### HYDROLOGIC AND HYDRAULICS CAPACITY REQUIREMENTS

### OWENSBORO MUNICIPAL UTILITIES ELMER SMITH STATION ASH POND OWENSBORO KENTUCKY

**Prepared for:** 

Owensboro Municipal Utilities Elmer Smith Station 4301 State Rt. 144 Owensboro, Kentucky 42303

**Prepared by:** 

Civil & Environmental Consultants, Inc. 333 Baldwin Road Pittsburgh, PA 15205

**CEC Project 164-014.0003** 

October 2016



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#### 1.0 PURPOSE

On behalf of Owensboro Municipal Utilities (OMU), Civil & Environmental Consultants, Inc. (CEC) has evaluated the Hydrologic and Hydraulic Capacity Requirements for the Ash Pond at the Elmer Smith Station in accordance with the United States Environmental Protection Agency (USEPA) Code of Federal Regulations, Title 40, Parts 257 and 261 Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule, dated April 17, 2015 (CCR Rule). This evaluation specifically addresses the requirements in Section 257.82 (§257.82) – Hydrologic and Hydraulic Capacity Requirements for CCR Surface Impoundments. The Ash Pond at the Elmer Smith Station is classified as an existing CCR surface impoundment by definition in §257.53.

#### 2.0 SITE DESCRIPTION

OMU owns and operates the Elmer Smith Station (Station), which is located in Owensboro, Kentucky. The Station is a coal-burning facility that consists of two units with a combined capacity of 433 MW. The two units of the Station have been in operation since 1964 and 1974. The Ash Pond is located to the northwest of the Station. The Ash Pond is less than 10 acres in size and consists of three separate unlined ash settling basins (Ponds 1, 2, and 3). The Ash Pond receives flow from the Station and runoff from areas surrounding the Station. The Ash Pond is continuously dredged. The dredged materials are allowed to dewater from the piles and drain back into the ponds. The materials are either sold for beneficial use or transported to offsite disposal.

The location of the Station and the Ash Pond is shown on Figure 1 -Site Location Map. The existing conditions are shown on Figure 2 -Existing Conditions.

#### 3.0 §257.82(a) INFLOW DESIGN FLOOD

The applicable sections of §257.82(a) are reprinted below in bold, italic font. The responses follow each section of the rule and are provided in normal font.

(a) The owner or operator of an existing or new CCR surface impoundment or any lateral expansion of a CCR surface impoundment must design, construct, operate, and maintain an inflow design flood control system as specified in paragraphs (a)(1) and (2) of this section.

(a)(1) The inflow design flood control system must adequately manage flow into the CCR unit during and following the peak discharge of the inflow design flood specified in paragraph (a)(3) of this section.

(a)(2) The inflow design flood control system must adequately manage flow from the CCR unit to collect and control the peak discharge resulting from the inflow design flood specified in paragraph (a)(3) of this section.

(a)(3) The inflow design flood is:

(a)(3)(i) For a high hazard potential CCR surface impoundment, as determined under § 257.73(a)(2) or § 257.74(a)(2), the probable maximum flood;
(a)(3)(ii) For a significant hazard potential CCR surface impoundment, as determined under §257.73(a)(2) or §257.74(a)(2), the 1,000-year flood;
(a)(3)(iii) For a low hazard potential CCR surface impoundment, as determined under §257.73(a)(2) or §257.74(a)(2), the 100-year flood;
(a)(3)(iv) For an incised CCR surface impoundment, the 25-year flood.

The Ash Pond hazard classification was evaluated in accordance with §257.73 using the definitions in §257.53. §257.53 defines an incised CCR surface impoundment as a CCR surface impoundment that is constructed by excavating entirely below the adjacent natural ground surface, and does not consist of any constructed diked portion. Based on a review of aerial images, contour data from the USGS National Map, Owensboro East Quadrangle, and a site map prepared by Black & Veatch labeled "Structural Fill Finish Grading" dated 8-28-62, the Ash

Pond appears to be incised. This was confirmed through knowledge of site personnel. Since the Ash Pond is incised, the inflow design flood is the 25-year flood (25-year, 24-hour storm event).

#### 4.0 §257.82(b) SURFACE WATER REQUIREMENTS

§257.82(b) is reprinted below in bold, italic font. The responses follow in normal font.

#### §257.82(b) states:

# (b) Discharge from the CCR unit must be handled in accordance with the surface water requirements under §257.3-3.

In accordance with §257.3-3, discharges from the Site are authorized by and in compliance with Kentucky Pollutant Discharge Elimination System (KPDES) Permit No. KY001295. Dredged material or fill material is not discharged from the Site to waters of the United States in violation of the requirements under Section 404 of the Clean Water Act. Site operations have not caused non-point source pollution to waters of the United States in violation of the requirements under Section 208 of the Clean Water Act.

#### 5.0 §257.82(c) INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

The applicable sections of §257.82(c) are reprinted below in bold, italic font. The responses follow each section of the rule and are provided in normal font.

*§257.82(c) states:* 

#### (c) Inflow design flood control system plan

(c)(1) Content of the plan. The owner or operator must prepare initial and periodic inflow design flood control system plans for the CCR unit according to the timeframes specified in paragraphs (c)(3) and (4) of this section. These plans must document how the inflow design

flood control system has been designed and constructed to meet the requirements of this section. Each plan must be supported by appropriate engineering calculations. The owner or operator of the CCR unit has completed the inflow design flood control system plan when the plan has been placed in the facility's operating record as required by § 257.105(g)(4).

This Initial Inflow Design Flood Control System Plan evaluates the Ash Pond based on the requirements of this section. The Ash Pond receives flow from the Station and runoff from areas surrounding the Station. Pond 1 receives boiler slag sluice and FGD blowdown. Pond 2 receives sluiced fly ash and discharge from the Cavin Water Plant Sludge Lagoon (Cavin Sludge Lagoon). Pond 3 receives no direct flow from the Station and is used for final settling prior to discharge. Other Station discharges are routed through the Ash Pond, including discharge from roof drains and floor drains, etc. Runoff from various other ponds at the site is routed through the Ash Pond. Additionally, the Ash Pond receives runoff directly from adjacent areas. Pond 3 discharges into a canal to the south of the site, which discharges to the Ohio River through an outlet permitted under KPDES Permit No. KY001295.

The Hydrologic and Hydraulic Capacity Calculation presented in Appendix A considers the inflow to the Ponds 1, 2, and 3 of the Ash Pond, and evaluates the capacity of the Ash Pond. The calculation considers inflow from the 25-year, 24-hour storm event as required for an incised impoundment. Additionally, the calculation considers the flow from the Station to the Ash Pond. HydroCAD was used to route inflow from runoff during the 25-year, 24-hour storm event and flow from the Station through the Ash Pond.

Two scenarios were modeled for Pond 1 because limited information was available for the North Pond and the Coal Pile Runoff Ponds, which attenuate flow prior to discharge into Pond 1. The required pond capacity above the pool is based on the conservative model for Pond 1. CEC recommends maintaining the following capacities above the normal pool elevation.

Estimated Required Capacity above Pool					
Pond	Capacity (Ac-feet)				
Pond 1	9.3				
Pond 2	4.5				
Pond 3	7.8				

Alternately, a total capacity of 21.6 acre-feet can be maintained above all three ponds, since the ponds are interconnected. A table showing the approximate areas and depths above the pool that are needed to maintain these capacities is presented in Attachment 7 of Appendix A. CEC is basing the above requirements on a conservative assumption regarding the flow to Pond 1. CEC notes that incorporating more information about the North Ponds and the Coal Runoff Ponds into the model could reduce the required capacity above the pool elevation.

(c)(2) Amendment of the plan. The owner or operator of the CCR unit may amend the written inflow design flood control system plan at any time provided the revised plan is placed in the facility's operating record as required by § 257.105(g)(4). The owner or operator must amend the written inflow design flood control system plan whenever there is a change in conditions that would substantially affect the written plan in effect.

OMU will amend the Inflow Design Flood Control System Plan as needed and place it in the operating record.

(c)(3) Timeframes for preparing the initial plan-(i) Existing CCR surface impoundments. The owner or operator of the CCR unit must prepare the initial inflow design flood control system plan no later than October 17, 2016.

The Inflow Design Flood Control System Plan will be placed in the operating record no later than October 17, 2016.

(c)(4) Frequency for revising the plan. The owner or operator must prepare periodic inflow design flood control system plans required by paragraph (c)(1) of this section every five years. The date of completing the initial plan is the basis for establishing the deadline to complete the first periodic plan. The owner or operator may complete any required plan prior to the

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required deadline provided the owner or operator places the completed plan into the facility's operating record within a reasonable amount of time. In all cases, the deadline for completing a subsequent plan is based on the date of completing the previous plan. For purposes of this paragraph (c)(4), the owner or operator has completed an inflow design flood control system plan when the plan has been placed in the facility's operating record as required by 257.105(g)(4).

Periodic Inflow Design Flood Control System Plans will be prepared and added to the operating record by this date every five years. The Periodic Inflow Design Flood Control System Plan will be considered complete once placed in the operating record within a reasonable amount of time.

(c)(5) The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic inflow design flood control system plans meet the requirements of this section.

The certification statement provided by a qualified professional engineer states that this Initial Inflow Design Flood Control System Plan meets the requirements stated in §257.82(c).

#### 6.0 CONCLUSIONS

For this plan, a hydraulic and hydrologic capacity calculation was performed. The calculation considers the inflow to the Ponds 1, 2, and 3 of the Ash Pond, and evaluates the capacity of the Ash Pond. The calculation considers inflow from the 25-year flood (25-year, 24-hour storm event) as required for an incised impoundment. Additionally, the calculation considers the flow from the Station to the Ash Pond. Based on the calculations, CEC recommends maintaining the following capacities above the pool of the ponds.

Estimated Required Capacity above Pool						
Pond	Capacity (Ac-feet)					
Pond 1	9.3					
Pond 2	4.5					
Pond 3	7.8					

Alternately, a total capacity of 21.6 acre-feet can be maintained above all three ponds, since the ponds are interconnected. CEC is basing the above requirements on a conservative assumption about the flow to Pond 1. Incorporating more information about the North Ponds and the Coal Runoff Ponds into the model could reduce the required capacity above the pools.

#### 7.0 CERTIFICATION

I, Rick J. Buffalini, P.E., a registered professional engineer certify that Elmer Smith Station Ash Pond fulfils the Initial Inflow Design Flood Control System Plan requirements of §257.82(c). This certification is based on my review of the Initial Inflow Design Flood Control System Plan. This Initial Inflow Design Flood Control System Plan will be placed in the operating record by October 17, 2016.

Rick J. Buffalini, P.E. Printed Name of Professional Engineer

Signature

<u>041196-E</u> Registration No.

/0-17-16 Date

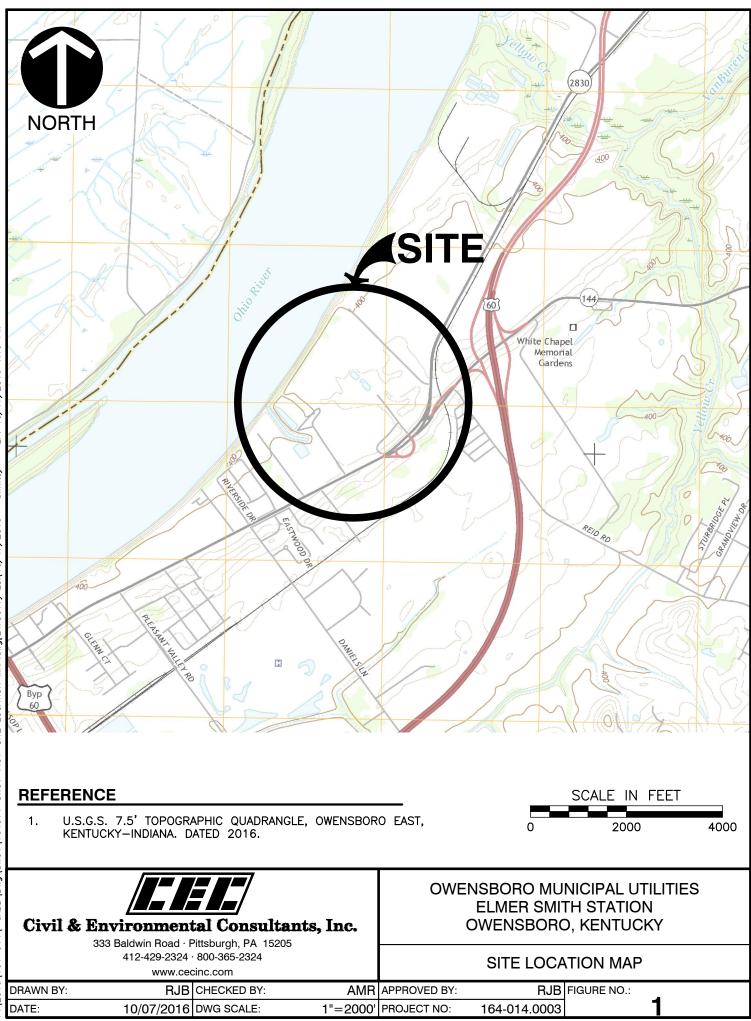
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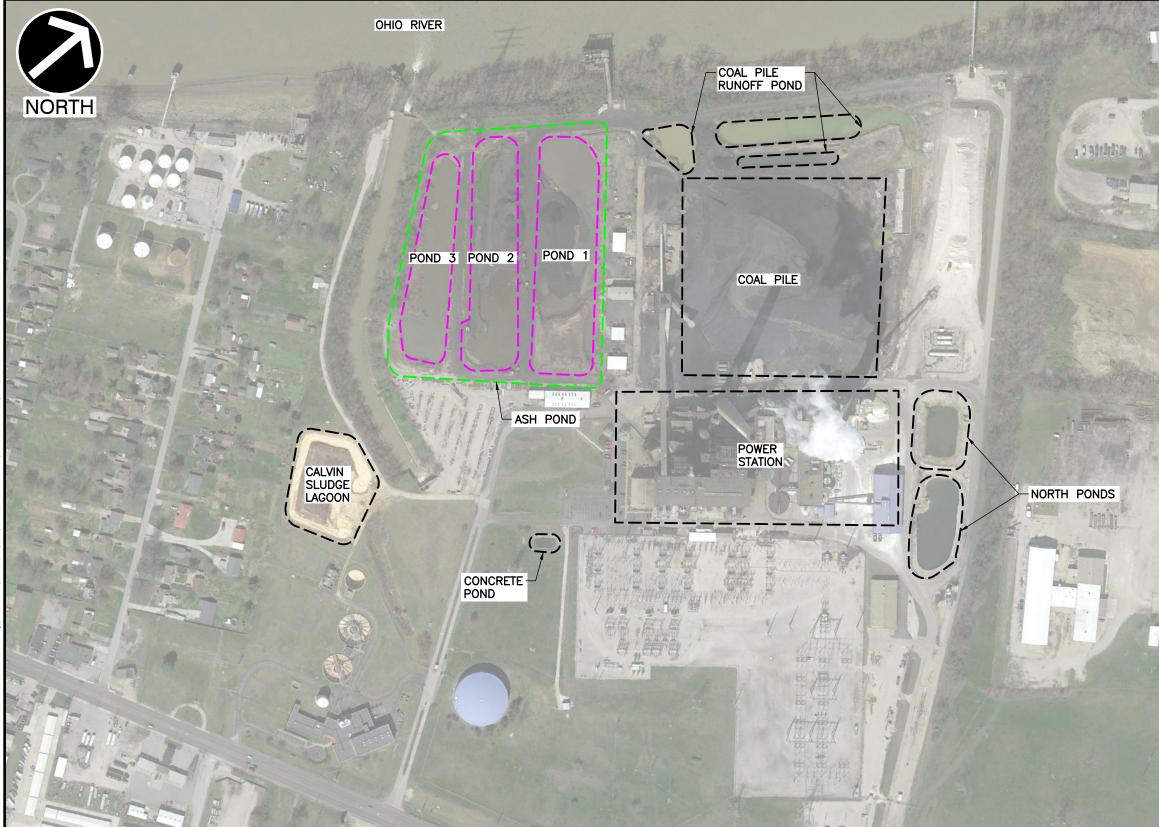


#### 8.0 **REFERENCES**

- 1. United States Department of Agriculture. Natural Resources Conservation Service. Web Soil Survey. <u>http://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm</u>
- 2. National Oceanic and Atmospheric Administration (NOAA), National Weather Service, Hydrometeorological Design Studies Center, Precipitation Frequency Data Server (PFDS). <u>http://hdsc.nws.noaa.gov/hdsc/pfds/</u>
- 3. 10-foot contour data provided by USGS National Map from the National Elevation Dataset (NED), Owensboro East Quadrangle, Publication Date 05/27/2016
- 4. Site Map labeled prepared by Black & Veatch labeled "Structural Fill Finish Grading" dated 8-28-62.

FIGURES







#### REFERENCE

1. AERIAL PHOTOGRAPHY COPYRIGHT GOOGLE EARTH PRO VERSION 6.2, IMAGERY DATE 3-25-2016.

	LEGEND
	ASH POND LIMITS APPROXIMATE FOOTPRINT 
	OTHER SITE FEATURES
	NOTES
	<ol> <li>THE APPROXIMATE FOOTPRINT OF PONDS 1, 2, AND 3 IS BASED ON DRAWING NO. S-7 " STRUCTURAL FILL FINISH GRADING" PREPARED BY BLACK AND VEACH, DATED 8-28-62 AND THE AERIAL PHOTOGRAPHY (SEE REFERENCE 1).</li> </ol>
-	SCALE IN FEET
•	OWENSBORO MUNICIPAL UTILITIES ELMER SMITH STATION OWENSBORO, KENTUCKY
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RJB FIGURE NO .:

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### **APPENDIX A**

# HYDROLOGIC AND HYDRAULIC CAPACITY CALCULATIONS



Civil & Environmental Consultants, Inc.									
PROJECT Owensboro Municipal Utilities					PROJEC	CT NO.	164-014.0003		
	Elmer Smith St	PAGE	1	OF	11				
Hydrologic and Hydraulic Capacity Calculation									
MADE BY	AMR	DATE	10/14/2016	CHECKED BY	AAW	DATE	10/14/20	16	

#### **OBJECTIVE:**

This calculation is being performed to evaluate the Hydrologic and Hydraulic Capacity of the Ash Pond at the Elmer Smith Station in accordance with CCR Rule §257.82. The Ash Pond at the Elmer Smith Station is classified as an existing CCR surface impoundment by definition in §257.53.

#### METHOD:

Use HydroCAD 10.0 to route the design storm through the Ash Pond.

#### **REFERENCES:**

- 1. HydroCAD Stormwater Modeling 10.0, HydroCAD Software Solutions, LLC., 2015.
- 2. United States Department of Agriculture. Natural Resources Conservation Service. Web Soil Survey. <u>http://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm</u>
- 3. National Oceanic and Atmospheric Administration (NOAA), National Weather Service, Hydrometeorological Design Studies Center, Precipitation Frequency Data Server (PFDS). http://hdsc.nws.noaa.gov/hdsc/pfds/
- 4. 10-foot contour data provided by USGS National Map from the National Elevation Dataset (NED), Owensboro East Quadrangle, Publication Date 05/27/2016
- 5. Site Map labeled prepared by Black & Veatch labeled "Structural Fill Finish Grading" dated 8-28-62.

#### **DESCRIPTION:**

The Ash Pond at the Elmer Smith Station (Station) receives flow from the Station and runoff from areas surrounding the Station. The Ash Pond is less than 10 acres in size and consists of three separate unlined ash settling basins (Ponds 1, 2, and 3). Pond 1 receives boiler slag sluice and FGD blowdown. Pond 2 receives fly ash sluice and discharge from the Cavin Water Plant Sludge Lagoon (Cavin Sludge Lagoon). Pond 3 receives no direct flow from the Station and is used for final settling prior to discharge. Other Station discharges are routed through the Ash Pond, including discharge from roof drains and floor drains, etc. Runoff from various ponds at the site is routed through the Ash Pond. Additionally, the Ash Pond receives runoff directly from adjacent areas. Pond 3 discharges into a canal to the south of the site, which discharges to the Ohio River through an outlet permitted under Kentucky Pollutant Discharge Elimination System (KPDES) Permit No. KY001295. Figure 1 shows the approximate location of the Station and Ash Pond and Figure 2 show the existing conditions.



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This calculation is being performed to evaluate the Hydrologic and Hydraulic Capacity of the Ash Pond at the Elmer Smith Station. Flow from the Station and runoff are considered in this evaluation.

#### ANALYSIS:

#### HYDROLOGIC EVALUATION

CCR Rule §257.82 bases the design flood (storm event) on the hazard potential of the CCR surface impoundment. Based on a review of aerial images, contour data from the USGS National Map, Owensboro East Quadrangle, and a site map prepared by Black & Veatch labeled "Structural Fill Finish Grading" dated 8-28-62, the Ash Pond appears to be incised. This was confirmed through knowledge of site personnel. Since the Ash Pond is incised, the inflow design flood is the 25-year flood (25-year, 24-hour design storm event). HydroCAD uses the 2-year, 24-hour storm event when calculating the time of concentration. The rainfall from the 2-year, 24-hour storm event and the 25-year, 24-hour storm event is presented below in inches:

Table 1 – Storm Information						
Storm Event	24-Hour Rainfall					
	(inches)					
2-YEAR	3.26					
25-YEAR	5.67					

The rainfall values for the storm events were determined by referencing the National Oceanic and Atmospheric Administration's (NOAA) Precipitation Frequency Estimates for Owensboro, Kentucky. The NOAA data is presented in Attachment 1. The Type II Storm event was modeled, which represents the most intense short duration rainfall in most regions of the United States.

#### Runoff:

HydroCAD was used to model the runoff and route the flow through the system of ponds. The rate of runoff is based on the relationships between the amount of rainfall, soil type, infiltration, land cover, travel time, and the size of the drainage area. The land cover over the site varies, and includes areas with poor grass cover, unpaved parking areas with no aggregate cover, unpaved roadways with no aggregate cover, soil stockpile areas, coal stockpile areas, paved parking areas, rooftops, and the pond surface. The Soil Conservation Service (SCS) Technical Release No. 20 (TR20) segmental approach methodology within HydroCAD was used to calculate the time of concentration and peak discharge in each drainage area.

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The times of concentration were estimated as the sum of sheet flow, shallow concentrated flow, and culverted flow. The times of concentration depend on the surface. Sheet flow calculations use a roughness of 0.15 for short grass, a roughness of 0.011 for smooth dirt surfaces, a roughness of 0.050 for rough dirt surfaces (fallow). The pipe calculations use a roughness of 0.010 for plastic pipe, a roughness of 0.025 for steel pipe (assumed corrugated metal), and a roughness of 0.012 for concrete pipe. Shallow flow calculations use a velocity factor of 16.1 ft/sec for unpaved surfaces.

The curve number was determined based on the hydrologic soil group for soils at the site and the land cover. The hydrologic soil group for the soils at the site was determined by referencing the United States Department of Agriculture – Natural Resources Conservation Service (USDA NRCS) soil survey map. The local soils at the site are generally classified in soils group B. The output from the USDA NRCS soil survey map is provided in Attachment 2. The following table summarizes the curve numbers used for each of the different land covers.

Table 2 – CN Data						
Land Cover	CN					
Poor Grass Cover	79					
Unpaved Parking Areas (dirt)	82					
Unpaved Roadways (dirt)	82					
Soil Stockpile Areas (bare soil)	86					
Coal Stockpile Areas (bare soil)	86					
Paved Parking Areas	98					
Rooftops	98					
Pond Surface	98					

The drainage areas to the Ash Pond were delineated and entered into HydroCAD. A table with the drainage areas is below:

Table 3 – Drainage Areas							
Drainage	Drainage	<b>Description/Assumptions</b>	Curve				
Area ID	Area (acres)		Number				
DA-1	1.93	Unpaved roadway, pond surface	82, 98				
DA-2	1.17	Unpaved roadway, pond surface	82, 98				
DA-3	2.55	Soil stockpile area	86				
DA-4 9.25		Coal stockpile, soil stockpile	86, 82,				
		Unpaved roadway, rooftops	98				
DA-5	4.71	Coal stockpile, pond surface	86, 98				
DA-6 2.39		Coal stockpile, pond surface	86, 98				
DA-7	19.59	Coal stockpile, ash pond surface,	86, 82,				



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		unpaved parking, rooftops and paved parking	98
DA-8	6.22	Pond surface, rooftops, poor grass, unpaved parking	98,79, 82
DA-9	5.14	Pond surface, unpaved parking	98, 82
Cavin Sludge Lagoon Area	1.59	Bare soil, pond surface	86, 98
Concrete Pond Area	0.10	Pond surface	98

Runoff from drainage areas DA-1 and DA-2 is drained to ponds labeled the North Ponds. Runoff from stockpile drainage areas DA-3 and DA-4 is drained to open channels. Runoff from the coal stockpile drainage areas DA-5 and DA-6 is drained to ponds labeled the Coal Pile Runoff Ponds. Discharge from the North Ponds is routed through the open channels to the Coal Pile Runoff Ponds. Discharge from the Coal Pile Runoff Ponds is routed into Pond 3.

Runoff from drainage area DA-7 is assumed to drain directly to Pond 1. Runoff from drainage area DA-8 is assumed to drain directly to Pond 2. Additionally, runoff and flow from the Cavin Sludge Lagoon area and the Concrete Pond area are assumed to drain directly to Pond 2.

Runoff from drainage area DA-9 is assumed to drain directly to Pond 3. Additionally, discharge from Pond 1 and Pond 2 is routed through Pond 3. A figure showing the drainage areas and a schematic of a drainage diagram is presented in Figure 3.

#### Flow from Station:

As discussed above, in addition to runoff, the Ash Pond receives flow from the Station. CCR is sluiced from the Station to the Ash Pond. Pond 1 receives boiler slag sluice, FGD blowdown, and flow from the coal pile runoff ponds. Pond 2 receives fly ash sluice and discharge from the Cavin Water Plant Lagoon. Pond 3 receives no direct flow from the Station and is used for final settling prior to discharge. Personnel at the site provided the approximate flows from the Station to Ponds 1 and 2. Below is a summary of the flow rates from the Station to the Ash Pond:



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Table 4 – Pond 1 Flow Data						
Flow Description	Flow (GPD)	Flow (cfs)				
Boiler Slag Sluice	250,000	0.39				
FGD Blowdown	66,400	0.10				
Coal Pile Runoff	55,000	0.085				
Total:	371,400	0.58				

The flow into Pond 1 is approximately 371,400 gallons per day (GPD) or 0.58 cfs based on these flows provided from personnel at the Station.

