_{3.4} NA	well casing
10 4 DP	100	Light brown SAND , some silt, poor	ly graded, loose, moist	NA	
	100			NA	
_ DP 6	10			NA	
- DP 7				NA	
DP 8				NA	-
20 DP	75			NA NA	-
- HDP	70			NA NA	-
- 10 DP	70			NA	- ■Benseal grout
- 11 DP	_			NA	
30 12 DP				NA	
13 DP	70			NA	
X 14	70			NA	
DP 15	1 70 114			NA	
DP 16	I / U 1 1 1 1	38.5	36	NA NA	
40 X DP		Brown to olive gray silty CLAY , so	me sand, moist	NA	
	1////	light brown, poorly graded sand Light gray, medium stiff, moist, a	seam as above	NA	
_ <u>18</u> _ DP				NA	Hydrated bentonite seal
- 19 DP	100			NA	
20 SS	_ 	reddish brown, sandy, medium s 49.0 ▽	tiff, moist, as above 35		▼ Filter pack
		Light brown SAND , poorly graded,			
- SS 22		▼		NA	
SS 23		_		NA	0.010-slot
- SS 24	1 57			NA	UPack PVC well screen
60 SS 25	100			NA	Unslotted
√ SS	100			NA	threaded end cap
<u>/ 26</u> SS		63.0	hole at 63.0 feet		_
27 SS 28 SS 29		BOILLOM OI	Hole at 03.0 leet		

BH / TP / WELL 164-014 BORING LOGS.GPJ GOOD TEMPLATE.GDT 10/2/17

GENERAL