Table 5 – Pond 2 Flow Data						
Flow Description	Flow (GPD)	Flow (cfs)				
Fly Ash Sluice	375,000	0.58				
Cavin Water Plant Lagoon Sludge	40,000	0.062				
Discharge						
Total:	415,000	0.64				

The flow into Pond 2 is approximately 415,000 gallons per day (GPD) or 0.64 cubic feet per second (cfs) based on these flows provided from personnel at the Station. Correspondence with site personnel regarding the flow is provided in Attachment 3.

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#### HYDRAULIC EVALUATION

#### Preliminary Evaluation:

A preliminary evaluation of the Ash Pond was performed to compare the pond capacity with the inflow from runoff and flow from the Station. For this evaluation, the Ash Pond capacity was obtained from Drawing No. S-7 labeled "Structural Finish Grading", which was prepared by Black & Veatch and is dated 8-28-62. This drawing shows contours for Ponds 1, 2, and 3. This drawing shows the maximum footprint of the ponds, and the maximum available pond capacity. The drawing is presented on a site specific coordinate and elevation system, indicated by a reference arrow and a true north area. Based on the drawing, the crest of the ponds are at elevation 95-feet and the bottom of the ponds are at elevation 87-feet, which provides approximately 8-feet of total storage depth. Based on current information from the site, the normal pool of the pond is approximately 6-feet below the pond crest, or at approximate elevation 89-feet. Since the pool elevations are assumed to be at elevation 89-feet, the inlet of the discharge structures in Ponds 1 and 2 were assumed to be at elevation 89-feet, and the inlet of the discharge structure in Pond 3 was assumed to be at elevation 88-feet. It was assumed that the pond capacity above the pool and above the inlet of the discharge structure is available for routing inflow. The contours as presented in the "Structural Finish Grading" drawing were used to obtain stage storage curves to calculate the available pond volume above the pool. The drawing with the contours used for the evaluation is presented in Attachment 4 with the stage storage curves for the ponds. The maximum available capacity above the pool (elevation 89-feet) for each of the ponds is summarized in the table below:

Table 6 – Available Capacity above Pool (Maximum Pond Footprint)					
Pond	Capacity (Ac-feet)				
Pond 1	19.0				
Pond 2	19.3				
Pond 3	15.4				

Preliminary evaluations were performed using the available capacity above the normal pool using the maximum pond footprint. The preliminary evaluation considered the flows into Ponds 1 and 2 separately, with no assumed discharge structures, which is conservative. Two scenarios were evaluated for Pond 1 because limited information was available about the North Pond and Coal Pile Runoff Ponds, which attenuate flow prior to discharge into Pond 1. Pond 3 was also considered in the preliminary evaluations, which are described below:

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#### Pond 1, Scenario1:

For Pond 1, the normal pool elevation of approximately 89-feet was used as the starting elevation for the analysis. The inflow from runoff and flow from the Station was routed above the pool elevation. The flow from the boiler slag sluice, FGD blowdown, and coal pile runoff ponds as presented in Table 4 was set as a base flow of 0.58 cfs for Pond 1. Runoff from drainage areas DA-1 through DA-6 is routed through the coal pile runoff ponds. Since a flow was provided from the coal pile runoff ponds, drainage areas DA-1 through DA-6 were not included in the analysis. Runoff from drainage area DA-7 during the 25-year, 24-hour storm event was routed through Pond 1 with the base flow. Refer to Table 3 for the summary of drainage areas. The peak elevation was 91.8-feet, which is below the crest elevation of the pond.

#### Pond 1, Scenario 2:

An additional analysis was performed for Pond 1 which included the runoff from drainage areas DA-1 through DA-6 and DA-7. Again, the normal pool elevation of approximately 89-feet was used as the starting elevation for the analysis. The inflow from runoff and flow from the Station was routed above the pool elevation. The flow from the boiler slag sluice and blowdown as presented in Table 4 was sent as a base flow of 0.50 cfs for Pond 1. The base flow was reduced from 0.58 cfs to 0.50 cfs in this analysis, since 0.085 cfs is from the coal pile runoff ponds. The runoff from DA-1 through DA-7 during the 25-year, 24-hour storm event was routed through Pond 1 with the base flow. Refer to Table 3 for the summary of drainage areas. The peak elevation was 94.1-feet, which is below the crest elevation of the pond. This is conservative because it assumes drainage from DA-1 through DA-6 directly to Pond 1, when the flow is actually attenuated in ponds prior to discharge into Pond 1.

#### Pond 2:

For Pond 2, the normal pool elevation of approximately 89-feet was used as the starting elevation for the analysis. The inflow from runoff and flow from the Station was routed above the pool elevation. The flow from the fly ash sluice and the Cavin Sludge Lagoon as presented in Table 5 was set as a base flow of 0.64 cfs for Pond 2. Runoff from drainage area DA-8, from the Cavin Sludge Lagoon, and from the Concrete Pond was routed through Pond 2 with the base flow. The peak elevation was 90.5-feet, which is below the crest elevation of the pond.

#### Pond 3:

Discharge from Pond 1 and Pond 2 is routed through Pond 3. Based on information from site personnel, the discharge culvert from Pond 1 is a 30-inch diameter plastic pipe. The discharge culvert from Pond 2 is two 16-inch diameter steel pipes. As stated above, the inlet of the discharge structures in Ponds 1 and 2 were assumed to be at elevation 89-feet. Based on information from site personnel,

	Civil & Environmental C	onsultant	s, Inc.	
PROJECT	Owensboro Municipal Utilities	PROJECT NO.	164-014.0003	
	Elmer Smith Station Ash Pond		PAGE 8	OF <b>11</b>
Hydrolog	ic and Hydraulic Capacity Calculation		_	
MADE BY	AMR DATE 10/14/2016 CHE	ECKED BY	AAW DATE	10/14/2016

the discharge culverts slope approximately 1 to 2-feet. Based on this, the outlets of the discharge culverts were assumed to be at 88-feet. The lengths of the discharge culverts were approximated, and the approximate locations are shown on Figure 3. For each discharge pipe, an entrance coefficient (Ke) of 0.90 was used for projecting pipe with no headwall. This information was used in the HydroCAD model to route the flow from Ponds 1 and 2 into Pond 3.

For Pond 3, a normal pool elevation of 89-feet was used as the starting elevation for the analysis. The inflow from runoff and flow from the Station was routed above the pool elevation. Based on information from site personnel, the discharge culvert from Pond 3 is a 24-inch diameter concrete pipe. As stated above, the inlet of the discharge structure in Pond 3 was assumed to be at elevation 88-feet. The discharge structure is assumed to slope approximately 1-foot. Based on this, the outlet of the discharge structure was assumed to be at 87-feet. The length of the discharge structure was approximated, and the approximate location is shown on Figure 3. For this discharge pipe, an entrance coefficient (Ke) of 0.50 was used for a square edge headwall for concrete pipe. Based on information from site personnel, the emergency spillway is a 24-inch diameter metal pipe and is approximately 2-feet higher than the primary discharge structure. For this discharge structure, an entrance coefficient (Ke) of 0.90 was used for projecting pipe with no headwall. This information was used in the HydroCAD model.

The conservative analysis of Pond 1 (Pond 1, Scenario 2) was used when routing discharges from Pond 1 and Pond 2 through Pond 3. In addition to the flow from Ponds 1 and 2, drainage area DA-9 from Table 3 drains directly to Pond 3. During the analysis, the sim-route routing procedure was used, which allows reverse flow through ponds. Additionally, reverse culverts were added to model reverse flow from Pond 3 to Ponds 1 and 2. Using this method, the peak elevation in Pond 1 was 91.9-feet, the peak elevation in Pond 2 was 90.1-feet, and the peak elevation in Pond 3 was 90.1-feet. The peak elevations in the ponds are below the crest elevations of the ponds.

This preliminary evaluation indicates that the ponds have the required capacity for the 25-year, 24-hour storm event above the normal pool, using the maximum footprint of the ponds. In reality, the footprint of the pond and therefore, the pond capacity is reduced because CCR is temporarily stored in the ponds. An additional evaluation was performed to estimate the required capacity in the ponds assuming that the capacity is reduced due to CCR storage.

#### Additional Evaluation:

An additional evaluation was performed to estimate the required capacity of Ponds 1, 2, and 3. To perform this evaluation, the surface area of the existing pool was approximated using the aerial image. The sideslopes of the ponds are assumed to be approximately 2.5H:1V based on information provided by site personnel. Using the sideslopes and an assumed depth of approximately 8-feet, the approximate existing available pond capacity was estimated. Based on current information from the



Civil & Environmental Consultants, Inc.										
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site, the normal pool of the pond is approximately 6-feet below the pond crest, or at approximate elevation 89-feet. It was assumed that the pond capacity above the pool and above the inlet of the discharge structure is available for routing inflow. A figure showing the contours used to estimate the existing capacity above the pool is presented in Attachment 5 with the stage storage curves for the ponds. The existing capacity above the pool (elevation 89-feet) for each of the ponds is summarized in the table below:

Table 7 – Estimated Existing Capacity above Pool					
Pond	Capacity (Ac-feet)				
Pond 1	4.6				
Pond 2	4.5				
Pond 3	7.8				

The estimated capacity was entered into HydroCAD. An analysis was performed using the 25-year, 24-hour storm event. A starting elevation of approximately 89-feet was assumed in all ponds. The inflow from runoff and flow from the Station was routed above the normal pool elevation. When using the less conservative scenario for Pond 1 (Pond 1, Scenario 1), the existing capacity above the pool was sufficient. The peak elevation in Pond 1 was 93.0-feet, the peak elevation in Pond 2 was 91.7-feet, and the peak elevation in Pond 3 was 90.9-feet. The peak elevations in the ponds are below the crest elevations of the pond.

When using the conservative scenario for Pond 1 (Pond 1, Scenario 2), the existing capacity of Pond 1 above the pool was insufficient. The capacity of Ponds 2 and 3 were sufficient. The storage capacity of Pond 1 was increased in the HydroCAD model, until sufficient capacity was achieved. The estimated required pond capacity based on the conservative HydroCAD model for each pond is summarized in the table below:

Table 8 – Estimated Red	quired Capacity above Pool
Pond	Capacity (Ac-feet)
Pond 1	9.3
Pond 2	4.5
Pond 3	7.8

The peak elevation in Pond 1 was 93.9-feet, the peak elevation in Pond 2 was 91.8-feet, and the peak elevation in Pond 3 was 91.3-feet. The peak elevations in the ponds are below the crest elevations of the pond, and approximately 1-foot of freeboard is maintained.

		Civil &	k Environment	al Consulta	nts, Inc	•				
PROJECT	T Owensboro Municipal Utilities				PROJE	CT NO.	164-014.0003			
	Elmer Smith S	tation As	h Pond		PAGE	10	OF	11		
Hydrolog	Hydrologic and Hydraulic Capacity Calculation									
MADE BY	AMR	DATE	10/14/2016	CHECKED BY	AAW	DATE	10/14/20	16		

#### **CONCLUSIONS:**

Calculations were performed to compare the pond capacity with the inflow from runoff resulting from the 25 year, 24 hour storm, and flow from the Station. The HydroCAD routing for each evaluation is provided in Attachment 6. For Pond 1, two scenarios were analyzed. The first scenario included flow from the Coal Pile Runoff Ponds in the base flow, as provided by site personnel (Pond 1, Scenario 1). The second scenario used drainage areas to model runoff into Pond 1 (Pond 1, Scenario 2). This is conservative because it assumes drainage from DA-1 through DA-6 directly to Pond 1, when the flow is actually attenuated in ponds prior to discharge into Pond 1.

During the preliminary evaluation, the available capacity above the pool using the maximum footprint of the ponds was used. This preliminary evaluation indicates that the ponds have the required capacity for the 25-year, 24-hour storm event. In reality, the footprint of the pond and therefore, the pond capacity is reduced because CCR is temporarily stored in the ponds. An additional evaluation was performed to estimate the required capacity in the ponds assuming that the capacity is reduced due to CCR storage. When using the less conservative scenario for Pond 1 (Pond 1, Scenario 1), the existing capacity above the normal pool was sufficient. The estimated existing pond capacity above the pool is as follows:

Table 7 – Estimated Existing Capacity above Pool							
Pond	Capacity (Ac-feet) 4.6						
Pond 1	4.6						
Pond 2	4.5						
Pond 3	7.8						

Based on a conservative estimate of inflow into Pond 1 (Pond 1, Scenario 2), the estimated required pond capacity above the normal pool is as follows:

Table 8 – Estimated Required Capacity above Pool								
Pond	Capacity (Ac-feet)							
Pond 1	9.3							
Pond 2	4.5							
Pond 3	7.8							



		Civil &	& Environmenta	l Consultar	nts, Inc.			
PROJECT	Owensboro Mu	inicipal U	J <b>tilities</b>		PROJEC	T NO.	164-01	14.0003
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Hydrologi	ic and Hydraulic	Capacit	y Calculation					
MADE BY	AMR	DATE	10/14/2016	CHECKED BY	AAW	DATE	10/14/2	016

#### **RECOMMENDATIONS:**

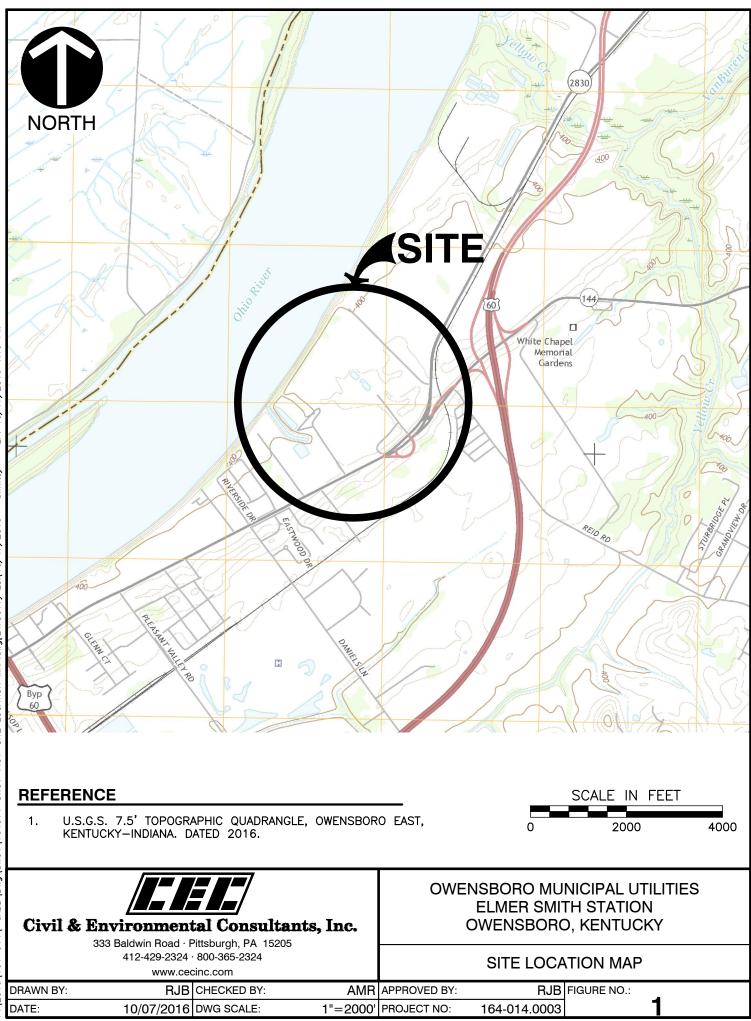
CEC recommends maintaining the following capacities above the normal pool.

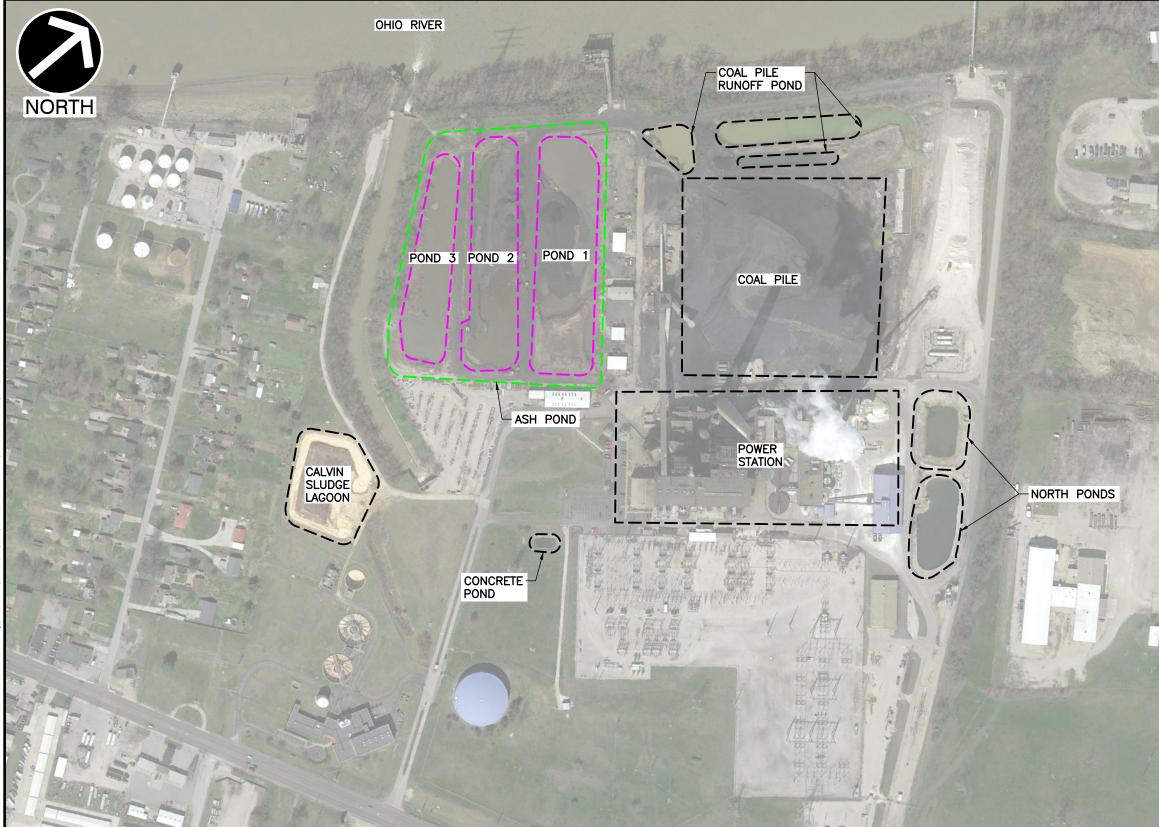
Table 8 – Estimated Required Capacity above Pool							
Pond	Capacity (Ac-feet)						
Pond 1	9.3						
Pond 2	4.5						
Pond 3	7.8						

Alternately, a total capacity of 21.6 acre-feet can be maintained above all three ponds, since the ponds are interconnected. A table showing the approximate areas and depths above the pool that are needed to maintain these capacities is presented in Attachment 7.

During these evaluations, limited information about Ponds 1, 2, and 3 of the Ash Pond was available, so assumptions were made by CEC. CEC is basing the above requirements on a conservative assumption about the flow to Pond 1. CEC notes that incorporating more information about the North Ponds and the Coal Runoff Ponds into the model could reduce the required capacity above the pool elevation.

### FIGURES







#### REFERENCE

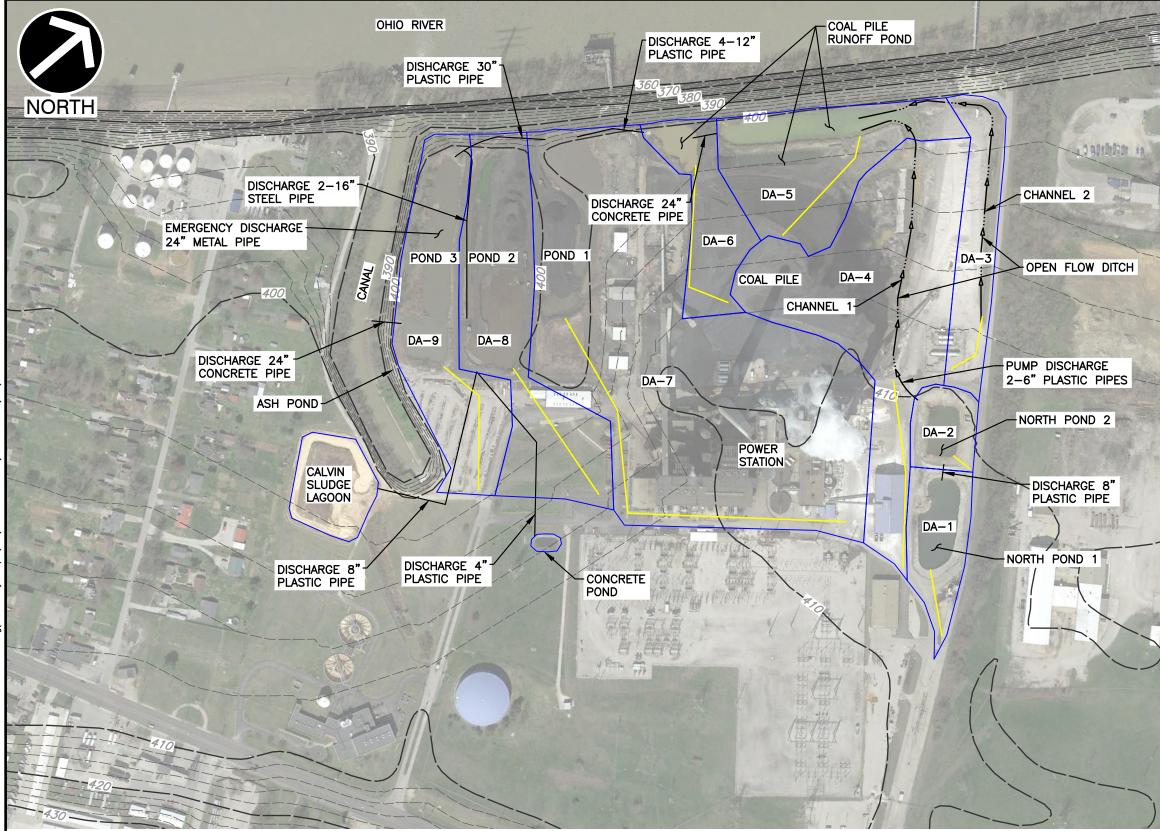
1. AERIAL PHOTOGRAPHY COPYRIGHT GOOGLE EARTH PRO VERSION 6.2, IMAGERY DATE 3-25-2016.

LEGEND
ASH POND LIMITS APPROXIMATE FOOTPRINT 
OTHER SITE FEATURES
NOTES
1. THE APPROXIMATE FOOTPRINT OF PONDS 1, 2, AND 3 IS BASED ON DRAWING NO. S-7 " STRUCTURAL FILL FINISH GRADING" PREPARED BY BLACK AND VEACH, DATED 8-28-62 AND THE AERIAL PHOTOGRAPHY (SEE REFERENCE 1).
SCALE IN FEET
0 300 600
OWENSBORO MUNICIPAL UTILITIES ELMER SMITH STATION OWENSBORO, KENTUCKY
EXISTING CONDITIONS

RJB FIGURE NO .:

164-014.0003

2



#### REFERENCE

- 1. AERIAL PHOTOGRAPHY COPYRIGHT GOOGLE EARTH PRO VERSION 6.2, IMAGERY DATE 3-25-2016.
- 10' CONTOUR DATA PROVIDED BY USGS NATIONAL MAP FROM THE NATIONAL ELEVATION DATASET (NED), OWENSBORO EAST QUADRANGLE, PUBLICATION DATE – 05/27/2016



LEGEND	
—— 400 ——	EXISTING TOPOGRAPHIC CONTOUR (SEE REFERENCE 2)
	EXISTING DISCHARGE PIPE (SEE NOTE 1)
⊳	EXISTING OPEN FLOW DITCH (SEE NOTE 1)
	TIME OF CONCENTRATION PATH
	DRAINAGE AREA BOUNDARY

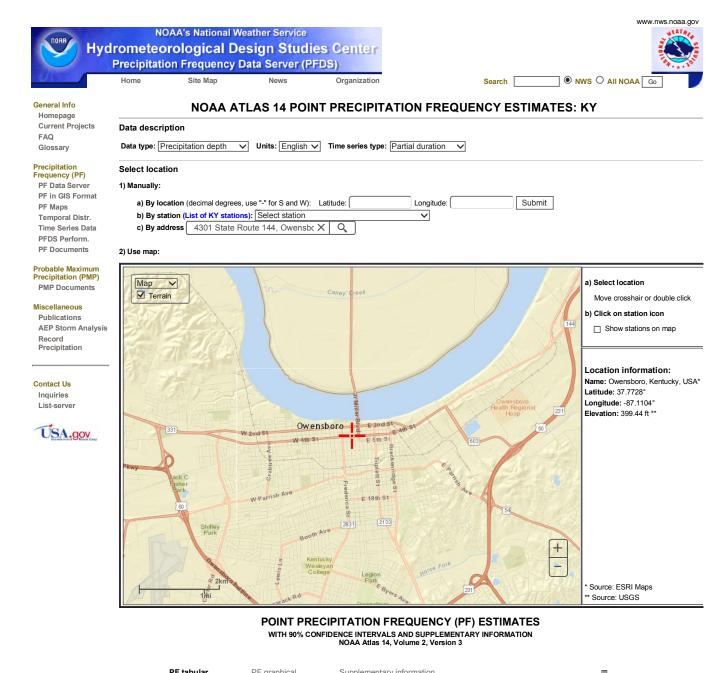
#### NOTES

	DISCHARGE PIPES AN OPEN FLOW DITCHES BASED ON INFORMAT PERSONNEL AND THI (SEE REFERENCE 1)	SIZES OF THE EXISTING ND THE LOCATIONS OF ARE APPROXIMATED TION PROVIDED BY SITE AERIAL PHOTOGRAPHY SCALE IN FEET
с.	OWENSBORO MUI ELMER SMIT OWENSBORC DRAINAGE	TH STATION D, KENTUCKY
AMR	APPROVED BY: RJB	FIGURE NO.:
=300'	PROJECT NO: 164-014.0003	3

### ATTACHMENTS

### ATTACHMENT 1

# NOAA DATA FOR OWENSBORO, KENTUCKY



	PF tabular	PF graphical Supplementary information						Print page				
		PDS-based	precipitatio	n frequency	estimates v	vith 90% cor	fidence inte	rvals (in inc	hes) <sup>1</sup>			
	Average recurrence interval (years)											
Duration	1	2	5	10	25	50	100	200	500	1000		
5-min	0.358	<b>0.421</b>	<b>0.491</b>	<b>0.544</b>	0.615	<b>0.667</b>	<b>0.718</b>	<b>0.771</b>	<b>0.838</b>	0.886		
	(0.327-0.393)	(0.385-0.462)	(0.449-0.539)	(0.496-0.597)	(0.558-0.673)	(0.602-0.730)	(0.645-0.785)	(0.688–0.846)	(0.742-0.919)	(0.779-0.97		
10-min	0.568	0.669	<b>0.778</b>	0.862	0.968	<b>1.05</b>	<b>1.13</b>	<b>1.20</b>	<b>1.30</b>	<b>1.37</b>		
	(0.518-0.622)	(0.612-0.734)	(0.712-0.855)	(0.785-0.945)	(0.878-1.06)	(0.946-1.15)	(1.01–1.23)	(1.07–1.32)	(1.15-1.42)	(1.20-1.50		
15-min	<b>0.707</b>	0.834	<b>0.976</b>	<b>1.08</b>	<b>1.22</b>	<b>1.32</b>	<b>1.42</b>	<b>1.51</b>	<b>1.63</b>	<b>1.71</b>		
	(0.646-0.775)	(0.763-0.916)	(0.893–1.07)	(0.986–1.19)	(1.11-1.33)	(1.19–1.44)	(1.27–1.55)	(1.35–1.66)	(1.44-1.79)	(1.50-1.88		
30-min	0.959	<b>1.14</b>	<b>1.37</b>	<b>1.55</b>	<b>1.78</b>	<b>1.96</b>	<b>2.14</b>	<b>2.31</b>	<b>2.54</b>	<b>2.71</b>		
	(0.876-1.05)	(1.05–1.26)	(1.26-1.51)	(1.42–1.70)	(1.62–1.95)	(1.77-2.14)	(1.92–2.34)	(2.06–2.53)	(2.25-2.79)	(2.39–2.99		
60-min	<b>1.19</b>	<b>1.43</b>	<b>1.75</b>	<b>2.01</b>	2.36	<b>2.64</b>	<b>2.92</b>	<b>3.21</b>	3.61	<b>3.92</b>		
	(1.09–1.31)	(1.31–1.57)	(1.60-1.93)	(1.83-2.20)	(2.14-2.58)	(2.38-2.89)	(2.62–3.19)	(2.87–3.52)	(3.20-3.96)	(3.45-4.32		
2-hr	<b>1.43</b>	<b>1.72</b>	<b>2.14</b>	<b>2.47</b>	<b>2.92</b>	<b>3.28</b>	<b>3.65</b>	<b>4.04</b>	<b>4.57</b>	<b>4.98</b>		
	(1.31–1.56)	(1.58–1.88)	(1.96–2.33)	(2.26–2.69)	(2.66-3.18)	(2.98-3.56)	(3.30–3.97)	(3.62–4.39)	(4.04-4.98)	(4.38-5.45		
3-hr	<b>1.54</b>	<b>1.86</b>	<b>2.30</b>	<b>2.67</b>	<b>3.17</b>	<b>3.58</b>	<b>4.00</b>	<b>4.44</b>	<b>5.06</b>	<b>5.56</b>		
	(1.42–1.68)	(1.71-2.03)	(2.11–2.52)	(2.44–2.91)	(2.89-3.45)	(3.24-3.89)	(3.61–4.35)	(3.98–4.83)	(4.47-5.52)	(4.86-6.07		
6-hr	<b>1.90</b>	<b>2.28</b>	<b>2.82</b>	<b>3.28</b>	<b>3.92</b>	<b>4.45</b>	<b>5.02</b>	<b>5.61</b>	<b>6.46</b>	<b>7.15</b>		
	(1.74–2.07)	(2.09–2.49)	(2.59–3.08)	(3.00-3.58)	(3.57-4.27)	(4.02-4.84)	(4.50–5.45)	(4.99–6.10)	(5.67-7.03)	(6.20-7.81		
12-hr	<b>2.27</b>	<b>2.73</b>	<b>3.39</b>	<b>3.93</b>	<b>4.70</b>	<b>5.33</b>	<b>6.01</b>	<b>6.72</b>	<b>7.74</b>	<b>8.57</b>		
	(2.08–2.49)	(2.51-3.00)	(3.10-3.71)	(3.58-4.30)	(4.26-5.14)	(4.81–5.82)	(5.38–6.56)	(5.97–7.35)	(6.79-8.48)	(7.42-9.41		
24-hr	2.71	3.26	4.07	4.72	5.67	6.45	7.28	8.17	9.43	10.5		

	(2.54-2.90)	(3.06-3.49)	(3.80-4.35)	(4.41-5.05)	(5.25-6.05)	(5.94-6.89)	(6.65-7.79)	(7.39-8.77)	(8.40-10.2)	(9.21-11.3)
2-day	3.26	3.91	<b>4.88</b>	5.68	6.83	7.79	8.83	<b>9.94</b>	<b>11.5</b>	<b>12.9</b>
	(3.04-3.50)	(3.64-4.20)	(4.53-5.24)	(5.27-6.09)	(6.30-7.33)	(7.14-8.39)	(8.02-9.52)	(8.94–10.8)	(10.2–12.6)	(11.3–14.1)
3-day	<b>3.47</b>	<b>4.16</b>	<b>5.19</b>	<b>6.04</b>	<b>7.28</b>	<b>8.32</b>	<b>9.43</b>	<b>10.6</b>	<b>12.4</b>	<b>13.8</b>
	(3.24–3.72)	(3.89-4.47)	(4.83–5.57)	(5.61–6.48)	(6.72-7.81)	(7.63-8.95)	(8.58-10.2)	(9.58–11.5)	(11.0-13.5)	(12.1–15.2)
4-day	<b>3.68</b>	<b>4.41</b>	<b>5.50</b>	<b>6.40</b>	<b>7.73</b>	<b>8.84</b>	<b>10.0</b>	<b>11.3</b>	<b>13.2</b>	<b>14.8</b>
	(3.44–3.95)	(4.13-4.74)	(5.13-5.90)	(5.96–6.87)	(7.15-8.29)	(8.12-9.51)	(9.14–10.8)	(10.2–12.3)	(11.7-14.4)	(13.0-16.2)
7-day	<b>4.28</b> (3.98-4.62)	<b>5.13</b> (4.77–5.55)	6.42 (5.96-6.94)	7.55 (6.98-8.16)	<b>9.24</b> (8.47-9.98)	<b>10.7</b> (9.74–11.6)	<b>12.3</b> (11.1–13.4)	<b>14.2</b> (12.6–15.5)	<b>16.9</b> (14.7-18.6)	<b>19.2</b> (16.5–21.3)
10-day	<b>4.82</b>	<b>5.77</b>	<b>7.19</b>	8.40	<b>10.2</b>	<b>11.8</b>	<b>13.5</b>	<b>15.3</b>	<b>18.1</b>	<b>20.5</b>
	(4.49–5.20)	(5.37–6.23)	(6.67–7.75)	(7.78-9.05)	(9.38-11.0)	(10.7-12.7)	(12.1–14.6)	(13.7–16.7)	(15.9–19.9)	(17.7-22.7)
20-day	<b>6.65</b>	<b>7.90</b>	<b>9.51</b>	<b>10.8</b>	<b>12.7</b>	<b>14.1</b>	<b>15.6</b>	<b>17.2</b>	<b>19.4</b>	<b>21.2</b>
	(6.27-7.06)	(7.44-8.39)	(8.94–10.1)	(10.1–11.5)	(11.8-13.5)	(13.1–15.0)	(14.4–16.7)	(15.8–18.4)	(17.6-20.9)	(19.0-22.9)
30-day	8.20	<b>9.70</b>	<b>11.5</b>	<b>12.9</b>	<b>14.9</b>	<b>16.5</b>	<b>18.0</b>	<b>19.6</b>	<b>21.8</b>	<b>23.4</b>
	(7.76-8.66)	(9.17–10.3)	(10.9–12.2)	(12.2–13.7)	(14.0-15.8)	(15.4–17.4)	(16.8–19.1)	(18.2–20.9)	(19.9–23.3)	(21.3-25.2)
45-day	<b>10.4</b> (9.85–10.9)	<b>12.2</b> (11.6–12.8)	<b>14.2</b> (13.5–14.9)	<b>15.8</b> (15.0–16.6)	<b>17.8</b> (16.8–18.7)	<b>19.3</b> (18.2–20.3)	<b>20.8</b> (19.6-22.0)	<b>22.3</b> (20.9–23.6)	<b>24.2</b> (22.5-25.7)	<b>25.6</b> (23.7–27.3)
60-day	<b>12.4</b>	<b>14.6</b>	<b>16.8</b>	<b>18.5</b>	<b>20.5</b>	<b>22.1</b>	<b>23.5</b>	24.9	<b>26.6</b>	27.8
	(11.8-13.0)	(13.9–15.3)	(16.0–17.6)	(17.5–19.3)	(19.5-21.5)	(20.9-23.2)	(22.2-24.7)	(23.4-26.2)	(24.9-28.1)	(25.9-29.5)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

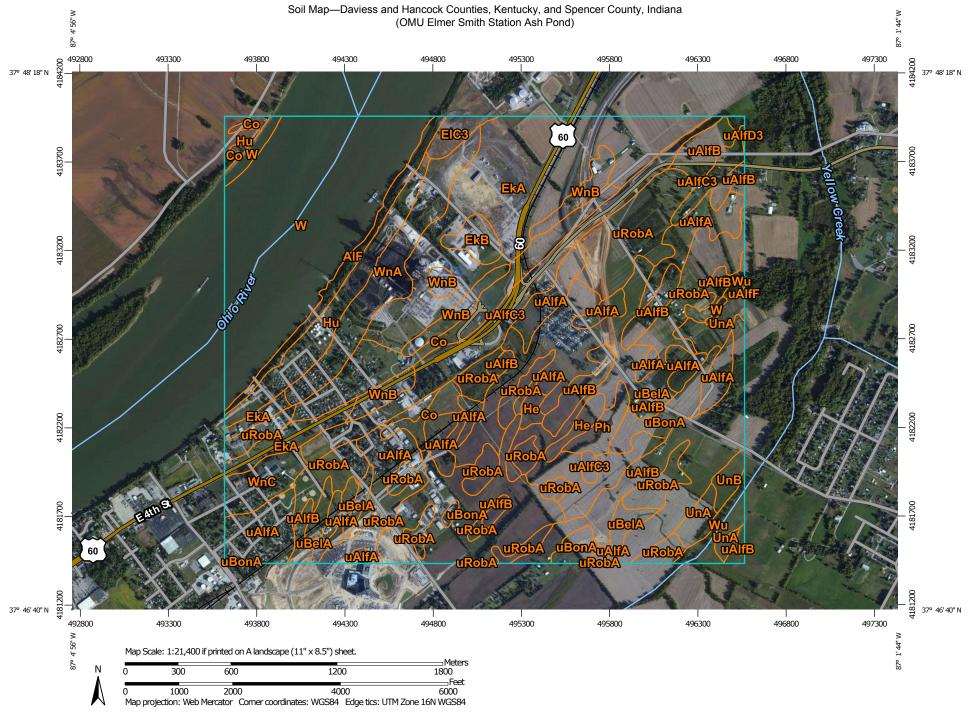
Estimates from the table in CSV format: Precipitation frequency estimates V Submit

#### Main Link Categories: Home | OWP(OHD)

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service Office of Water Prediction (OWP) 1325 East West Highway Silver Spring, MD 20910 Page Author: HDSC webmaster Page last modified: August 27, 2014 Map Disclaimer Disclaimer Credits Glossary Privacy Poli About I Career Opportuniti

### ATTACHMENT 2

### USDA NRCS SOIL SURVEY MAP



USDA Natural Resources

Conservation Service

Web Soil Survey National Cooperative Soil Survey

M	P LEGEND	MAP INFORMATION
Area of Interest (AOI) Area of Interest (A Soils Soil Map Unit Poly Soil Map Unit Line Soil Map Unit Poir Special Point Features Blowout Borrow Pit Clay Spot	DI) Spoil Area OI) Stony Spot Mons Wet Spot A Other	The soil surveys that comprise your AOI were mapped at scal ranging from 1:15,800 to 1:20,000. Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercat projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as t Albers equal-area conic projection, should be used if more accu- calculations of distance or area are required.
<ul> <li>Closed Depressio</li> <li>Gravel Pit</li> <li>Gravelly Spot</li> <li>Landfill</li> <li>Lava Flow</li> <li>Lava Flow</li> <li>Marsh or swamp</li> <li>Mine or Quarry</li> <li>Miscellaneous Wa</li> <li>Perennial Water</li> <li>Rock Outcrop</li> <li>Saline Spot</li> <li>Sandy Spot</li> <li>Severely Eroded S</li> <li>Sinkhole</li> <li>Slide or Slip</li> <li>Sodic Spot</li> </ul>	er	<ul> <li>This product is generated from the USDA-NRCS certified data the version date(s) listed below.</li> <li>Soil Survey Area: Daviess and Hancock Counties, Kentucky Survey Area Data: Version 14, Sep 15, 2015</li> <li>Soil Survey Area: Spencer County, Indiana Survey Area Data: Version 16, Sep 11, 2015</li> <li>Your area of interest (AOI) includes more than one soil survey at a different land use in mind, at different times, or at different lee of detail. This may result in map unit symbols, soil properties, interpretations that do not completely agree across soil survey boundaries.</li> <li>Soil map units are labeled (as space allows) for map scales 1:50 or larger.</li> <li>Date(s) aerial images were photographed: Oct 3, 2011—Oct 2011</li> <li>The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor sh of map unit boundaries may be evident.</li> </ul>

# Map Unit Legend

	Daviess and Hancock Count	cies, Kentucky (KY615)	
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
AIF	Alluvial land, steep (wheeling flooded)	25.9	1.4%
Со	Collins silt loam	74.9	4.1%
EkA	Elk silt loam, 0 to 2 percent slopes, rarely flooded	221.1	12.0%
EkB	Elk silt loam, 2 to 6 percent slopes, rarely flooded	13.7	0.7%
EIC3	Elk silty clay loam, 6 to 12 percent slopes, severely eroded	11.3	0.6%
Не	Henshaw silt loam	14.5	0.8%
Hu	Huntington silt loam	50.6	2.7%
Ph	Patton silt loam, overwash, 0 to 2 percent slopes, occasionally flooded	14.0	0.8%
uAlfA	Alford silt loam, 0 to 2 percent slopes	170.1	9.2%
uAlfB	Alford silt loam, 2 to 6 percent slopes	171.5	9.3%
uAlfC3	Alford silt loam, 6 to 12 percent slopes, severely eroded	100.7	5.5%
uAlfD3	Alford silt loam, 12 to 20 percent slopes, severely eroded	0.6	0.0%
uAlfF	Alford silt loam, 30 to 60 percent slopes	0.1	0.0%
uBelA	Belknap silt loam, 0 to 2 percent slopes, occasionally flooded	185.1	10.0%
uBonA	Bonnie silt loam, 0 to 2 percent slopes, occasionally flooded	122.0	6.6%
UnA	Uniontown silt loam, 0 to 2 percent slopes	30.2	1.6%
UnB	Uniontown silt loam, 2 to 6 percent slopes	8.4	0.5%
uRobA	Robbs silt loam, 0 to 2 percent slopes	206.6	11.2%
W	Water	251.5	13.6%
WnA	Wheeling loam, 0 to 2 percent slopes	68.1	3.7%
WnB	Wheeling loam, 2 to 6 percent slopes	44.3	2.4%
WnC	Wheeling loam, 6 to 12 percent slopes	25.2	1.4%
Wu	Wilbur silt loam	15.9	0.9%

Daviess and Hancock Counties, Kentucky (KY615)					
Map Unit Symbol         Map Unit Name         Acres in AOI         Percent of AOI					
Subtotals for Soil Survey Area		1,826.4	99.0%		
Totals for Area of Interest		1,845.2	100.0%		

Spencer County, Indiana (IN147)				
Map Unit Symb	ool Map Unit Name	Acres in AOI	Percent of AOI	
Co	Combs fine sandy loam, frequently flooded, brief duration	5.2	0.3%	
Hu	Huntington silt loam, frequently flooded, brief duration	5.9	0.3%	
W	Water	7.7	0.4%	
Subtotals for Soil Survey Area		18.8	1.0%	
Totals for Area of Interest		1,845.2	100.0%	

#### Huntington

Percent of map unit: 5 percent Hydric soil rating: No

#### Elk

Percent of map unit: 3 percent Hydric soil rating: No

#### Wheeling, (hydric-green river)

Percent of map unit: 1 percent Landform: Flood plains Landform position (two-dimensional): Backslope Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: Yes

### Wheeling, (hydric-ohio river)

Percent of map unit: 1 percent Landform: Flood plains Landform position (two-dimensional): Backslope Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: Yes

# **Co—Collins silt loam**

#### Map Unit Setting

National map unit symbol: Ifnq Elevation: 350 to 600 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 210 days Farmland classification: All areas are prime farmland

#### Map Unit Composition

*Collins, occasionally flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Collins, Occasionally Flooded**

#### Setting

Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Coarse-silty alluvium

#### **Typical profile**

H1 - 0 to 7 inches: silt loam

H2 - 7 to 60 inches: silt loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 18 to 36 inches
Frequency of flooding: Occasional
Frequency of ponding: None
Available water storage in profile: Very high (about 13.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: B/D Hydric soil rating: No

#### **Minor Components**

#### Belknap

Percent of map unit: 4 percent Hydric soil rating: No

#### Collins, (hydric)

Percent of map unit: 2 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Other soils

Percent of map unit: 2 percent Hydric soil rating: No

#### Grenada

Percent of map unit: 2 percent Hydric soil rating: No

# EkA—Elk silt loam, 0 to 2 percent slopes, rarely flooded

# Map Unit Setting

National map unit symbol: 2s2c7 Elevation: 320 to 640 feet Mean annual precipitation: 36 to 61 inches Mean annual air temperature: 42 to 70 degrees F Frost-free period: 154 to 232 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

*Elk, rarely flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Elk, Rarely Flooded**

#### Setting

Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Mixed fine-silty alluvium

#### **Typical profile**

Ap - 0 to 8 inches: silt loam BA - 8 to 12 inches: silty clay loam Bt - 12 to 36 inches: silty clay loam C - 36 to 80 inches: loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Rare
Frequency of ponding: None
Available water storage in profile: High (about 11.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 1 Hydrologic Soil Group: B Other vegetative classification: Deep Well Drained Upland Soils 0-30% (PHG-5) Hydric soil rating: No

#### **Minor Components**

#### Wheeling, rarely flooded

Percent of map unit: 4 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Sciotoville, rarely flooded

Percent of map unit: 4 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Weinbach, rarely flooded

Percent of map unit: 2 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

# EkB—Elk silt loam, 2 to 6 percent slopes, rarely flooded

#### Map Unit Setting

National map unit symbol: 2slf6 Elevation: 300 to 700 feet Mean annual precipitation: 36 to 61 inches Mean annual air temperature: 42 to 70 degrees F Frost-free period: 154 to 232 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

*Elk, rarely flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Elk, Rarely Flooded**

#### Setting

Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Parent material: Mixed fine-silty alluvium

#### **Typical profile**

Ap - 0 to 8 inches: silt loam BA - 8 to 12 inches: silty clay loam Bt - 12 to 36 inches: silty clay loam C - 36 to 80 inches: loam

### Properties and qualities

Slope: 2 to 6 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Rare
Frequency of ponding: None
Available water storage in profile: High (about 11.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: B Other vegetative classification: Deep Well Drained Upland Soils 0-30% (PHG-5) Hydric soil rating: No

#### **Minor Components**

#### Sciotoville, rarely flooded

Percent of map unit: 4 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Wheeling, rarely flooded

Percent of map unit: 4 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Weinbach, rarely flooded

Percent of map unit: 2 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

# EIC3—Elk silty clay loam, 6 to 12 percent slopes, severely eroded

#### **Map Unit Setting**

National map unit symbol: Ifnw Elevation: 360 to 420 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 210 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Elk, severely eroded, and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Other soils

Percent of map unit: 3 percent Hydric soil rating: No

# Hu—Huntington silt loam

#### Map Unit Setting

National map unit symbol: Ifp7 Elevation: 350 to 440 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 210 days Farmland classification: All areas are prime farmland

#### Map Unit Composition

*Huntington, occasionally flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Huntington, Occasionally Flooded**

#### Setting

Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Mixed fine-silty alluvium

#### **Typical profile**

H1 - 0 to 8 inches: silt loam H2 - 8 to 60 inches: silt loam

#### **Properties and qualities**

Slope: 0 to 4 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Occasional
Frequency of ponding: None
Available water storage in profile: High (about 11.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: B Hydric soil rating: No

#### **Minor Components**

#### Lindside

Percent of map unit: 3 percent Hydric soil rating: No

#### Ashton

Percent of map unit: 3 percent Hydric soil rating: No

### Other soils

Percent of map unit: 2 percent Hydric soil rating: No

#### Huntington, (hydric green river)

Percent of map unit: 1 percent Landform: Flood plains Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Huntington, (hydric ohio river)

Percent of map unit: 1 percent Landform: Flood plains Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

# Ph—Patton silt loam, overwash, 0 to 2 percent slopes, occasionally flooded

#### **Map Unit Setting**

National map unit symbol: 2r14l Elevation: 350 to 470 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 215 days Farmland classification: Prime farmland if drained

#### **Map Unit Composition**

Patton, occasionally flooded, overwash, and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### Description of Patton, Occasionally Flooded, Overwash

#### Setting

Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Estimates are based on observations, descriptions, and transects of the mapunit.

# WnA—Wheeling loam, 0 to 2 percent slopes

#### **Map Unit Setting**

National map unit symbol: Ifqt Elevation: 350 to 420 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 210 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Wheeling, rarely flooded, and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Wheeling, Rarely Flooded**

#### Setting

Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Fine-loamy alluvium

#### **Typical profile**

H1 - 0 to 7 inches: loam H2 - 7 to 25 inches: loam H3 - 25 to 60 inches: fine sandy loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Rare
Frequency of ponding: None
Available water storage in profile: Low (about 5.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 1 Hydrologic Soil Group: B Hydric soil rating: No

#### **Minor Components**

#### Other soils

Percent of map unit: 4 percent Hydric soil rating: No Elk

Percent of map unit: 2 percent Hydric soil rating: No

Sciotoville

Percent of map unit: 2 percent Hydric soil rating: No

Wheeling, (hydric ohio river)

Percent of map unit: 1 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Wheeling, (hydric green river)

Percent of map unit: 1 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### WnB—Wheeling loam, 2 to 6 percent slopes

#### Map Unit Setting

National map unit symbol: Ifqv Elevation: 350 to 430 feet Mean annual precipitation: 36 to 52 inches Mean annual air temperature: 46 to 68 degrees F Frost-free period: 174 to 210 days Farmland classification: All areas are prime farmland

### Map Unit Composition

*Wheeling, rarely flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Wheeling, Rarely Flooded**

#### Setting

Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Parent material: Fine-loamy alluvium

### **Typical profile**

*H1 - 0 to 7 inches:* loam *H2 - 7 to 25 inches:* loam

H3 - 25 to 72 inches: fine sandy loam

#### **Properties and qualities**

Slope: 2 to 6 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Rare
Frequency of ponding: None
Available water storage in profile: Low (about 5.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: B Hydric soil rating: No

#### **Minor Components**

### Other soils

Percent of map unit: 4 percent Hydric soil rating: No

#### Elk

*Percent of map unit:* 2 percent *Hydric soil rating:* No

#### Sciotoville

Percent of map unit: 2 percent Hydric soil rating: No

#### Wheeling, (hydric green river)

Percent of map unit: 1 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: Yes

#### Wheeling, (hydric ohio river)

Percent of map unit: 1 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: Yes

# ATTACHMENT 3

# CORRESPONDENCE

# Ramirez, Angela

From: Sent: To: Subject: Buffalini, Rick Friday, October 07, 2016 3:05 PM Ramirez, Angela Fwd: OMU Ash pond runoff

Sent from my iPhone

Begin forwarded message:

From: Jim Roberts <<u>RobertsJM@omu.org</u>>
Date: October 7, 2016 at 9:26:15 AM EDT
To: "Buffalini, Rick" <<u>rbuffalini@cecinc.com</u>>, "Dixon, Stephen" <<u>sdixon@cecinc.com</u>>
Subject: RE: OMU Ash pond runoff

Rick:

Water flows to the ash ponds, from plant use and not including any direct rainfall, total as follows: Pond #1 inflow: Slag sluice is 250,000 GPD, FGD Blowdown is 66,400 GPD, Coal Pile Runoff Pond is 55,000 GPD. Pond #2 inflow: Ash sluice is 375,000 GPD, Cavin Water Plant Sludge Discharge is 40,000 GPD. Jim James M. Roberts, P E Owensboro Municipal Utilities Fuels & By-Products Manager robertsjm@omu.org Office: 270-691-4221 Cell: 270-313-2999

From: Buffalini, Rick [mailto:rbuffalini@cecinc.com]
Sent: Thursday, October 06, 2016 7:32 AM
To: Jim Roberts; Dixon, Stephen
Subject: RE: OMU Ash pond runoff

Thank you James

Rick J. Buffalini, P.E. / Vice President Civil & Environmental Consultants, Inc. 333 Baldwin Road · Pittsburgh, PA 15205-1751 Toll-Free: 800-365-2324 · Direct: 412-249-3169 Mobile: 412-760-9133 · <u>http://www.cecinc.com</u> Senior Leadership · Integrated Services · Personal Business Relationships

From: Jim Roberts [mailto:RobertsJM@omu.org] Sent: Wednesday, October 05, 2016 5:24 PM To: Dixon, Stephen; Buffalini, Rick Subject: OMU Ash pond runoff Attached maps should depict runoff area into ash pond system. I will soon forward water balance for amounts of water OMU discharges into ponds under normal operating mode. Let me know if you have questions. THANKS Jim James M. Roberts, P E Owensboro Municipal Utilities Fuels & By-Products Manager <u>robertsjm@omu.org</u> Office: 270-691-4221 Cell: 270-313-2999

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# Ramirez, Angela

From:	Jim Roberts <robertsjm@omu.org></robertsjm@omu.org>
Sent:	Tuesday, October 11, 2016 3:59 PM
То:	Ramirez, Angela
Cc:	Buffalini, Rick; Dixon, Stephen
Subject:	Re: OMU Ash pond runoff

Ash ponds 1 and 2 inlets are at least 1 ft higher than outlet. Approx 6 feet of freeboard. Water depth is 12 to 14 feet. Emergency outfall from pond 3 is 2 feet higher than primary. Water can back up in all 3 ponds. Pond side slopes are 2.5 to 1. Ditch flow channels are 3 to 4 feet wide at flow line. Incised ponds.

Jim

On Oct 11, 2016, at 9:00 AM, "Ramirez, Angela" <aramirez@cecinc.com> wrote:

> James,

>

> Thanks for the information that you have provided up to this point. Can you please also provide/confirm the following information:

>

> · We assume the total pond capacity for Pond 1, 2, and 3 can be obtained based on the contours for the ponds in the attached pdf labeled 'Flow diagram questions'. Please confirm.

>

> · Provide approximate elevations of the beginning and ends of the discharge structures for Ponds 1, 2, and 3. The dimensions of the pipe were previously provided.

>

Provide the approximate depth of water (if available) in the ponded areas in Ponds 1, 2, and 3. The approximate > · extents of the ponded areas are shown on the attached pdf labeled 'Existing Conditions questions'. Additionally, provide the depth to water from the crest of the ponds.

>

Provide the approximate depth of the additional ponds that drain to Ponds 1, 2, and 3. Additionally, provide the > · depth to water from the crest of the ponds.

>

What is the approximate interior sideslopes of the additional ponds at the site that drain to Ponds 1, 2, and 3? > ·

>

Provide the approximate elevations of the beginning and ends of the discharge structures for the additional > • ponds. The dimensions of the pipe were previously provided.

>

> · Please provide the approximate dimensions of the open channels. The channels are shown on the pdf labeled 'Flow diagram questions'.

>

Please confirm whether the ponds are incised. Are there any structural fill embankments for the ponds? The > · CCR Rules define an incised CCR surface impoundment as follows:

>

> Incised CCR surface impoundment means a CCR surface impoundment which is constructed by excavating entirely below the natural ground surface, holds an accumulation of CCR entirely below the adjacent natural ground surface, and does not consist of any constructed diked portion.

>

- > Let me know if you have time for a call to discuss these questions. Thanks!
- >
- > Angela M. Ramirez / Project Manager
- > Civil & Environmental Consultants, Inc.
- > 333 Baldwin Road · Pittsburgh, PA 15205-1751
- > Toll-Free: (800) 365-2324 · Direct: (412) 249-2291 · Fax: (412)
- > 429-2114
- > Mobile: (724) 600-4880 · http://www.cecinc.com Senior Leadership ·
- > Integrated Services · Personal Business Relationships
- >
- > From: Buffalini, Rick
- > Sent: Friday, October 07, 2016 3:05 PM
- > To: Ramirez, Angela
- > Subject: Fwd: OMU Ash pond runoff
- >
- >
- >
- > Sent from my iPhone
- > 50111
- >
- > Begin forwarded message:
- > From: Jim Roberts < RobertsJM@omu.org < mailto:RobertsJM@omu.org >>
- > Date: October 7, 2016 at 9:26:15 AM EDT
- > To: "Buffalini, Rick"
- > <rbuffalini@cecinc.com<mailto:rbuffalini@cecinc.com>>, "Dixon,
- > Stephen" <sdixon@cecinc.com<mailto:sdixon@cecinc.com>>
- > Subject: RE: OMU Ash pond runoff
- > Rick:
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- > Pond #2 inflow: Ash sluice is 375,000 GPD, Cavin Water Plant Sludge Discharge is 40,000 GPD.
- > Jim
- > James M. Roberts, P E
- > Owensboro Municipal Utilities
- > Fuels & By-Products Manager
- > robertsjm@omu.org<mailto:robertsjm@omu.org>
- > Office: 270-691-4221
- > Cell: 270-313-2999
- >
- >
- >
- > From: Buffalini, Rick [mailto:rbuffalini@cecinc.com]
- > Sent: Thursday, October 06, 2016 7:32 AM
- > To: Jim Roberts; Dixon, Stephen
- > Subject: RE: OMU Ash pond runoff
- >
- > Thank you James
- >

<sup>&</sup>gt; Rick J. Buffalini, P.E. / Vice President Civil & Environmental

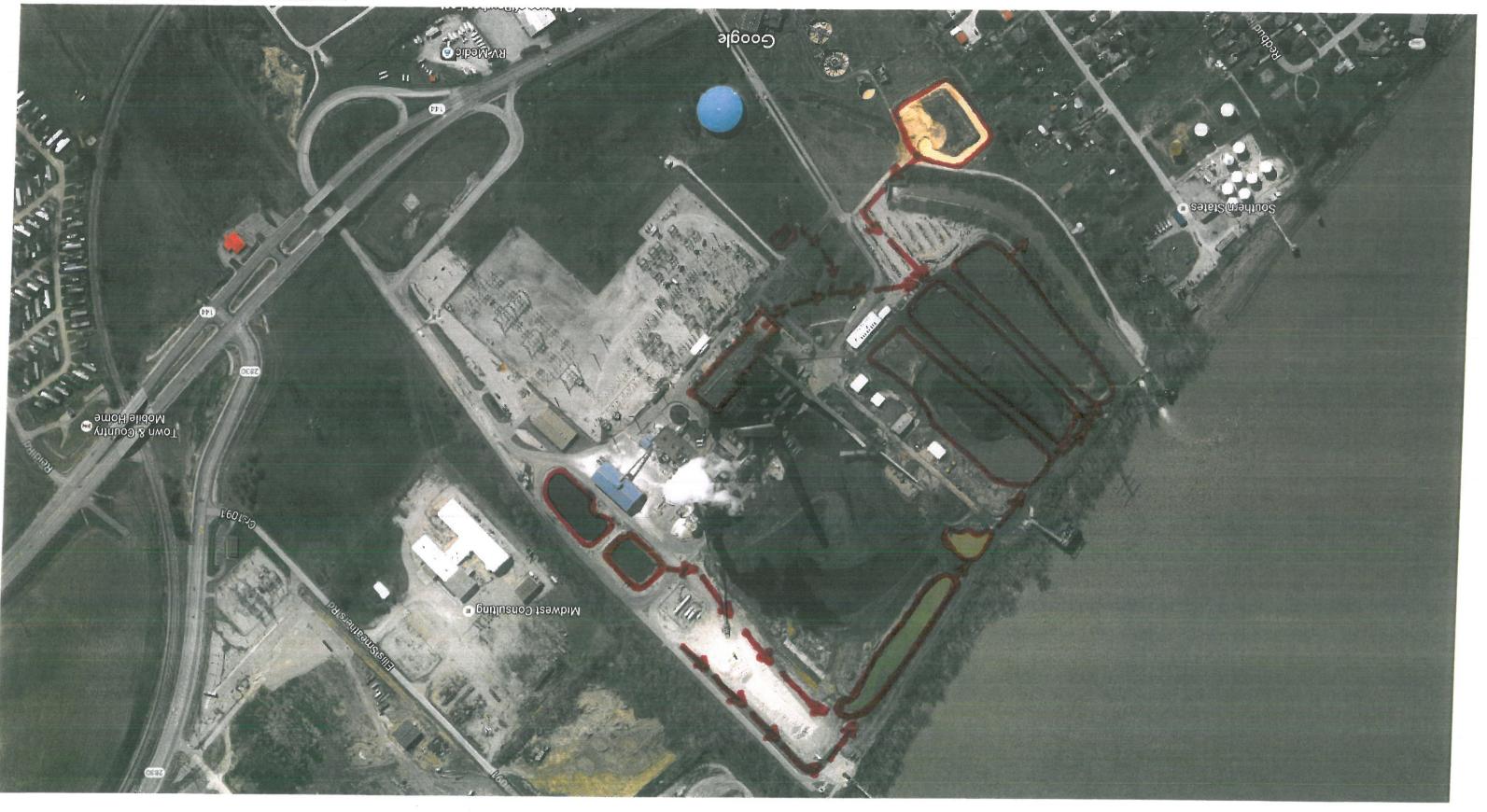
- > Consultants, Inc.
- > 333 Baldwin Road · Pittsburgh, PA 15205-1751
- > Toll-Free: 800-365-2324 · Direct: 412-249-3169
- > Mobile: 412-760-9133 · http://www.cecinc.com Senior Leadership ·
- > Integrated Services · Personal Business Relationships

>

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- > Sent: Wednesday, October 05, 2016 5:24 PM
- > To: Dixon, Stephen; Buffalini, Rick
- > Subject: OMU Ash pond runoff
- >
- >
- > Attached maps should depict runoff area into ash pond system.
- > I will soon forward water balance for amounts of water OMU discharges into ponds under normal operating mode.
- > Let me know if you have questions.
- > THANKS
- > Jim
- > James M. Roberts, P E
- > Owensboro Municipal Utilities
- > Fuels & By-Products Manager
- > robertsjm@omu.org<mailto:robertsjm@omu.org>
- > Office: 270-691-4221
- > Cell: 270-313-2999
- >
- >

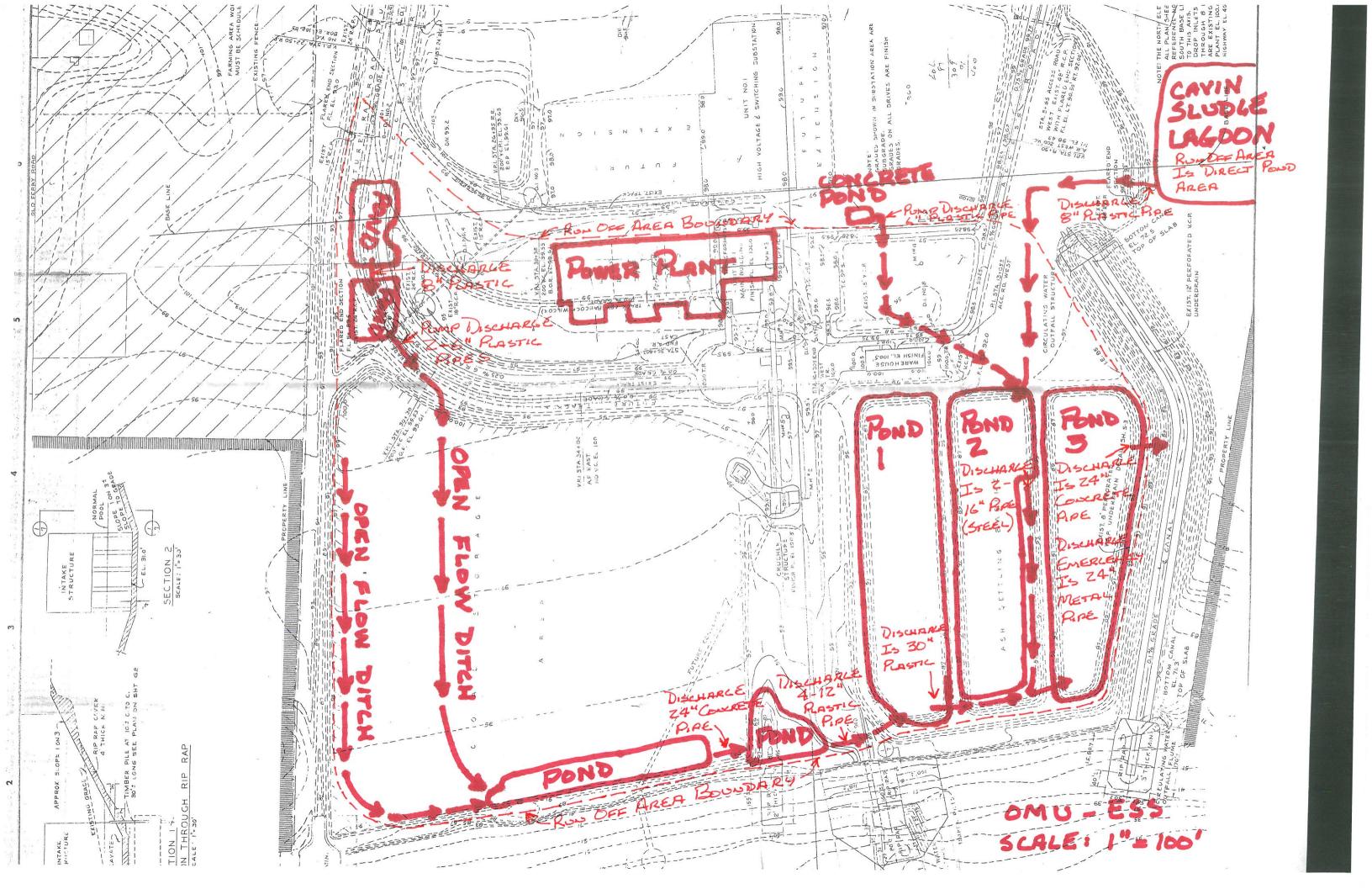
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- > <Flow Diagram questions.pdf>
- > <Existing Conditions questions.pdf>



Imagery ©2016 Google, Map data ©2016 Google 200 ft

# sqeM <mark>91000</mark>





**Photograph 1:** Ash Pond 1 – View Reference North (True North West)



Photograph 2:

Ash Pond 1 – View Reference South (True South East)



Owensboro Municipal Utilities Elmer Smith Station Ash Pond CEC Project: 164-014

Photographs provided by Owensboro Municipal Utilities



Photograph 3: Ash Pond 2



Photograph 4:

Ash Pond 3



Owensboro Municipal Utilities Elmer Smith Station Ash Pond CEC Project: 164-014

Photographs provided by Owensboro Municipal Utilities



Photograph 5:

Ash Pond 1, 2, and 3 – Sign



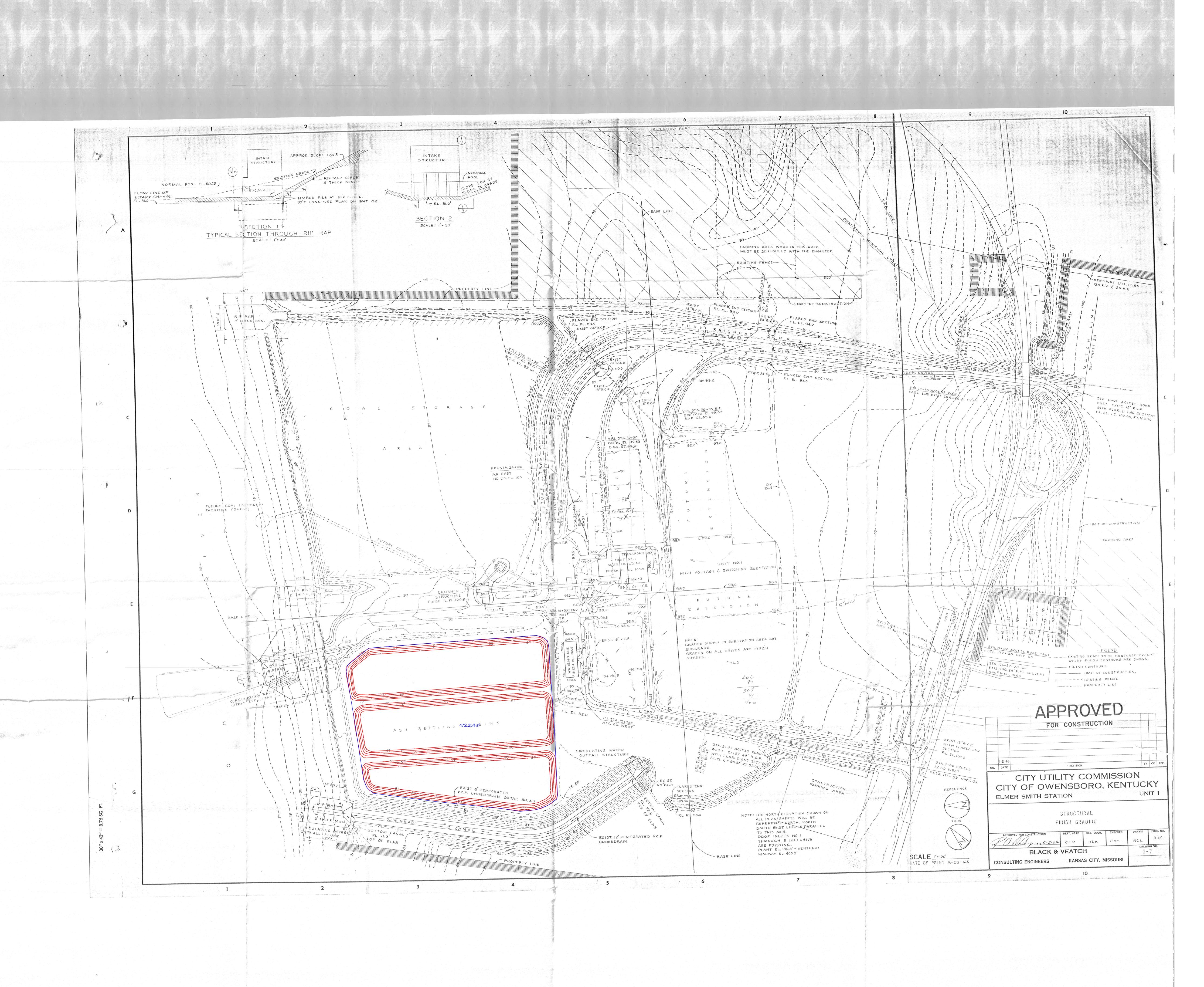
Phone: 412-429-2324

**Owensboro Municipal Utilities Elmer Smith Station Ash Pond** CEC Project: 164-014

Photographs provided by Owensboro Municipal Utilities

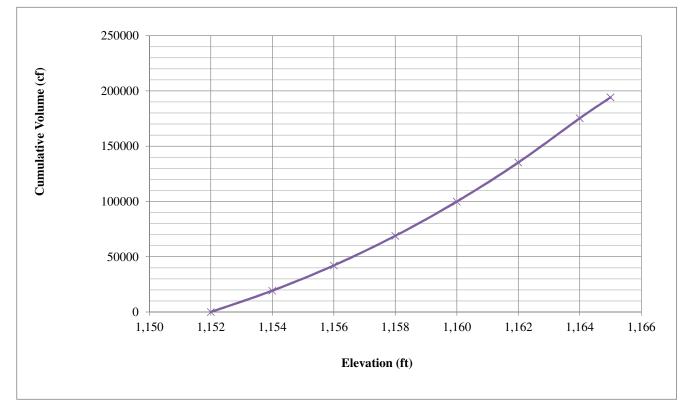
# ATTACHMENT 4

# STAGE STORAGE CURVES FOR MAXIMUM POND FOOTPRINTS



# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 1 - Maximum Available Capacity

Elevation (ft)	Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	110,823	0	0	0	0.0
89.00	121,712	116,268	232,535	232,535	5.3
91.00	132,375	127,044	254,087	486,622	11.2
93.00	143,325	137,850	275,700	762,322	17.5
95.00	154,200	148,763	297,525	1,059,847	24.3

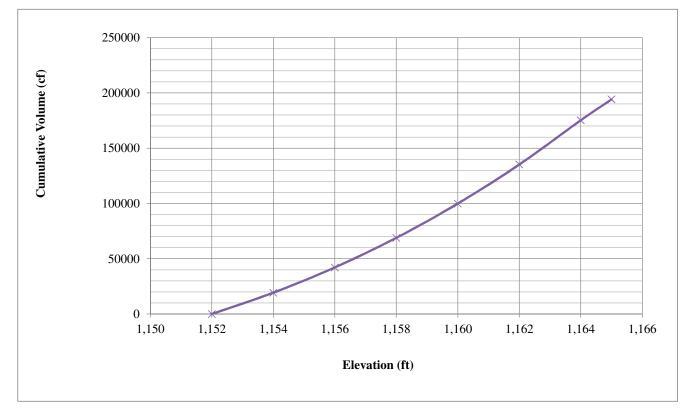


### **Pond Capacity Above Pool**

		Average	Incremental	Cumulative	Cumulative
Elevation	Area	Area	Volume	Volume	<b>Volume above Pool</b>
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)
89.00	121,712	0	0	0	0.0
91.00	132,375	127,044	254,087	254,087	5.8
93.00	143,325	137,850	275,700	529,787	12.2
95.00	154,200	148,763	297,525	827,312	19.0

# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 2 - Maximum Available Capacity

Elevation (ft)	Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	114,037	0	0	0	0.0
89.00	124,376	119,207	238,413	238,413	5.5
91.00	135,056	129,716	259,432	497,845	11.4
93.00	145,369	140,213	280,425	778,270	17.9
95.00	156,745	151,057	302,114	1,080,384	24.8

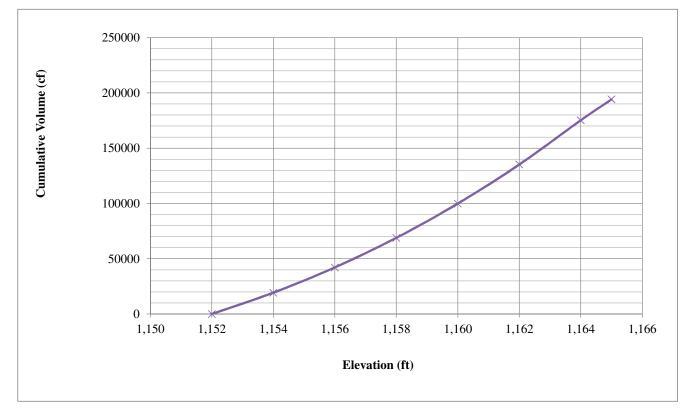


### **Pond Capacity Above Pool**

		Average	Incremental	Cumulative	Cumulative
Elevation	Area	Area	Volume	Volume	<b>7</b> olume above Pool
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)
89.00	124,376	0	0	0	0.0
91.00	135,056	129,716	259,432	259,432	6.0
93.00	145,369	140,213	280,425	539,857	12.4
95.00	156,745	151,057	302,114	841,971	19.3

# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 3 - Maximum Available Capacity

Elevation (ft)	Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	89,885	0	0	0	0.0
89.00	100,460	95,173	190,345	190,345	4.4
91.00	100,228	100,344	200,688	391,033	9.0
93.00	120,231	110,230	220,459	611,492	14.0
95.00	130,317	125,274	250,548	862,040	19.8

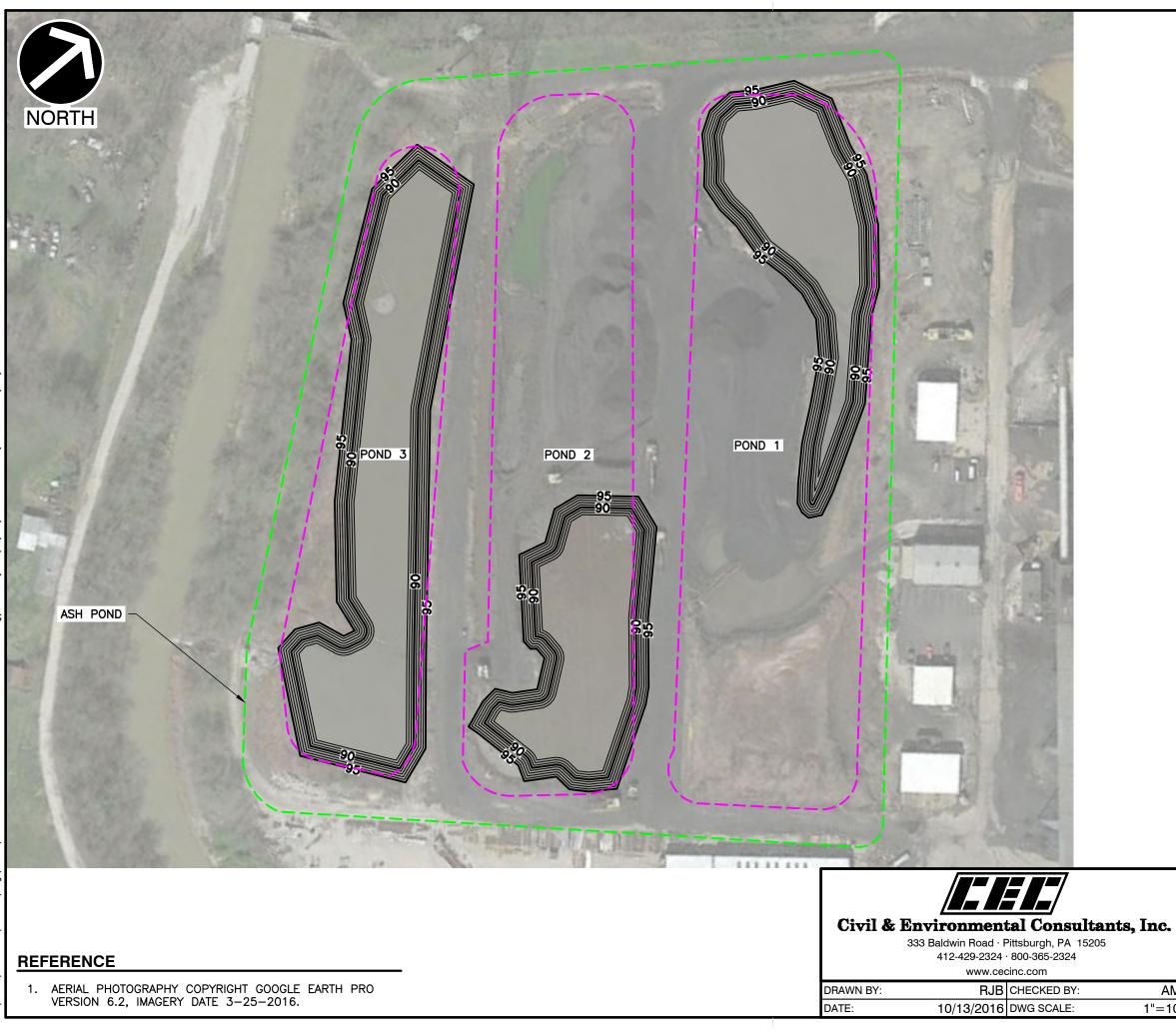


### **Pond Capacity Above Pool**

		Average	Incremental	Cumulative	Cumulative
Elevation	Area	Area	Volume	Volume	<b>7</b> olume above Pool
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)
89.00	100,460	0	0	0	0.0
91.00	100,228	100,344	200,688	200,688	4.6
93.00	120,231	110,230	220,459	421,147	9.7
95.00	130,317	125,274	250,548	671,695	15.4

# **ATTACHMENT 5**

# STAGE STORAGE CURVES FOR EXISTING POND FOOTPRINTS



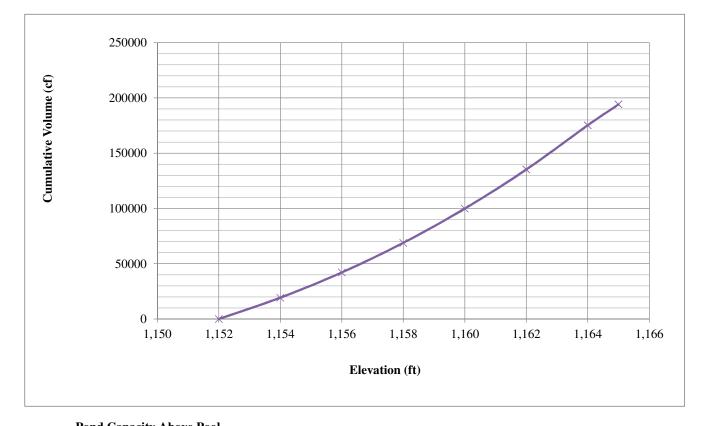
EGEND
ASH POND LIMITS
APPROXIMATE FOOTPRINT OF PONDS 1, 2, AND 3 (SEE NOTE 1)
90 ESTIMATED EXISTING POND CAPACITY CONTOUR (SEE NOTE 2)

# NOTES

	1. THE APPROXIMATE FOOTPRINT OF PONDS 1, 2, AND 3 IS BASED ON DRAWING NO. S–7 " STRUCTURAL FILL FINISH GRADING" PREPARED BY BLACK AND VEACH, DATED 8–28–62 AND THE AERIAL PHOTOGRAPHY (SEE REFERENCE 1).
	<ol> <li>THE ESTIMATED EXISTING POND CAPACITY IS BASED ON THE SURFACE AREA OF THE EXISTING POOL FROM THE AERIAL PHOTOGRAPHY, APPROXIMATE SIDE SLOPES OF 2.5H:1V, AND AN ASSUMED DEPTH OF 8-FT.</li> </ol>
	SCALE IN FEET
Inc.	OWENSBORO MUNICIPAL UTILITIES ELMER SMITH STATION OWENSBORO, KENTUCKY
	ESTIMATED EXISTING POND CAPACITY
	APPROVED BY: RJB FIGURE NO.:
1"=100'	PROJECT NO: 164-014.0003 4

# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 1 - Estimated Existing Capacity

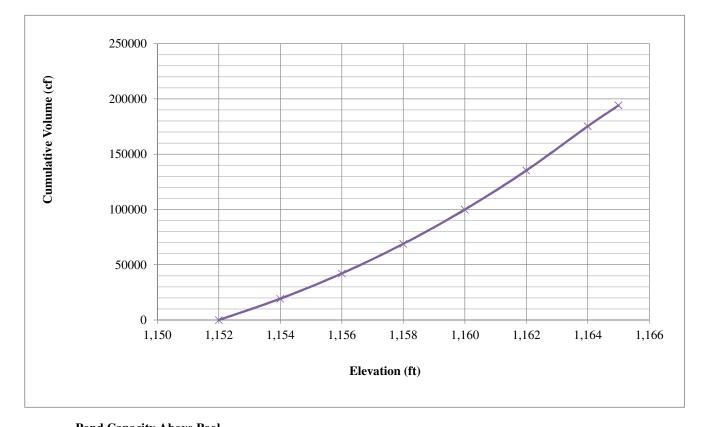
Elevation (ft)	Pool Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	21,286	0	0	0	0.0
89.00	26,050	23,668	47,336	47,336	1.1
91.00	31,061	28,556	57,111	104,447	2.4
93.00	36,237	33,649	67,298	171,745	3.9
95.00	41,576	38,907	77,813	249,558	5.7



ond Capacity Above Pool								
Pool	Average	Incremental	Cumulative	Cumulative				
Area	Area	Volume	Volume	<b>7</b> olume above Pool				
( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)				
26,050	0	0	0	0.0				
31,061	28,556	57,111	57,111	1.3				
36,237	33,649	67,298	124,409	2.9				
41,576	38,907	77,813	202,222	4.6				
	Pool Area (sf) 26,050 31,061 36,237	Pool         Average           Area         Area           (sf)         (sf)           26,050         0           31,061         28,556           36,237         33,649	Pool         Average         Incremental           Area         Area         Volume           (sf)         (sf)         (cf)           26,050         0         0           31,061         28,556         57,111           36,237         33,649         67,298	Pool         Average         Incremental         Cumulative           Area         Area         Volume         Volume           (sf)         (sf)         (cf)         (cf)           26,050         0         0         0           31,061         28,556         57,111         57,111           36,237         33,649         67,298         124,409				

# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 2 - Estimated Existing Capacity

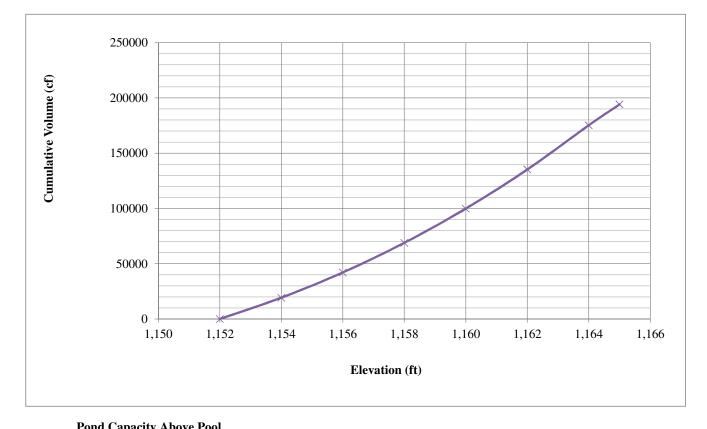
Elevation (ft)	Pool Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	22,225	0	0	0	0.0
89.00	26,085	24,155	48,310	48,310	1.1
91.00	30,139	28,112	56,224	104,535	2.4
93.00	34,382	32,261	64,521	169,056	3.9
95.00	38,815	36,599	73,197	242,253	5.6



ond Capacity Above Pool								
	Pool	Average	Incremental	Cumulative	Cumulative			
Elevation	Area	Area	Volume	Volume	<b>Volume above Pool</b>			
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)			
89.00	26,085	0	0	0	0.0			
91.00	30,139	28,112	56,224	56,224	1.3			
93.00	34,382	32,261	64,521	120,745	2.8			
95.00	38,815	36,599	73,197	193,942	4.5			

# Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 3 - Estimated Existing Capacity

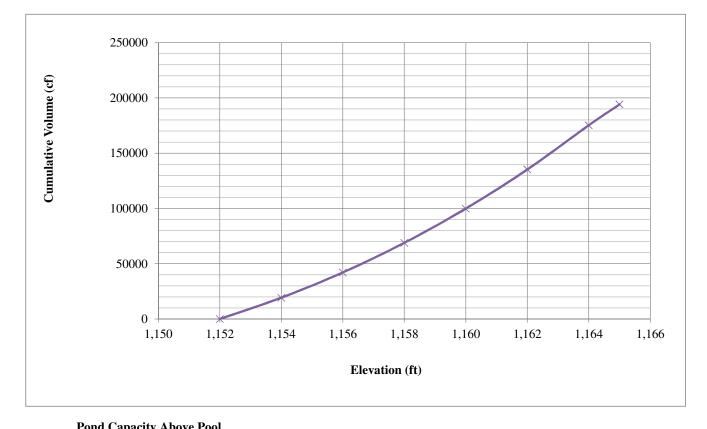
Elevation (ft)	Pool Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	38,391	0	0	0	0.0
89.00	45,585	41,988	83,976	83,976	1.9
91.00	52,960	49,273	98,545	182,521	4.2
93.00	60,515	56,738	113,475	295,996	6.8
95.00	68,252	64,384	128,767	424,763	9.8



ond Capacity Above Pool							
	Pool	Average	Incremental	Cumulative	Cumulative		
Elevation	Area	Area	Volume	Volume	<b>7</b> olume above Pool		
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)		
89.00	45,585	0	0	0	0.0		
91.00	52,960	49,273	98,545	98,545	2.3		
93.00	60,515	56,738	113,475	212,020	4.9		
95.00	68,252	64,384	128,767	340,787	7.8		

## Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Pond 1 - Estimated Required Capacity

Elevation (ft)	Pool Area (sf)	Average Area (sf)	Incremental Volume (cf)	Cumulative Volume (cf)	Cumulative Volume (ac-ft)
87.00	42,572	0	0	0	0.0
89.00	52,100	47,336	94,672	94,672	2.2
91.00	62,122	57,111	114,222	208,894	4.8
93.00	72,474	67,298	134,596	343,490	7.9
95.00	83,152	77,813	155,626	499,116	11.5



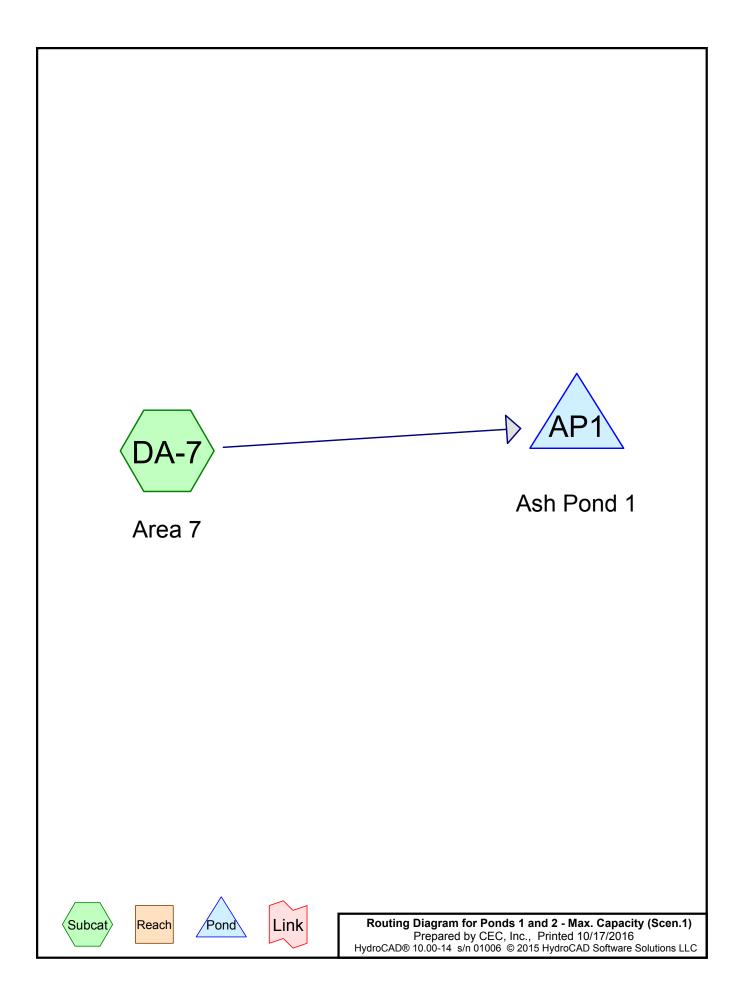
	Pool	Average	Incremental	Cumulative	Cumulative
Elevation	Area	Area	Volume	Volume	/olume above Pool
( <b>ft</b> )	( <b>sf</b> )	( <b>sf</b> )	( <b>cf</b> )	( <b>cf</b> )	(ac-ft)
89.00	52,100	0	0	0	0.0
91.00	62,122	57,111	114,222	114,222	2.6
93.00	72,474	67,298	134,596	248,818	5.7
95.00	83,152	77,813	155,626	404,444	9.3

# ATTACHMENT 6

# HYDROCAD ANALYSES

# PRELIMINARY EVALUATION (MAXIMUM POND FOOTPRINT)

POND 1, SCENARIO 1



Ponds 1 and 2 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

# Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
9.770	82	Dirt roads, HSG B (DA-7)
3.920	86	Fallow, bare soil, HSG B (DA-7)
3.920	98	Unconnected roofs, HSG B (DA-7)
1.980	98	Water Surface, HSG B (DA-7)
19.590	88	TOTAL AREA

# Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
19.590	HSG B	DA-7
0.000	HSG C	
0.000	HSG D	
0.000	Other	
19.590		TOTAL AREA

Ponds 1 and 2 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	9.770	0.000	0.000	0.000	9.770	Dirt roads	DA-7
0.000	3.920	0.000	0.000	0.000	3.920	Fallow, bare soil	DA-7
0.000	3.920	0.000	0.000	0.000	3.920	Unconnected roofs	DA-7
0.000	1.980	0.000	0.000	0.000	1.980	Water Surface	DA-7
0.000	19.590	0.000	0.000	0.000	19.590	TOTAL AREA	

## Ground Covers (selected nodes)

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentDA-7: Area 7 Runoff Area=19.590 ac 30.12% Impervious Runoff Depth=4.31" Flow Length=1,335' Slope=0.0100 '/' Tc=14.4 min CN=88 Runoff=107.47 cfs 7.034 af

Pond AP1: Ash Pond 1

Peak Elev=91.82' Storage=13.772 af Inflow=108.05 cfs 8.472 af Outflow=0.00 cfs 0.000 af

Total Runoff Area = 19.590 ac Runoff Volume = 7.034 af Average Runoff Depth = 4.31" 69.88% Pervious = 13.690 ac 30.12% Impervious = 5.900 ac

#### Summary for Subcatchment DA-7: Area 7

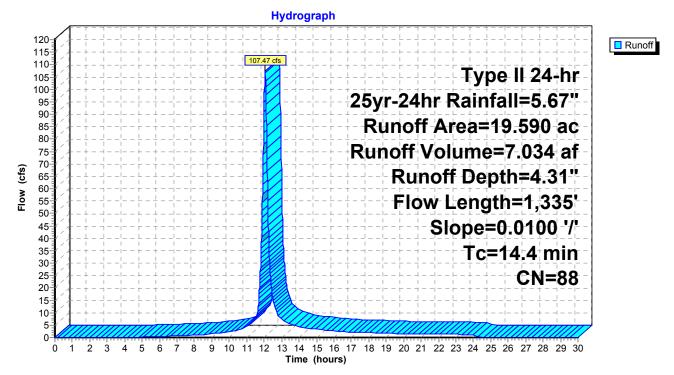
Runoff = 107.47 cfs @ 12.06 hrs, Volume= 7.034 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN	Desc	cription		
	1.	980	98	Wate	er Surface	, HSG B	
	3.	920	86	Fallo	w, bare so	oil, HSG B	
	3.	920	98	Unco	onnected r	oofs, HSG	В
_	9.	770	82	Dirt ı	roads, HS	GВ	
	19.	590	88	Weig	ghted Aver	age	
	13.	690		69.8	8% Pervio	us Area	
	5.	900		30.1	2% Imperv	ious Area	
	3.	920		66.4	4% Uncon	nected	
	_						
	Тс	Length		lope	Velocity	Capacity	Description
_	(min)	(feet)	) (1	ft/ft)	(ft/sec)	(cfs)	
	1.6	100	0.0	100	1.05		Sheet Flow,
							Smooth surfaces n= 0.011 P2= 3.26"
	12.8	1,235	0.0	100	1.61		Shallow Concentrated Flow,
_							Unpaved Kv= 16.1 fps
		4 005	· • •	L _ I			

14.4 1,335 Total

## Subcatchment DA-7: Area 7



## Summary for Pond AP1: Ash Pond 1

Inflow Are	a =	19.590 ac, 3	0.12% Impervious, Inf	low Depth > 5.19" for 25yr-24hr event
Inflow	=	108.05 cfs @	12.06 hrs, Volume=	8.472 af, Incl. 0.58 cfs Base Flow
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 100%, Lag= 0.0 min
Pouting by		Stor-Ind method	1 Time Span= 0.00-30	0.0  brs dt = 0.01  brs / 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs / 3 Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 5.300 af Peak Elev= 91.82' @ 30.00 hrs Surf.Area= 0.000 ac Storage= 13.772 af (8.472 af above start)

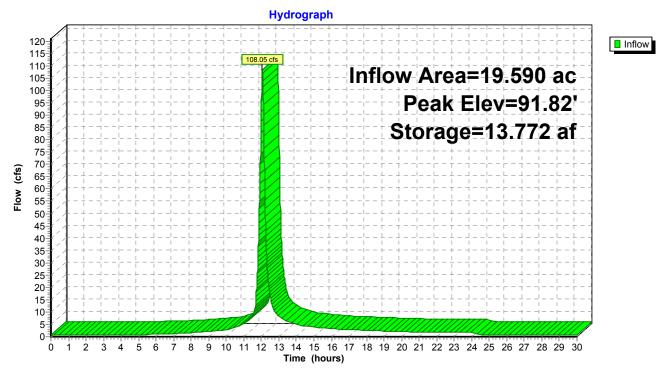
Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

95.00

24.300

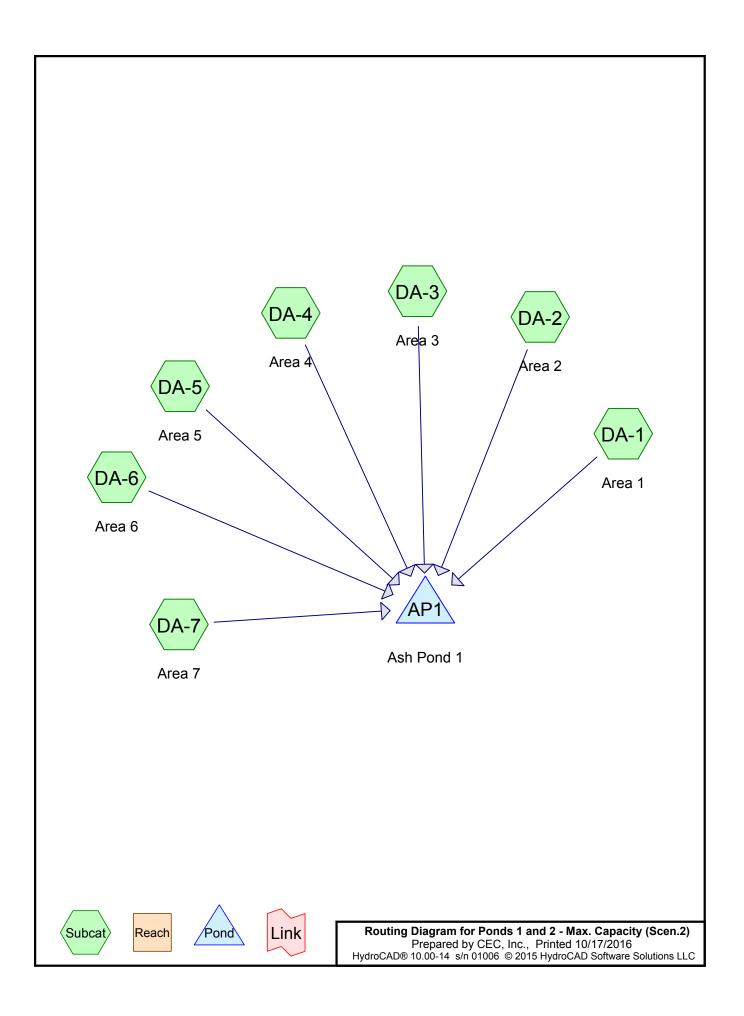
Volume	Invert	Avail.Storage	Storage Description
#1	87.00'	24.300 af	Custom Stage DataListed below
Elevation (feet)	Cum.St (acre-fe		
87.00	0.	000	
89.00	5.	300	
91.00	11.	200	
93.00	17.	500	

## Pond AP1: Ash Pond 1



# PRELIMINARY EVALUATION (MAXIMUM POND FOOTPRINT)

POND 1, SCENARIO 2



## Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
13.360	82	Dirt roads, HSG B (DA-1, DA-2, DA-4, DA-7)
19.320	86	Fallow, bare soil, HSG B (DA-3, DA-4, DA-5, DA-6, DA-7)
4.290	98	Unconnected roofs, HSG B (DA-4, DA-7)
4.620	98	Water Surface, HSG B (DA-1, DA-2, DA-5, DA-6, DA-7)
41.590	87	TOTAL AREA

# Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
41.590	HSG B	DA-1, DA-2, DA-3, DA-4, DA-5, DA-6, DA-7
0.000	HSG C	
0.000	HSG D	
0.000	Other	
41.590		TOTAL AREA

Ponds 1 and 2 - Max. Capacity (Scen.2) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

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-	HSG-A acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
	0.000	13.360	0.000	0.000	0.000	13.360	Dirt roads	DA-1, DA-2, DA-4, DA-7
	0.000	19.320	0.000	0.000	0.000	19.320	Fallow, bare soil	DA-3, DA-4, DA-5, DA-6, DA-7
	0.000	4.290	0.000	0.000	0.000	4.290	Unconnected roofs	DA-4, DA-7
	0.000	4.620	0.000	0.000	0.000	4.620	Water Surface	DA-1, DA-2, DA-5, DA-6, DA-7
	0.000	41.590	0.000	0.000	0.000	41.590	TOTAL AREA	

## Ground Covers (selected nodes)

Ponds 1 and 2 - Max. Capacity (Scen.2) Type II 24-hr 25yr-24hr Rainfall=5.67" Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentDA-1: Are	<b>ea 1</b> Flow Length=210'	Runoff Area=1. Slope=0.0100 '/'				
SubcatchmentDA-2: Are	ea 2 Flow Length=65	Runoff Area=1. 5' Slope=0.3300 '/		•	•	
SubcatchmentDA-3: Are	ea 3 Flow Length=210'		2.550 ac 0.00 Tc=2.7 min (			
SubcatchmentDA-4: Ar	ea 4 Flow Length=590'		9.250 ac 4.00 Tc=6.7 min (			
SubcatchmentDA-5: Ar		Runoff Area=4. Flow Length=400'		•	•	
SubcatchmentDA-6: Ar		Runoff Area=2. Flow Length=510'		•	•	
SubcatchmentDA-7: Ar Flo		Runoff Area=19. Slope=0.0100 '/' T		•	•	
Pond AP1: Ash Pond 1		Peak Elev=94.11'	Storage=21.2		230.02 cfs 15. ow=0.00 cfs 0	
Total Dun	off Area - 44 500	an Dunoff Valu			Dunoff Dont	h = 4.95

Total Runoff Area = 41.590 ac Runoff Volume = 14.739 af Average Runoff Depth = 4.25" 78.58% Pervious = 32.680 ac 21.42% Impervious = 8.910 ac

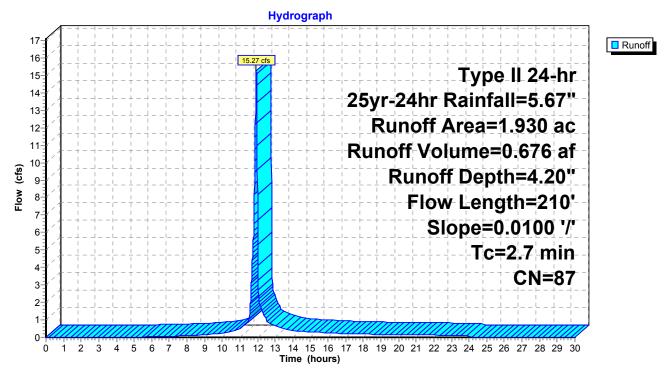
#### Summary for Subcatchment DA-1: Area 1

Runoff = 15.27 cfs @ 11.93 hrs, Volume= 0.676 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) C	N Des	cription		
	1.	270 8	32 Dirt	roads, HS	GВ	
	0.	<u>660</u>	98 Wat	er Surface	, HSG B	
	1.	930 8	37 Weig	ghted Aver	age	
	1.	270	65.8	0% Pervio	us Area	
	0.	660	34.2	0% Imperv	ious Area	
	Тс	Length	Slope	Velocity	Capacity	Description
(	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.6	100	0.0100	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
	1.1	110	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	2.7	210	Total			

#### Subcatchment DA-1: Area 1



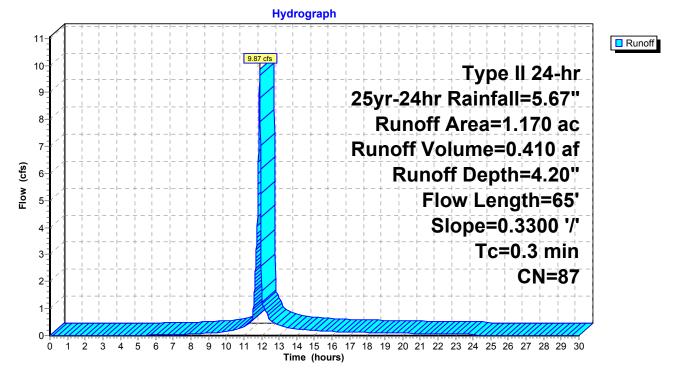
#### Summary for Subcatchment DA-2: Area 2

Runoff = 9.87 cfs @ 11.90 hrs, Volume= 0.410 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac)	CN	Desc	cription					
0	.840	82	Dirt r	oads, HSC	ЭB				
0	.330	98	Wate	er Surface,	, HSG B				
1	.170	87	Weig	hted Aver	age				
0	.840		71.7	9% Pervio	us Area				
0.330 28.21% Impervious Area					ious Area				
Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
0.3	6	5 0.	.3300	3.91		Sheet Flow, Smooth surfaces	n= 0.011	P2= 3.26"	





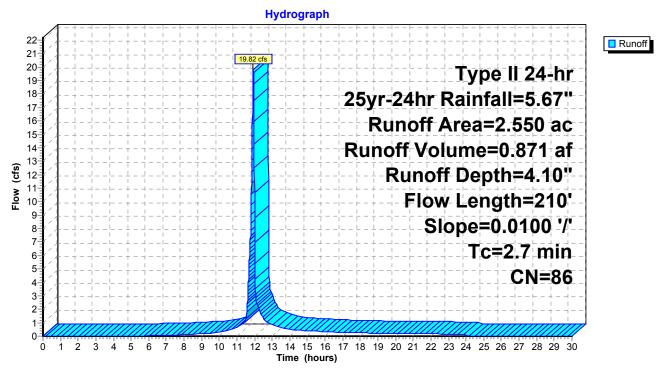
#### Summary for Subcatchment DA-3: Area 3

Runoff = 19.82 cfs @ 11.93 hrs, Volume= 0.871 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) C	N Des	cription		
	2.	550 8	6 Fallo	ow, bare so	oil, HSG B	
-	2.	550	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	1.6	100	0.0100	1.05		Sheet Flow,
	1.1	110	0.0100	1.61		Smooth surfaces n= 0.011 P2= 3.26" <b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
-	2.7	210	Total			

## Subcatchment DA-3: Area 3



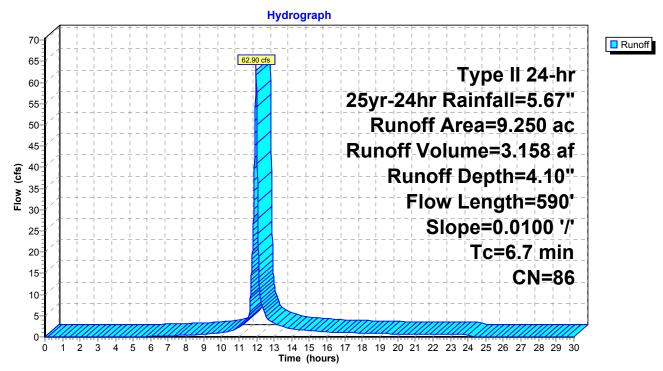
#### Summary for Subcatchment DA-4: Area 4

Runoff = 62.90 cfs @ 11.98 hrs, Volume= 3.158 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN I	Desc	ription		
1.480 82 Dirt roads, HSG B						GΒ	
	7.	400	86 F	Fallo	w, bare so	oil, HSG B	
	0.	370	98 l	Unco	onnected r	oofs, HSG	В
	9.	250	86 \	Weig	hted Aver	age	
	8.	880	ç	96.00	0% Pervio	us Area	
	0.	370	4	4.00	% Impervi	ous Area	
	0.	370		100.0	00% Unco	nnected	
	Tc (min)	Length (feet)		ope t/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	1.6	100	0.01	100	1.05		Sheet Flow,
	5.1	490	0.01	100	1.61		Smooth surfaces n= 0.011 P2= 3.26" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	6.7	590	Tota	al			

## Subcatchment DA-4: Area 4



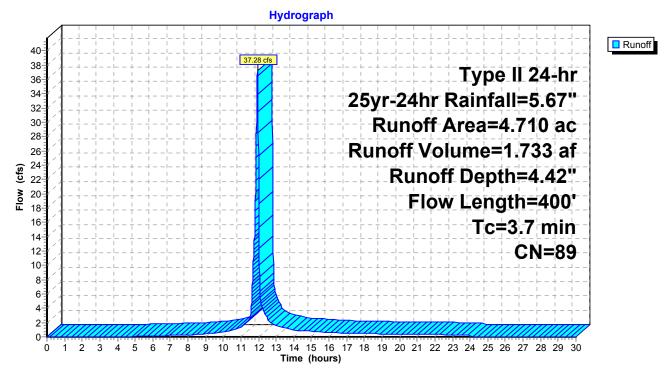
#### Summary for Subcatchment DA-5: Area 5

Runoff = 37.28 cfs @ 11.94 hrs, Volume= 1.733 af, Depth= 4.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) C	N Dese	cription		
3.380 86 Fallow, bare soil, HSG B						
_	1.	330 9	98 Wate	er Surface	, HSG B	
	4.	710 8	9 Weig	ghted Aver	age	
	3.	380	71.7	6% Pervio	us Area	
	1.	330	28.2	4% Imper	ious Area	
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.3	100	0.3300	1.27		Sheet Flow,
						Fallow n= 0.050 P2= 3.26"
	0.1	80	0.3300	9.25		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	2.3	220	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	3.7	400	Total			

## Subcatchment DA-5: Area 5



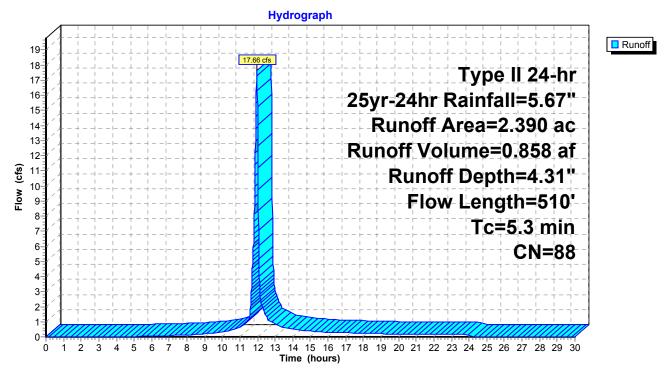
#### Summary for Subcatchment DA-6: Area 6

Runoff = 17.66 cfs @ 11.96 hrs, Volume= 0.858 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) C	N Desc	cription		
2.070 86 Fallow, bare soil, HSG B						
	0.	320 9	98 Wate	er Surface	, HSG B	
	2.	390 E	88 Weig	ghted Aver	age	
	2.	070	86.6	1% Pervio	us Area	
	0.	320	13.3	9% Imperv	vious Area	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.3	100	0.3300	1.27		Sheet Flow,
						Fallow n= 0.050 P2= 3.26"
	0.1	30	0.3300	9.25		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	3.9	380	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	5.3	510	Total			

## Subcatchment DA-6: Area 6



#### Summary for Subcatchment DA-7: Area 7

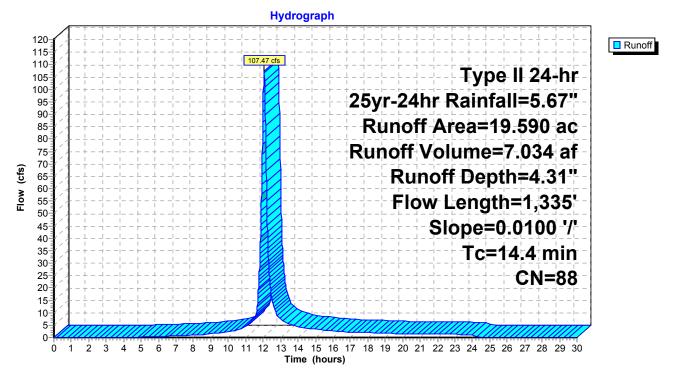
Runoff = 107.47 cfs @ 12.06 hrs, Volume= 7.034 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) (	CN D	esc	ription		
	1.	980	98 W	/ate	r Surface	, HSG B	
	3.	920	86 F	allo	w, bare so	oil, HSG B	
	3.	920	98 U	nco	nnected r	oofs, HSG	В
	9.	770	82 D	irt ro	oads, HS0	GВ	
	19.	590	88 W	/eig	hted Aver	age	
	13.	690	6	9.88	3% Pervio	us Area	
	5.	900	3	0.12	2% Imperv	vious Area	
	3.	920	6	6.44	I% Uncon	nected	
	Тс	Length	Slop	с	Velocity	Capacity	Description
_	(min)	(feet)	(ft/	ft)	(ft/sec)	(cfs)	
	1.6	100	0.010	00	1.05		Sheet Flow,
							Smooth surfaces n= 0.011 P2= 3.26"
	12.8	1,235	0.010	00	1.61		Shallow Concentrated Flow,
							Unpaved Kv= 16.1 fps
		4 005	<b>T</b> - 4 - 1	1			

14.4 1,335 Total

## Subcatchment DA-7: Area 7



## Summary for Pond AP1: Ash Pond 1

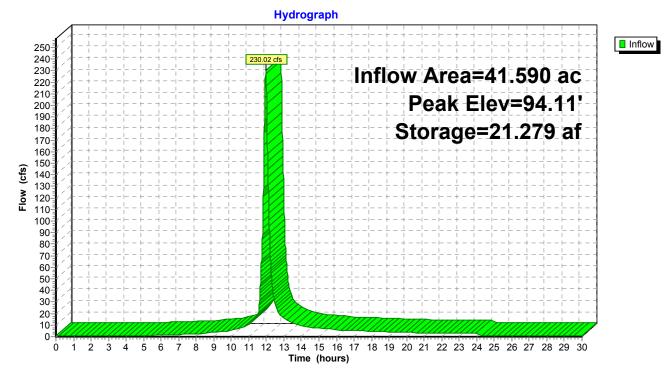
Inflow Area =41.590 ac, 21.42% Impervious, Inflow Depth > 4.61" for 25yr-24hr eventInflow =230.02 cfs @11.96 hrs, Volume=15.979 af, Incl. 0.50 cfs Base FlowOutflow =0.00 cfs @0.00 hrs, Volume=0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs / 3 Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 5.300 af Peak Elev= 94.11' @ 30.00 hrs Surf.Area= 0.000 ac Storage= 21.279 af (15.979 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

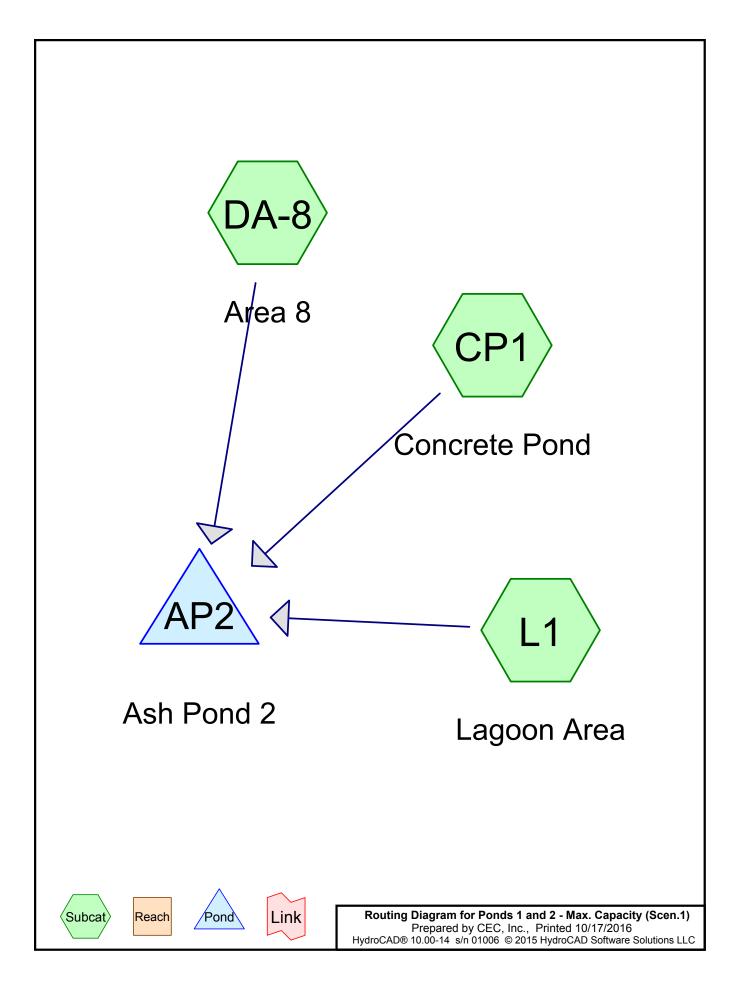
Volume	Invert	Avail.Storage	Storage Description
#1	87.00'	24.300 af	Custom Stage DataListed below
Elevation (feet)	Cum.S (acre-f		
87.00	0.	.000	
89.00	5.	.300	
91.00	11.	.200	
93.00	17.	.500	
95.00	24	.300	

## Pond AP1: Ash Pond 1



# PRELIMINARY EVALUATION (MAXIMUM POND FOOTPRINT)

POND 2



Ponds 1 and 2 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

## Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.410	79	<50% Grass cover, Poor, HSG B (DA-8)
1.280	82	Dirt roads, HSG B (DA-8)
0.950	86	Fallow, bare soil, HSG B (L1)
0.120	98	Unconnected roofs, HSG B (DA-8)
3.150	98	Water Surface, HSG B (CP1, DA-8, L1)
7.910	88	TOTAL AREA

# Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
7.910	HSG B	CP1, DA-8, L1
0.000	HSG C	
0.000	HSG D	
0.000	Other	
7.910		TOTAL AREA

Ponds 1 and 2 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

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 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 0.000	2.410	0.000	0.000	0.000	2.410	<50% Grass cover, Poor	DA-8
0.000	1.280	0.000	0.000	0.000	1.280	Dirt roads	DA-8
0.000	0.950	0.000	0.000	0.000	0.950	Fallow, bare soil	L1
0.000	0.120	0.000	0.000	0.000	0.120	Unconnected roofs	DA-8
0.000	3.150	0.000	0.000	0.000	3.150	Water Surface	CP1,
							DA-8, L1
0.000	7.910	0.000	0.000	0.000	7.910	TOTAL AREA	

## Ground Covers (selected nodes)

Ponds 1 and 2 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

 Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
 1	CP1	0.00	0.00	550.0	0.0200	0.010	6.0	0.0	0.0
2	L1	0.00	0.00	710.0	0.0200	0.010	8.0	0.0	0.0

# Pipe Listing (selected nodes)

Ponds 1 and 2 - Max. Capacity (Sce Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 Hydro			5yr-24hr Rainfall=5.67" Printed 10/17/2016 Page <u>6</u>
	0.00 hrs, dt=0.01 hrs -20 method, UH=SC method - Pond rou	S, Weighted-CN	Ind method
SubcatchmentCP1: Concrete Pond Flow Length=550'		•	ious Runoff Depth=5.43" Runoff=0.92 cfs 0.045 af
SubcatchmentDA-8: Area 8 Flow Length=475' S			ious Runoff Depth=4.20" Runoff=31.28 cfs 2.178 af
SubcatchmentL1: Lagoon Area Flow Length=710		•	ious Runoff Depth=4.63" Runoff=13.71 cfs 0.614 af
Pond AP2: Ash Pond 2	Peak Elev=90.50'	5	Inflow=33.68 cfs 4.425 af Outflow=0.00 cfs 0.000 af
Total Runoff Area = 7.910			rage Runoff Depth = 4.30" ŀ% Impervious = 3.270 ac

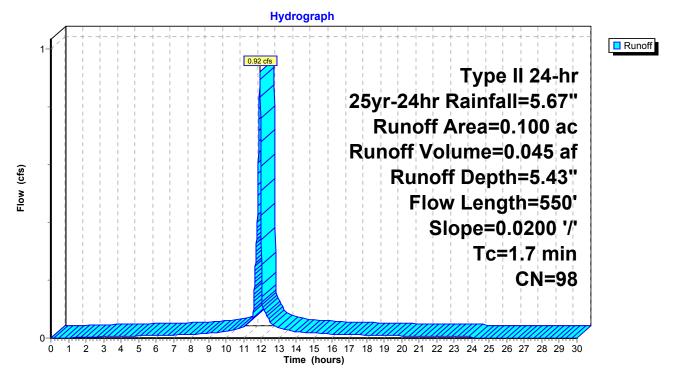
#### Summary for Subcatchment CP1: Concrete Pond

Runoff = 0.92 cfs @ 11.92 hrs, Volume= 0.045 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) C	N Des	cription				
_	0.	100 9	98 Wat	er Surface	, HSG B			
	0.100 100.00% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	1.7	550	0.0200	5.25	1.03	<b>Pipe Channel,</b> 6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13' n= 0.010 PVC, smooth interior		

#### Subcatchment CP1: Concrete Pond



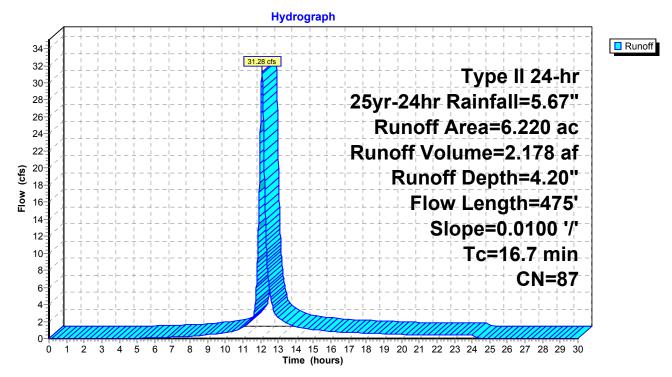
#### Summary for Subcatchment DA-8: Area 8

Runoff = 31.28 cfs @ 12.08 hrs, Volume= 2.178 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN I	Desc	cription			
2.	2.410 98			Water Surface, HSG B			
2.	410	79 •	<50%	% Grass co	over, Poor,	HSG B	
1.	280	82 I	Dirt ı	roads, HS	GΒ		
0.	120	98 l	Unco	onnected r	oofs, HSG	В	
6.	220	87 \	Weig	ghted Aver	age		
3.	690	Ę	59.3	2% Pervio	us Area		
2.	2.530			40.68% Impervious Area			
0.	0.120			4.74% Unconnected			
Тс	Length		эре	Velocity	Capacity	Description	
(min)	(feet)	) (fl	t/ft)	(ft/sec)	(cfs)		
12.8	100	0.01	100	0.13		Sheet Flow,	
						Grass: Short n= 0.150 P2= 3.26"	
3.9	375	0.01	100	1.61		Shallow Concentrated Flow,	
						Unpaved Kv= 16.1 fps	
16.7	475	o Tota	al				

#### Subcatchment DA-8: Area 8



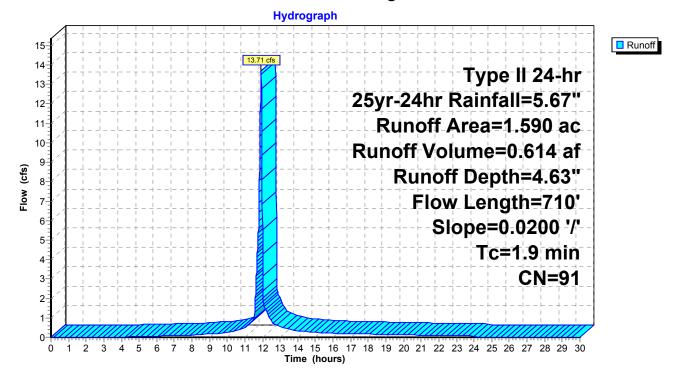
#### Summary for Subcatchment L1: Lagoon Area

Runoff = 13.71 cfs @ 11.92 hrs, Volume= 0.614 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	N Des	scription		
0.	640	98 Wa	ter Surface	, HSG B	
0.	950	86 Fal	ow, bare se	oil, HSG B	
1.	590	91 We	ighted Ave	rage	
0.	950	59.	75% Pervic	ous Area	
0.	640	40.	25% Imper	vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
1.9	710	0.0200	6.36	2.22	<b>Pipe Channel,</b> 8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17' n= 0.010 PVC, smooth interior

#### Subcatchment L1: Lagoon Area



## Summary for Pond AP2: Ash Pond 2

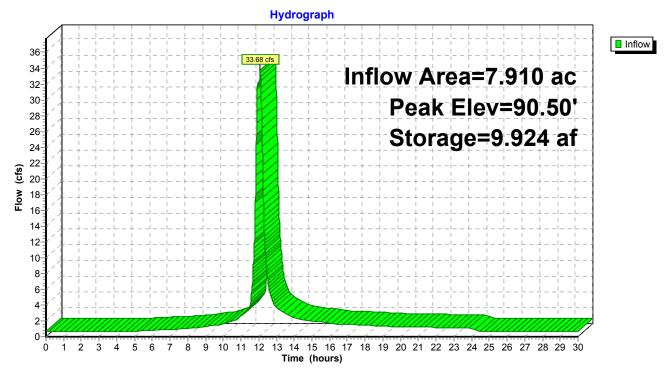
Inflow Area =	7.910 ac, 41.34% Impervi	ous, Inflow Depth > 6.71"	for 25yr-24hr event
Inflow =	33.68 cfs @ 12.08 hrs, Vo	lume= 4.425 af, Inc	I. 0.64 cfs Base Flow
Outflow =	0.00 cfs @ 0.00 hrs, Vo	lume= 0.000 af, Atte	en= 100%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs / 3 Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 5.500 af Peak Elev= 90.50' @ 30.00 hrs Surf.Area= 0.000 ac Storage= 9.924 af (4.424 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

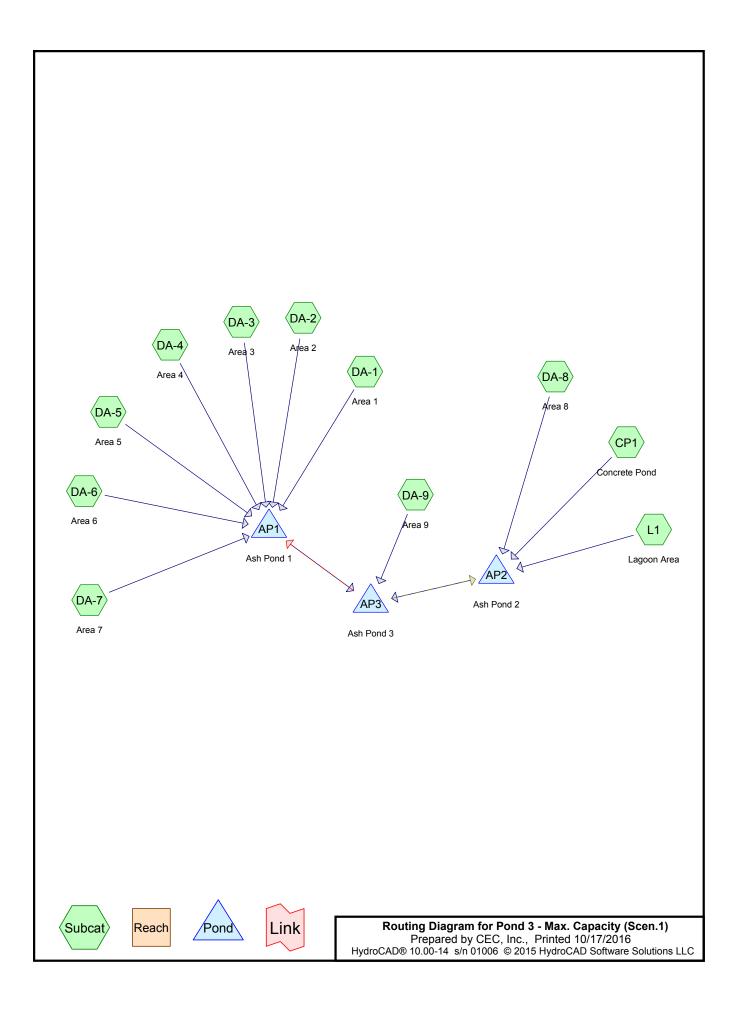
Volume	Invert	Avail.Storage	Storage Description
#1	87.00'	24.800 af	Custom Stage DataListed below
Elevation (feet)	Cum.S (acre-f		
87.00	0	.000	
89.00	5	.500	
91.00	11	.400	
93.00	17	.900	
95.00	24	.800	

## Pond AP2: Ash Pond 2



# PRELIMINARY EVALUATION (MAXIMUM POND FOOTPRINT)

POND 3



# Pond 3 - Max. Capacity (Scen.1)

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## Area Listing (selected nodes)

Ar	ea CN	Description	
(acre	es)	(subcatchment-numbers)	
2.4	10 79	<50% Grass cover, Poor, HSG B (DA-8)	
17.9	90 82	Dirt roads, HSG B (DA-1, DA-2, DA-4, DA-7, DA-8, DA-9)	
20.2	70 86	Fallow, bare soil, HSG B (DA-3, DA-4, DA-5, DA-6, DA-7, L1)	
4.4	10 98	Unconnected roofs, HSG B (DA-4, DA-7, DA-8)	
9.5	60 98	Water Surface, HSG B (CP1, DA-1, DA-2, DA-5, DA-6, DA-7, DA-8, DA-9, L1)	
54.6	40 87	TOTAL AREA	

# Pond 3 - Max. Capacity (Scen.1)

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# Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
54.640	HSG B	CP1, DA-1, DA-2, DA-3, DA-4, DA-5, DA-6, DA-7, DA-8, DA-9, L1
0.000	HSG C	
0.000	HSG D	
0.000	Other	
54.640		TOTAL AREA

Pond 3 - Max. Capacity (Scen.1) Prepared by CEC, Inc. HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

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HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
 0.000	2.410	0.000	0.000	0.000	2.410	<50% Grass cover, Poor	DA-8
0.000	17.990	0.000	0.000	0.000	17.990	Dirt roads	DA-1,
							DA-2,
							DA-4,
							DA-7,
							DA-8,
							DA-9
0.000	20.270	0.000	0.000	0.000	20.270	Fallow, bare soil	DA-3,
							DA-4,
							DA-5,
							DA-6,
							DA-7, L1
0.000	4.410	0.000	0.000	0.000	4.410	Unconnected roofs	DA-4,
							DA-7,
							DA-8
0.000	9.560	0.000	0.000	0.000	9.560	Water Surface	CP1,
							DA-1,
							DA-2,
							DA-5,
							DA-6,
							DA-7,
							DA-8,
							DA-9, L1
0.000	54.640	0.000	0.000	0.000	54.640	TOTAL AREA	

# Pond 3 - Max. Capacity (Scen.1)

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Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
 1	CP1	0.00	0.00	550.0	0.0200	0.010	6.0	0.0	0.0
2	L1	0.00	0.00	710.0	0.0200	0.010	8.0	0.0	0.0
3	AP1	89.00	88.00	280.0	0.0036	0.010	30.0	0.0	0.0
4	AP2	89.00	88.00	540.0	0.0019	0.025	16.0	0.0	0.0
5	AP3	88.00	87.00	100.0	0.0100	0.012	24.0	0.0	0.0
6	AP3	88.00	89.00	280.0	-0.0036	0.010	30.0	0.0	0.0
7	AP3	88.00	89.00	540.0	-0.0019	0.025	16.0	0.0	0.0
8	AP3	90.00	89.00	100.0	0.0100	0.025	24.0	0.0	0.0

# Pipe Listing (selected nodes)

Pond 3 - Max. Capacity (Scen.1)	Type II 24-hr	25yr-24hr Rainfall=5.67"
Prepared by CEC, Inc.		Printed 10/17/2016
HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutio	ns LLC	Page 6
		-

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Sim-Route method - Pond routing by Sim-Route method

SubcatchmentCP1: Concrete Pond Flow Length=550' Slope=0.0200 '/' Tc=1.7 min CN=98 Runoff=0.92 cfs 0.045 af
SubcatchmentDA-1: Area 1Runoff Area=1.930 ac34.20% ImperviousRunoff Depth=4.20"Flow Length=210'Slope=0.0100 '/'Tc=2.7 minCN=87Runoff=15.27 cfs0.676 af
SubcatchmentDA-2: Area 2Runoff Area=1.170 ac28.21% ImperviousRunoff Depth=4.20"Flow Length=65'Slope=0.3300 '/'Tc=0.3 minCN=87Runoff=9.87 cfs0.410 af
SubcatchmentDA-3: Area 3 Flow Length=210' Slope=0.0100 '/' Tc=2.7 min CN=86 Runoff=19.82 cfs 0.871 af
SubcatchmentDA-4: Area 4 Runoff Area=9.250 ac 4.00% Impervious Runoff Depth=4.10" Flow Length=590' Slope=0.0100 '/' Tc=6.7 min CN=86 Runoff=62.90 cfs 3.158 af
SubcatchmentDA-5: Area 5Runoff Area=4.710 ac28.24% ImperviousRunoff Depth=4.42"Flow Length=400'Tc=3.7 minCN=89Runoff=37.28 cfs1.733 af
SubcatchmentDA-6: Area 6Runoff Area=2.390 ac13.39% ImperviousRunoff Depth=4.31"Flow Length=510'Tc=5.3 minCN=88Runoff=17.66 cfs0.858 af
SubcatchmentDA-7: Area 7 Runoff Area=19.590 ac 30.12% Impervious Runoff Depth=4.31" Flow Length=1,335' Slope=0.0100 '/' Tc=14.4 min CN=88 Runoff=107.47 cfs 7.034 af
SubcatchmentDA-8: Area 8 Runoff Area=6.220 ac 40.68% Impervious Runoff Depth=4.20" Flow Length=475' Slope=0.0100 '/' Tc=16.7 min CN=87 Runoff=31.28 cfs 2.178 af
SubcatchmentDA-9: Area 9 Flow Length=435' Slope=0.0100 '/' Tc=5.1 min CN=88 Runoff=38.23 cfs 1.846 af
SubcatchmentL1: Lagoon Area Runoff Area=1.590 ac 40.25% Impervious Runoff Depth=4.63" Flow Length=710' Slope=0.0200 '/' Tc=1.9 min CN=91 Runoff=13.71 cfs 0.614 af
Pond AP1: Ash Pond 1         Peak Elev=91.86' Storage=13.913 af Inflow=230.02 cfs 15.979 af 30.0" Round Culvert n=0.010 L=280.0' S=0.0036 '/' Outflow=23.69 cfs 13.969 af
Pond AP2: Ash Pond 2         Peak Elev=90.14' Storage=8.854 af Inflow=33.68 cfs 4.569 af 16.0" Round Culvert x 2.00 n=0.025 L=540.0' S=0.0019 '/' Outflow=1.87 cfs 1.985 af
Pond AP3: Ash Pond 3         Peak Elev=90.11'         Storage=6.964 af         Inflow=52.32 cfs         17.796 af           Primary=16.01 cfs         17.754 af         Secondary=0.00 cfs         0.000 af         Tertiary=1.06 cfs         0.145 af         Outflow=17.00 cfs         17.898 af
Total Runoff Area = 54.640 ac Runoff Volume = 19.422 af Average Runoff Depth = 4.2

Total Runoff Area = 54.640 ac Runoff Volume = 19.422 af Average Runoff Depth = 4.27" 74.43% Pervious = 40.670 ac 25.57% Impervious = 13.970 ac

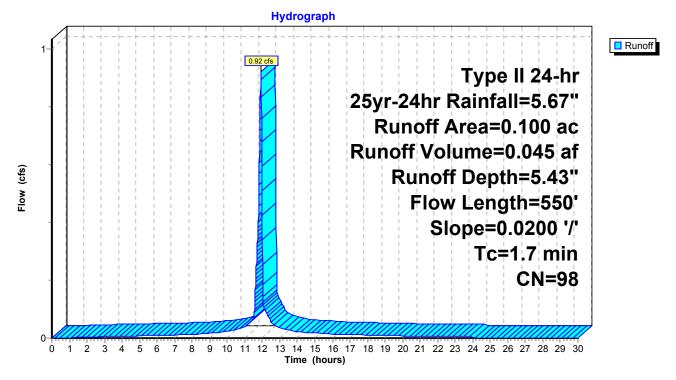
#### Summary for Subcatchment CP1: Concrete Pond

Runoff 0.92 cfs @ 11.92 hrs, Volume= 0.045 af, Depth= 5.43" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) C	N Des	cription				
_	0.	100 9	98 Wat	er Surface	, HSG B			
	0.100 100.00% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	1.7	550	0.0200	5.25	1.03	<b>Pipe Channel,</b> 6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13' n= 0.010 PVC, smooth interior		

#### Subcatchment CP1: Concrete Pond



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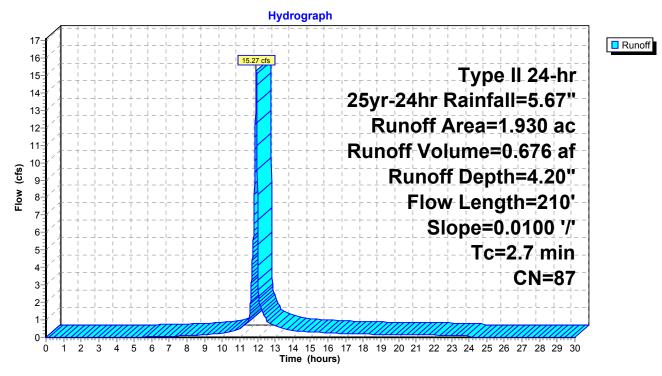
# Summary for Subcatchment DA-1: Area 1

Runoff = 15.27 cfs @ 11.93 hrs, Volume= 0.676 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	a (ac)	CN	Desc	cription		
	1.270	82	Dirt ı	roads, HS	ЭB	
(	0.660	98	Wate	er Surface	, HSG B	
	1.930	87	Weig	ghted Aver	age	
-	1.270		65.8	0% Pervio	us Area	
(	0.660		34.2	0% Imperv	ious Area	
Tc	Lengt	h S	Slope	Velocity	Capacity	Description
(min)	(feet	)	(ft/ft)	(ft/sec)	(cfs)	
1.6	10	0 0.	.0100	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
1.1	11	0 0.	.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
2.7	21	0 To	otal			

# Subcatchment DA-1: Area 1



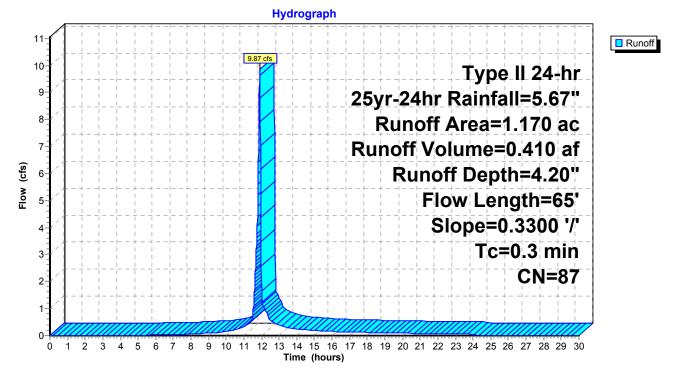
# Summary for Subcatchment DA-2: Area 2

Runoff = 9.87 cfs @ 11.90 hrs, Volume= 0.410 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac)	CN	Desc	cription					
0	.840	82	Dirt r	roads, HS0	GВ				
0	.330	98	Wate	er Surface,	, HSG B				
1	.170	87	Weig	ghted Aver	age				
0	.840		71.7	9% Pervio	us Area				
0	.330		28.2	1% Imperv	ious Area/				
Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
0.3	6	50	.3300	3.91		Sheet Flow, Smooth surfaces	n= 0.011	P2= 3.26"	





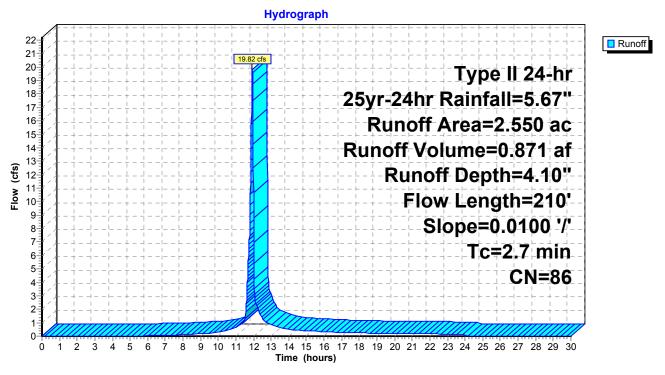
# Summary for Subcatchment DA-3: Area 3

Runoff = 19.82 cfs @ 11.93 hrs, Volume= 0.871 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) C	N Des	cription						
	2.550 86 Fallow, bare soil, HSG B									
	2.	550	100.	00% Pervi	ous Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
-	1.6	100	0.0100	1.05		Sheet Flow,				
	1.1	110	0.0100	1.61		Smooth surfaces n= 0.011 P2= 3.26" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
	2.7	210	Total							

# Subcatchment DA-3: Area 3



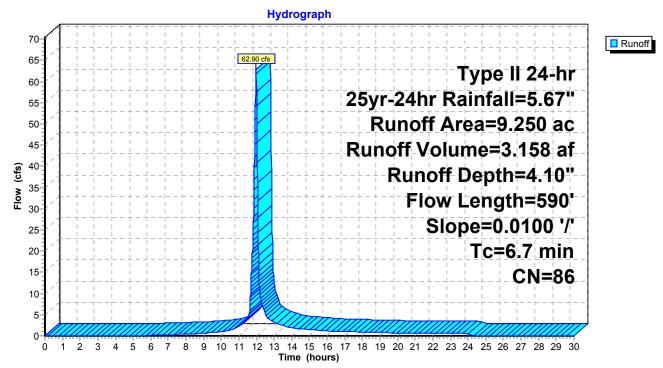
# Summary for Subcatchment DA-4: Area 4

Runoff = 62.90 cfs @ 11.98 hrs, Volume= 3.158 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac)	CN	Desc	cription						
	1.	480	82	Dirt r	rt roads, HSG B						
	7.	400	86	Fallo	w, bare so	oil, HSG B					
	0.	370	98	Unco	onnected r	oofs, HSG	В				
	9.	250	86	Weig	hted Aver	age					
	8.	880		96.0	0% Pervio	us Area					
	0.	370		4.00	% Impervi	ous Area					
	0.	370		100.0	00% Unco	nnected					
	Tc (min)	Length (feet)		lope ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
_	1.6	100	0.0	)100	1.05		Sheet Flow,				
	5.1	490	0.0	)100	1.61		Smooth surfaces n= 0.011 P2= 3.26" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
	6.7	590	) Tot	tal							

# Subcatchment DA-4: Area 4



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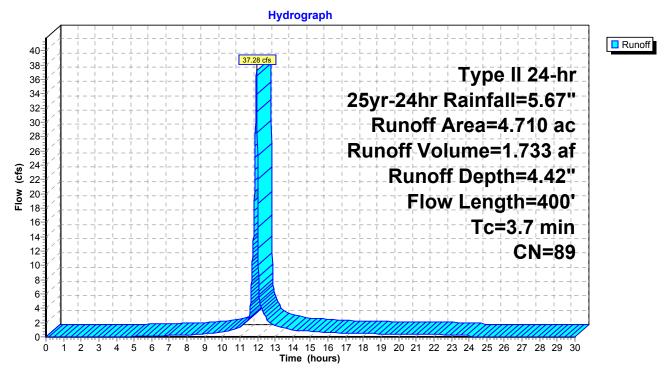
# Summary for Subcatchment DA-5: Area 5

Runoff = 37.28 cfs @ 11.94 hrs, Volume= 1.733 af, Depth= 4.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

A	rea	(ac) C	N Desc	cription		
3.380 86 Fallow, bare soil, HSG B				w, bare so	oil, HSG B	
	1.	330 9	98 Wate	er Surface	, HSG B	
	4.	710 8	9 Weig	ghted Aver	age	
	3.	380	71.7	6% Pervio	us Area	
	1.	330	28.2	4% Imper	vious Area	
	_					
	Тс	Length	Slope	Velocity	Capacity	Description
(m	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.3	100	0.3300	1.27		Sheet Flow,
						Fallow n= 0.050 P2= 3.26"
(	0.1	80	0.3300	9.25		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
:	2.3	220	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	3.7	400	Total			

# Subcatchment DA-5: Area 5



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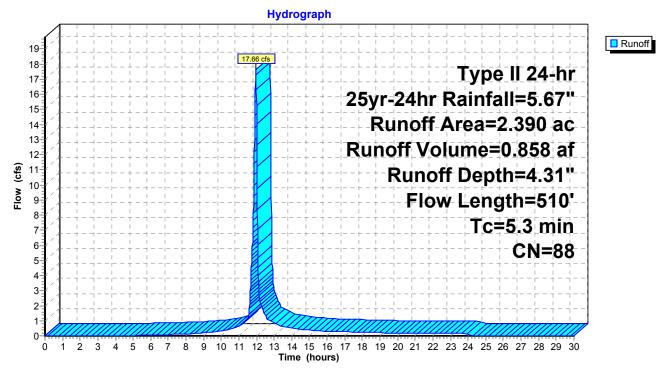
# Summary for Subcatchment DA-6: Area 6

Runoff = 17.66 cfs @ 11.96 hrs, Volume= 0.858 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) C	N Desc	cription		
2.070 86 Fallow, bare soil, HSG B						
	0.	320 9	98 Wate	er Surface	, HSG B	
	2.	390 E	88 Weig	ghted Aver	age	
	2.	070	86.6	1% Pervio	us Area	
	0.	320	13.3	9% Imperv	vious Area	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.3	100	0.3300	1.27		Sheet Flow,
						Fallow n= 0.050 P2= 3.26"
	0.1	30	0.3300	9.25		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	3.9	380	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	5.3	510	Total			

# Subcatchment DA-6: Area 6



### Summary for Subcatchment DA-7: Area 7

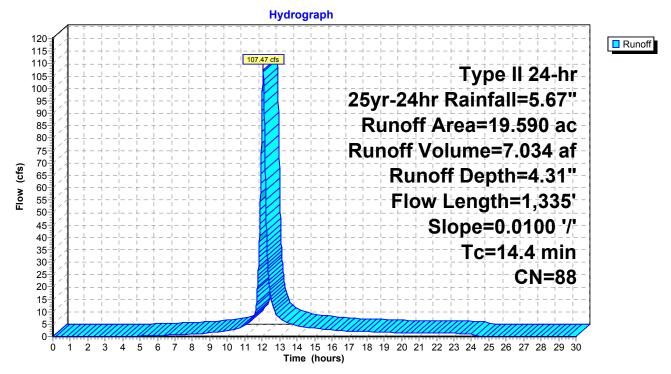
Runoff = 107.47 cfs @ 12.06 hrs, Volume= 7.034 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN De	escription		
	1.	980	98 W	ater Surfac	e, HSG B	
	3.	920	86 Fa	llow, bare	soil, HSG B	
	3.	920	98 Uı	nconnected	l roofs, HSG	В
	9.	770	82 Di	rt roads, H	SG B	
	19.	590	88 W	eighted Av	erage	
	13.	690	69	.88% Perv	ious Area	
	5.	900			rvious Area	
	3.	920	66	.44% Unco	onnected	
	-		0		0 "	
	Tc	Length		-		Description
_	(min)	(feet)	(ft/f	t) (ft/sec	) (cfs)	
	1.6	100	0.010	0 1.05	5	Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
	12.8	1,235	0.010	0 1.6 <sup>-</sup>		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	444	4 005	Tatal			

14.4 1,335 Total

# Subcatchment DA-7: Area 7



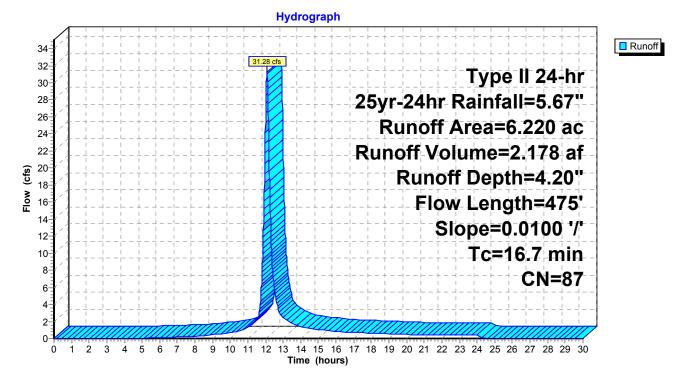
### Summary for Subcatchment DA-8: Area 8

Runoff = 31.28 cfs @ 12.08 hrs, Volume= 2.178 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN D	)esc	cription				
2.410 98 Water Surface, HSG B								
2.410 79 <50% Grass cover, Poor, HSG B								
1.280 82 Dirt roads, HSG B								
0.	120	98 U	Inco	onnected r	oofs, HSG	В		
6.	220	87 V	Veig	phted Aver	age			
3.	690	5	9.3	2% Pervio	us Area			
2.	530	4	0.6	8% Imperv	ious Area			
0.	120	4	.74	% Unconn	ected			
Тс	Length			Velocity	Capacity	Description		
(min)	(feet)	(ft/	′ft)	(ft/sec)	(cfs)			
12.8	100	0.01	00	0.13		Sheet Flow,		
						Grass: Short n= 0.150 P2= 3.26"		
3.9	375	0.01	00	1.61		Shallow Concentrated Flow,		
						Unpaved Kv= 16.1 fps		
16.7	475	Tota	I					

Subcatchment DA-8: Area 8



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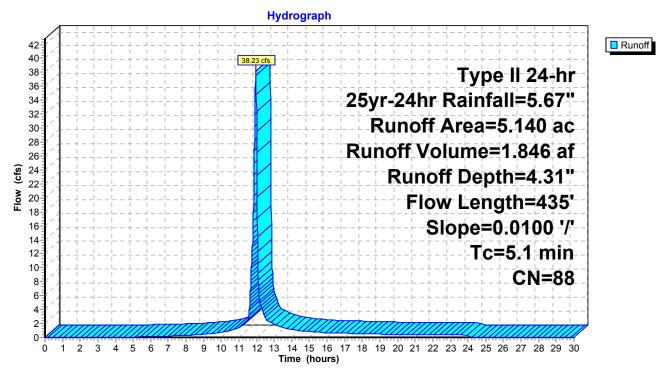
### Summary for Subcatchment DA-9: Area 9

Runoff = 38.23 cfs @ 11.96 hrs, Volume= 1.846 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Are	a (ac)	С	N Dese	cription		
1.790 98 Water Surface, HSG B						
	3.350	8	2 Dirt	roads, HS	ЭB	
	5.140	8	8 Weig	ghted Aver	age	
	3.350		65.1	8% Pervio	us Area	
	1.790		34.8	2% Imperv	vious Area	
Т	c Leng	gth	Slope	Velocity	Capacity	Description
(min	) (fe	et)	(ft/ft)	(ft/sec)	(cfs)	
1.6	51	00	0.0100	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
3.5	53	35	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
5.	1 4	35	Total			

# Subcatchment DA-9: Area 9



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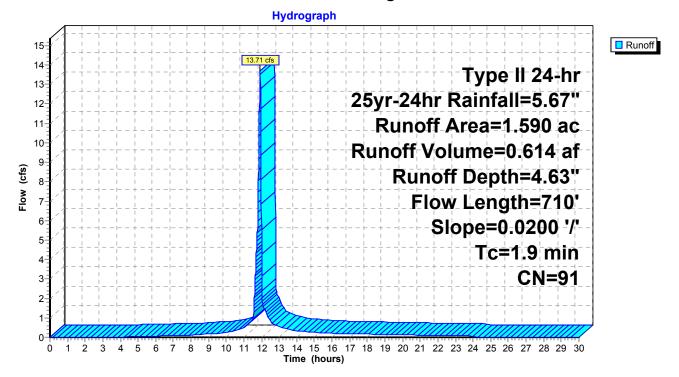
# Summary for Subcatchment L1: Lagoon Area

Runoff = 13.71 cfs @ 11.92 hrs, Volume= 0.614 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN De	scription		
0.	640	98 W	ater Surface	, HSG B	
0.	950	86 Fa	llow, bare s	oil, HSG B	
1.	590	91 W	eighted Ave	rage	
0.	950	59	.75% Pervic	ous Area	
0.	640	40	.25% Imper	vious Area	
Tc (min)	Length (feet)		,	Capacity (cfs)	Description
1.9	710	0.020	0 6.36	2.22	<b>Pipe Channel,</b> 8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17' n= 0.010 PVC, smooth interior

# Subcatchment L1: Lagoon Area



# Summary for Pond AP1: Ash Pond 1

Inflow Outflow Primary	= = =	23.69 c	fs @ 1	1.96 hrs, Volume=15.979 af, Incl. 0.50 cfs Base Flow2.59 hrs, Volume=13.969 af, Atten= 90%, Lag= 37.8 min2.59 hrs, Volume=13.969 af						
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 5.300 af Peak Elev= 91.86' @ 12.59 hrs Surf.Area= 0.000 ac Storage= 13.913 af (8.613 af above start)										
	Plug-Flow detention time= 521.6 min calculated for 8.669 af (54% of inflow) Center-of-Mass det. time= 231.6 min(1,034.7 - 803.1)									
Volume	1	nvert Av	ail.Stora	age Storage Description						
#1	8	7.00'	24.30	0 af Custom Stage DataListed below						
Elevatio		Cum.Stor	-							
(fee	/	(acre-feet	-							
87.0	-	0.00	-							
89.0 91.0	-	5.30 11.20								
91.0	-	17.50	-							
93.0 95.0		24.30								
95.0	0	24.50	J							
Device	Routir	ng	Invert	Outlet Devices						
#1	Prima	iry	89.00'	<b>30.0" Round Culvert</b> L= 280.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 89.00' / 88.00' S= 0.0036 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf						

Primary OutFlow Max=23.69 cfs @ 12.59 hrs HW=91.86' TW=89.36' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 23.69 cfs @ 4.83 fps)

### Pond 3 - Max. Capacity (Scen.1) Prepared by CEC, Inc.

Hydrograph Inflow Primary 230.02 cfs 240 Peak Elev=91.86' 220 Storage=13.913 af 200 30.0" 180 160 **Round Culvert** (**sj**) 140-**M**) 120n=0.010 L=280.0' 100-80-S=0.0036 '/' 60 40 23.69 cfs 20 0-6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ο i 2 3 4 5 Time (hours)

# Pond AP1: Ash Pond 1

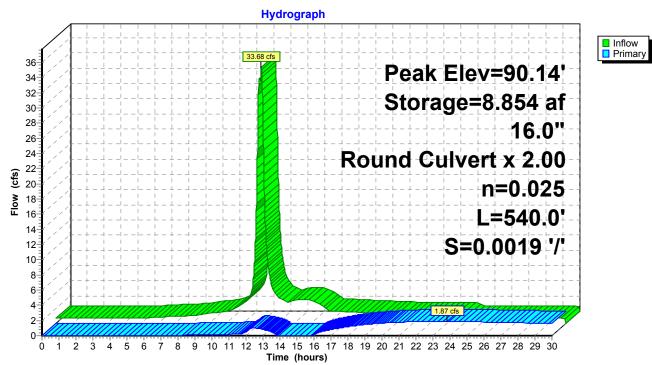
# Summary for Pond AP2: Ash Pond 2

Inflow Outflow Primary	= 1.8	7 cfs @ 2	12.08 hrs, Volume=4.569 af, Incl. 0.64 cfs Base Flow23.85 hrs, Volume=1.985 af, Atten= 94%, Lag= 705.9 min23.85 hrs, Volume=1.985 af						
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 5.500 af Peak Elev= 90.14' @ 18.64 hrs Surf.Area= 0.000 ac Storage= 8.854 af (3.354 af above start)									
Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 523.5 min ( 1,358.7 - 835.2 )									
Volume	Invert	Avail.Stora	age Storage Description						
#1	87.00'	24.80	0 af Custom Stage DataListed below						
Elevation (feet)	Cum.S (acre-fe								
87.00	0.	000							
89.00	-	500							
91.00	11.	400							
93.00	17.	900							
95.00	24.	800							
Device R	outing	Invert	Outlet Devices						
#1 P	rimary	89.00'	<b>16.0" Round Culvert X 2.00</b> L= 540.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 89.00' / 88.00' S= 0.0019 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.40 sf						
Primary O	<b>Primary OutElow</b> Max = 1.87 cfc @ 23.85 brc $HW/=00.06'$ TW/=80.36' (Dynamic Tailwater)								

Primary OutFlow Max=1.87 cfs @ 23.85 hrs HW=90.06' TW=89.36' (Dynamic Tailwater) ☐ 1=Culvert (Outlet Controls 1.87 cfs @ 1.07 fps)

# Pond 3 - Max. Capacity (Scen.1)

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# Pond AP2: Ash Pond 2

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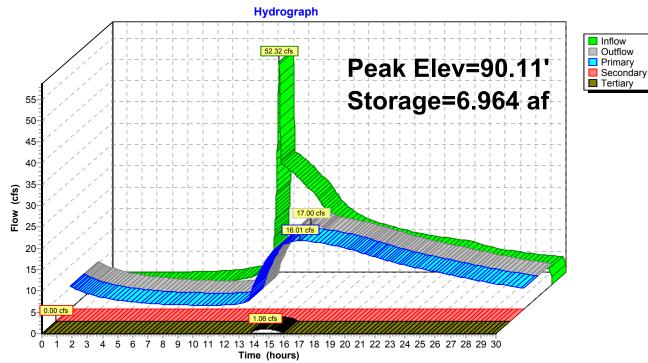
# Summary for Pond AP3: Ash Pond 3

Inflow Outflow Primary Seconda Tertiary	= 17.00 c = 16.01 c ary = 0.00 c	cfs @ 14 cfs @ 14 cfs @ 14	1.97 hrs, Volume=17.796 af4.98 hrs, Volume=17.898 af, Atten= 68%, Lag= 180.7 min5.21 hrs, Volume=17.754 af0.00 hrs, Volume=0.000 af4.71 hrs, Volume=0.145 af						
Starting	Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 4.400 af Peak Elev= 90.11' @ 15.21 hrs Surf.Area= 0.000 ac Storage= 6.964 af (2.564 af above start)								
	Plug-Flow detention time= 341.4 min calculated for 13.498 af (76% of inflow) Center-of-Mass det. time= 37.6 min(1,082.9 - 1,045.3)								
Volume		vail.Stora	age Storage Description						
#1	87.00'	19.800	af Custom Stage DataListed below						
(fee 87.0 89.0 91.0 93.0	Elevation         Cum.Store           (feet)         (acre-feet)           87.00         0.000           89.00         4.400           91.00         9.000           93.00         14.000								
95.0	)0 19.80	0							
Device	Routing		Outlet Devices						
#1	Primary	88.00'	<b>24.0" Round Principal Spillway Culvert</b> L= 100.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 88.00' / 87.00' S= 0.0100 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 3.14 sf						
#2	Secondary	89.00'	<b>30.0"</b> Round Culvert to AP1 L= 280.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $88.00' / 89.00'$ S= -0.0036 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf						
#3	Tertiary	89.00'	<b>16.0</b> " Round Culvert to AP2 X 2.00 L= 540.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $88.00'$ / $89.00'$ S= -0.0019 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.40 sf						
#4	Primary	90.00'	24.0" Round Emergency Spillway Culvert L= 100.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 90.00' / 89.00' S= 0.0100 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 3.14 sf						

Primary OutFlow Max=16.01 cfs @ 15.21 hrs HW=90.11' (Free Discharge) -1=Principal Spillway Culvert (Inlet Controls 15.97 cfs @ 5.08 fps) -4=Emergency Spillway Culvert (Barrel Controls 0.04 cfs @ 0.87 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=89.00' TW=89.00' (Dynamic Tailwater) 2=Culvert to AP1 (Controls 0.00 cfs)

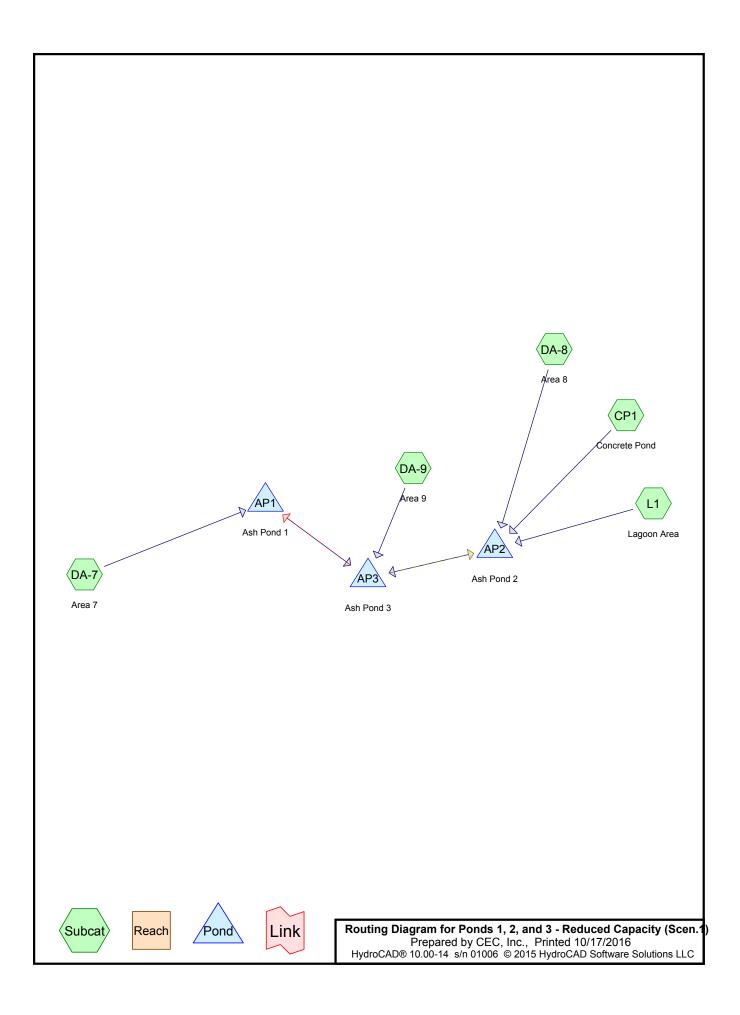
**Tertiary OutFlow** Max=1.05 cfs @ 14.71 hrs HW=90.09' TW=90.00' (Dynamic Tailwater) **3=Culvert to AP2** (Outlet Controls 1.05 cfs @ 0.38 fps)



# Pond AP3: Ash Pond 3

# ADDITIONAL EVALUATION (EXISTING POND FOOTPRINT)

PONDS 1, 2, AND 3 (POND 1, SCENARIO 1)



Ponds 1, 2, and 3 - Reduced Capacity (Scen.1)

# Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.410	79	<50% Grass cover, Poor, HSG B (DA-8)
14.400	82	Dirt roads, HSG B (DA-7, DA-8, DA-9)
4.870	86	Fallow, bare soil, HSG B (DA-7, L1)
4.040	98	Unconnected roofs, HSG B (DA-7, DA-8)
6.920	98	Water Surface, HSG B (CP1, DA-7, DA-8, DA-9, L1)
32.640	88	TOTAL AREA

# Soil Listing (selected nodes)

Area	Soil	Subcatchment		
(acres)	Group	Numbers		
0.000	HSG A			
32.640	HSG B	CP1, DA-7, DA-8, DA-9, L1		
0.000	HSG C			
0.000	HSG D			
0.000	Other			
32.640		TOTAL AREA		

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HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
0.000	2.410	0.000	0.000	0.000	2.410	<50% Grass cover, Poor	DA-8
0.000	14.400	0.000	0.000	0.000	14.400	Dirt roads	DA-7,
							DA-8,
							DA-9
0.000	4.870	0.000	0.000	0.000	4.870	Fallow, bare soil	DA-7, L1
0.000	4.040	0.000	0.000	0.000	4.040	Unconnected roofs	DA-7,
							DA-8
0.000	6.920	0.000	0.000	0.000	6.920	Water Surface	CP1,
							DA-7,
							DA-8,
							DA-9, L1
0.000	32.640	0.000	0.000	0.000	32.640	TOTAL AREA	

# Ground Covers (selected nodes)

Ponds 1, 2, and 3 - Reduced Capacity (Scen.1)

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 Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
 1	CP1	0.00	0.00	550.0	0.0200	0.010	6.0	0.0	0.0
2	L1	0.00	0.00	710.0	0.0200	0.010	8.0	0.0	0.0
3	AP1	89.00	88.00	280.0	0.0036	0.010	30.0	0.0	0.0
4	AP2	89.00	88.00	540.0	0.0019	0.025	16.0	0.0	0.0
5	AP3	88.00	87.00	100.0	0.0100	0.012	24.0	0.0	0.0
6	AP3	88.00	89.00	280.0	-0.0036	0.010	30.0	0.0	0.0
7	AP3	88.00	89.00	540.0	-0.0019	0.025	16.0	0.0	0.0
8	AP3	90.00	89.00	100.0	0.0100	0.025	24.0	0.0	0.0

# Pipe Listing (selected nodes)

Ponds 1, 2, and 3 - Reduced Capacity (Scen.1)Type II 24-hrPrepared by CEC, Inc.HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Sim-Route method - Pond routing by Sim-Route method

SubcatchmentCP1: Concrete Pond Flow Length=550' Slope=0.0200 '/' Tc=1.7 min CN=98 Runoff=0.92 cfs 0.04	
SubcatchmentDA-7: Area 7 Runoff Area=19.590 ac 30.12% Impervious Runoff Depth= Flow Length=1,335' Slope=0.0100 '/' Tc=14.4 min CN=88 Runoff=107.47 cfs 7.03	
SubcatchmentDA-8: Area 8 Runoff Area=6.220 ac 40.68% Impervious Runoff Depth= Flow Length=475' Slope=0.0100 '/' Tc=16.7 min CN=87 Runoff=31.28 cfs 2.1	
SubcatchmentDA-9: Area 9 Runoff Area=5.140 ac 34.82% Impervious Runoff Depth= Flow Length=435' Slope=0.0100 '/' Tc=5.1 min CN=88 Runoff=38.23 cfs 1.84	
SubcatchmentL1: Lagoon Area Runoff Area=1.590 ac 40.25% Impervious Runoff Depth= Flow Length=710' Slope=0.0200 '/' Tc=1.9 min CN=91 Runoff=13.71 cfs 0.6	
Pond AP1: Ash Pond 1         Peak Elev=93.02' Storage=3.921 af Inflow=108.05 cfs 8.4           30.0" Round Culvert n=0.010 L=280.0' S=0.0036 '/' Outflow=31.08 cfs 8.2	
Pond AP2: Ash Pond 2         Peak Elev=91.74' Storage=2.957 af Inflow=33.68 cfs 4.4           16.0" Round Culvert x 2.00 n=0.025 L=540.0' S=0.0019 '/' Outflow=4.05 cfs 4.0	
Pond AP3: Ash Pond 3         Peak Elev=90.85' Storage=4.023 af Inflow=58.96 cfs         14.1           Primary=23.06 cfs         14.575 af         Secondary=0.00 cfs         0.000 af         Tertiary=0.00 cfs         0.000 af         Outflow=23.06 cfs         14.575	

Total Runoff Area = 32.640 ac Runoff Volume = 11.717 af Average Runoff Depth = 4.31" 66.42% Pervious = 21.680 ac 33.58% Impervious = 10.960 ac

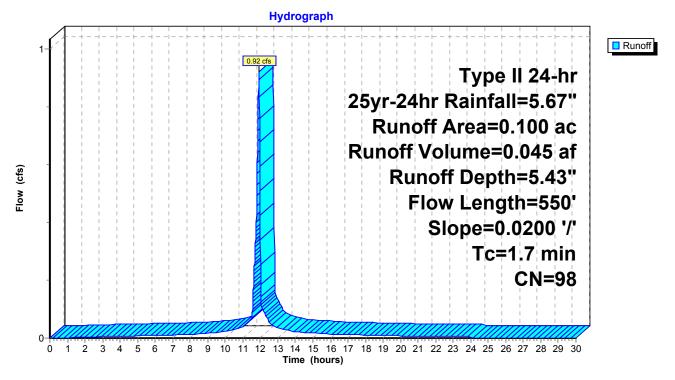
### Summary for Subcatchment CP1: Concrete Pond

Runoff = 0.92 cfs @ 11.92 hrs, Volume= 0.045 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

 Area	(ac) C	N Des	cription		
0.	100 9	98 Wat	er Surface	, HSG B	
0.	100	100	.00% Impe	rvious Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.7	550	0.0200	5.25	1.03	<b>Pipe Channel,</b> 6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13' n= 0.010 PVC, smooth interior

#### Subcatchment CP1: Concrete Pond



#### Summary for Subcatchment DA-7: Area 7

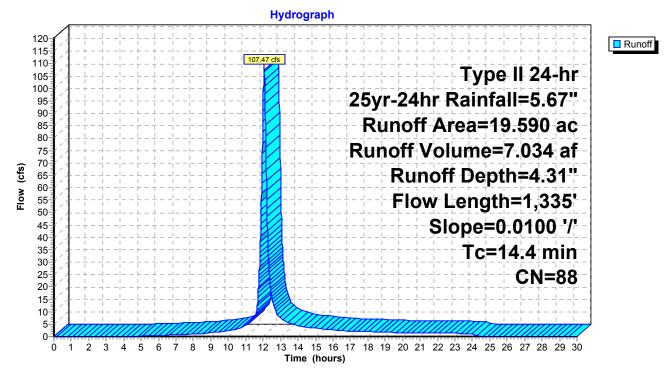
Runoff = 107.47 cfs @ 12.06 hrs, Volume= 7.034 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN De	escription		
	1.	980	98 W	ater Surfac	e, HSG B	
	3.	920	86 Fa	allow, bare	soil, HSG B	
	3.	920	98 Ur	nconnected	roofs, HSG	В
	9.	770	82 Di	rt roads, H	SG B	
	19.	590	88 W	eighted Av	erage	
	13.	690	69	.88% Perv	ous Area	
	5.	900			rvious Area	
	3.	920	66	6.44% Unco	onnected	
	-		01		0 1	
	Tc	Length				Description
_	(min)	(feet)	(ft/f	t) (ft/sec)	) (cfs)	
	1.6	100	0.010	0 1.05	5	Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
	12.8	1,235	0.010	0 1.61		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	444	4 005	Tatal			

14.4 1,335 Total

# Subcatchment DA-7: Area 7



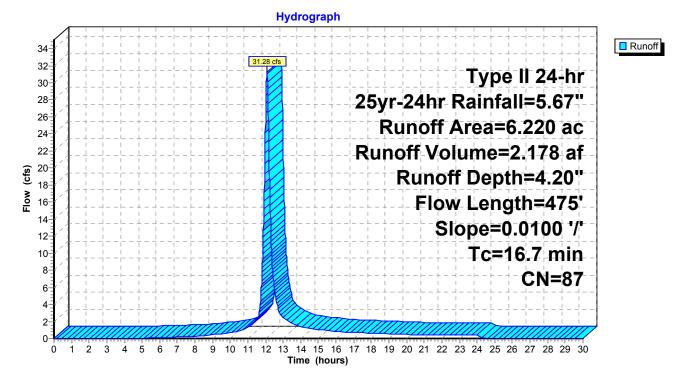
#### Summary for Subcatchment DA-8: Area 8

Runoff = 31.28 cfs @ 12.08 hrs, Volume= 2.178 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN I	Desc	cription		
2.	410	98 \	Wate	er Surface	, HSG B	
2.	410	79 •	<50%	% Grass co	over, Poor,	HSG B
1.	280	82 I	Dirt ı	roads, HS	GΒ	
0.	120	98 I	Unco	onnected r	oofs, HSG	В
6.	220	87 V	Weig	ghted Aver	age	
3.	690	į	59.3	2% Pervio	us Area	
2.	530	4	40.6	8% Imperv	ious Area	
0.	120	4	4.74	% Unconn	ected	
Тс	Length		эре	Velocity	Capacity	Description
(min)	(feet)	) (f	t/ft)	(ft/sec)	(cfs)	
12.8	100	0.01	100	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.26"
3.9	375	0.01	100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
16.7	475	o Tota	al			

Subcatchment DA-8: Area 8



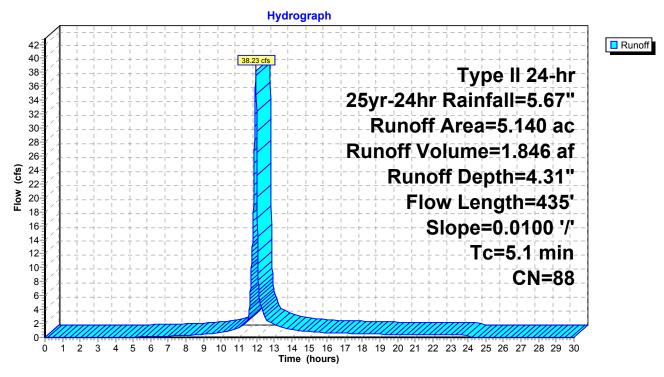
#### Summary for Subcatchment DA-9: Area 9

Runoff = 38.23 cfs @ 11.96 hrs, Volume= 1.846 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Are	a (ac)	С	N Des	cription		
	1.790	9	8 Wat	er Surface	, HSG B	
	3.350	8	2 Dirt	roads, HS	ЭB	
	5.140	8	8 Weig	ghted Aver	age	
	3.350		65.1	8% Pervio	us Area	
	1.790		34.8	2% Imperv	ious Area	
Т	c Len	gth	Slope	Velocity	Capacity	Description
(min	) (fe	et)	(ft/ft)	(ft/sec)	(cfs)	
1.0	61	00	0.0100	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
3.	53	335	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
5.	1 4	135	Total			

#### Subcatchment DA-9: Area 9



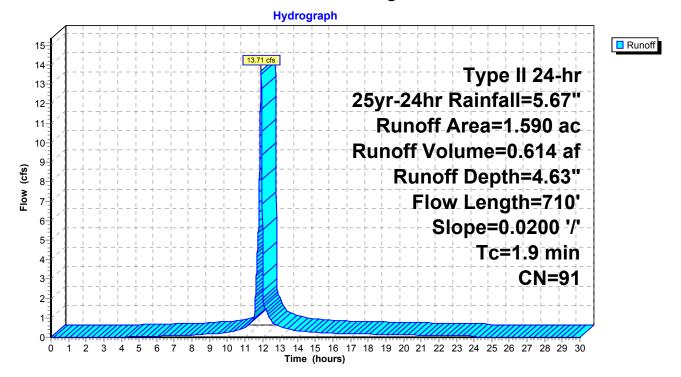
### Summary for Subcatchment L1: Lagoon Area

Runoff = 13.71 cfs @ 11.92 hrs, Volume= 0.614 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN De	scription		
0.	640	98 Wa	ater Surface	, HSG B	
0.	950	86 Fa	low, bare s	oil, HSG B	
1.	590	91 We	eighted Ave	rage	
0.	950	59	75% Pervic	ous Area	
0.	640	40	25% Imper	vious Area	
Tc (min)	Length (feet)		,	Capacity (cfs)	Description
1.9	710	0.020	) 6.36	2.22	<b>Pipe Channel,</b> 8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17' n= 0.010 PVC, smooth interior

#### Subcatchment L1: Lagoon Area



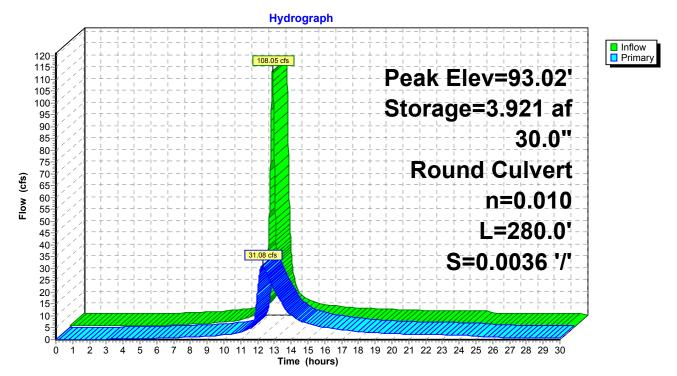
# Summary for Pond AP1: Ash Pond 1

Inflow = Outflow = Primary =	31.08 cfs @ 12	2.06 hrs, Volume=8.472 af, Incl. 0.58 cfs Base Flow2.32 hrs, Volume=8.235 af, Atten= 71%, Lag= 15.7 min2.32 hrs, Volume=8.235 af						
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 1.100 af Peak Elev= 93.02' @ 12.32 hrs Surf.Area= 0.000 ac Storage= 3.921 af (2.821 af above start)								
•	Plug-Flow detention time= 231.8 min calculated for 7.133 af (84% of inflow) Center-of-Mass det. time= 86.1 min ( 901.4 - 815.3 )							
Volume	Invert Avail.Stora	age Storage Description						
#1	87.00' 5.700							
Elevation (feet) 87.00	Cum.Store (acre-feet) 0.000							
89.00 91.00	1.100 2.400							
93.00	3.900							
95.00	5.700							
Device Rout		Outlet Devices						

001100	rtouting	1110010	Odiot Borrisco
#1	Primary	89.00'	30.0" Round Culvert
	·		L= 280.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 89.00' / 88.00' S= 0.0036 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf

**Primary OutFlow** Max=31.08 cfs @ 12.32 hrs HW=93.02' TW=90.23' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 31.08 cfs @ 6.33 fps)

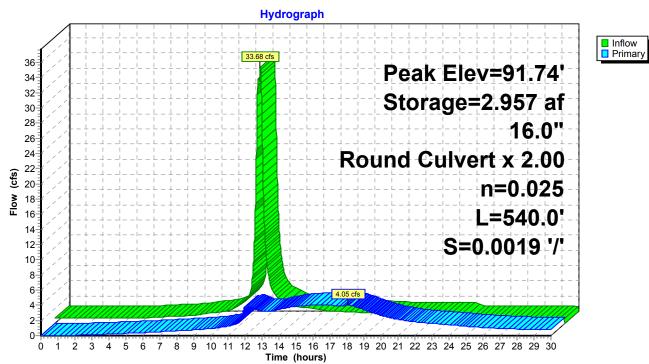
Pond AP1: Ash Pond 1



# Summary for Pond AP2: Ash Pond 2

Outflow = 4.05	3 cfs @ 12.08 hrs, Volume= 5 cfs @ 18.05 hrs, Volume= 5 cfs @ 18.05 hrs, Volume=	4.424 af, Incl. 0.64 cfs Base Flow 4.055 af, Atten= 88%, Lag= 357.9 min 4.055 af						
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 1.100 af Peak Elev= 91.74' @ 13.28 hrs Surf.Area= 0.000 ac Storage= 2.957 af (1.857 af above start)								
	Plug-Flow detention time= 536.9 min calculated for 2.955 af (67% of inflow) Center-of-Mass det. time= 205.0 min(1,038.4 - 833.4)							
Volume Invert	Avail.Storage Storage Description	on						
#1 87.00'	5.600 af Custom Stage Da	ataListed below						
89.001.791.002.493.003.9	ore							
		X 2 00						
#1 Primary	L= 540.0' CMP, proje Inlet / Outlet Invert= 89	ecting, no headwall, Ke= 0.900 9.00' / 88.00' S= 0.0019 '/' Cc= 0.900 metal, Flow Area= 1.40 sf						
		$\mathbf{T}$						

Primary OutFlow Max=4.05 cfs @ 18.05 hrs HW=90.71' TW=89.43' (Dynamic Tailwater) ☐ 1=Culvert (Outlet Controls 4.05 cfs @ 1.47 fps) HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC



## Pond AP2: Ash Pond 2

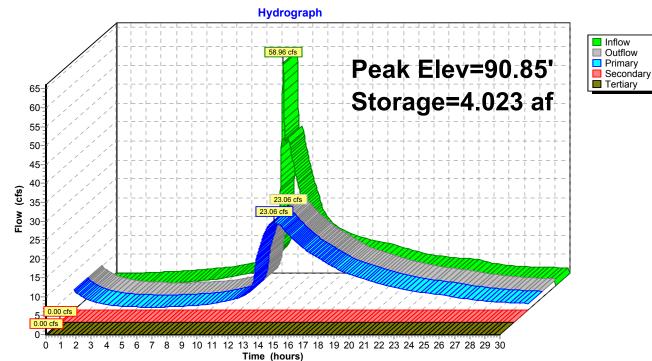
## Summary for Pond AP3: Ash Pond 3

Inflow Outflow Primary Seconda Tertiary	= 23.06 c = 23.06 c ary = 0.00 c	cfs @ 13 cfs @ 13 cfs @ 1	1.97 hrs, Volume=14.135 af3.22 hrs, Volume=14.575 af, Atten= 61%, Lag= 75.3 min3.22 hrs, Volume=14.575 af0.00 hrs, Volume=0.000 af0.00 hrs, Volume=0.000 af								
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 1.900 af Peak Elev= 90.85' @ 13.22 hrs Surf.Area= 0.000 ac Storage= 4.023 af (2.123 af above start)											
Plug-Flow detention time= 185.6 min calculated for 12.671 af (90% of inflow) Center-of-Mass det. time= 33.1 min ( 959.1 - 926.0 )											
Volume		vail.Stora	age Storage Description								
#1	87.00'	9.800	af Custom Stage DataListed below								
Elevatio (fee 87.0 89.0	et) (acre-fee	<u>et)</u> )O									
89.0 91.0											
93.0	00 6.80	00									
95.0	9.80	00									
Device	Routing	Invert	Outlet Devices								
#1	Primary	88.00'	<b>24.0" Round Principal Spillway Culvert</b> L= 100.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 88.00' / 87.00' S= 0.0100 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 3.14 sf								
#2	2 Secondary 8		<b>30.0"</b> Round Culvert to AP1 L= 280.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 88.00' / 89.00' S= -0.0036 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf								
#3	Tertiary 89.00'		<b>16.0"</b> Round Culvert to AP2 X 2.00 L= 540.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $88.00' / 89.00'$ S= -0.0019 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.40 sf								
#4	4 Primary 90.00'		<b>24.0" Round Emergency Spillway Culvert</b> L= 100.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 90.00' / 89.00' S= 0.0100 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 3.14 sf								

**Primary OutFlow** Max=23.06 cfs @ 13.22 hrs HW=90.85' (Free Discharge) -1=Principal Spillway Culvert (Inlet Controls 20.55 cfs @ 6.54 fps) 4=Emergency Spillway Culvert (Barrel Controls 2.51 cfs @ 2.93 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=89.00' TW=89.00' (Dynamic Tailwater) 2=Culvert to AP1 (Controls 0.00 cfs)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=89.00' TW=89.00' (Dynamic Tailwater) -3=Culvert to AP2 (Controls 0.00 cfs)

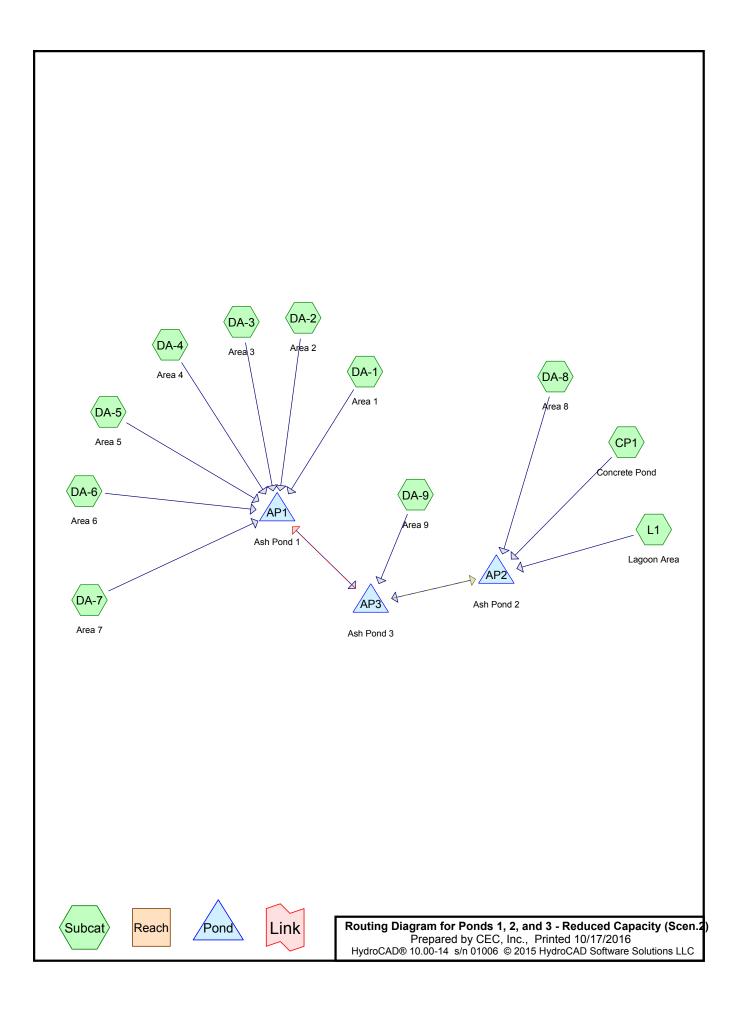


# Pond AP3: Ash Pond 3

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# ADDITIONAL EVALUATION (REQUIRED POND FOOTPRINT)

PONDS 1, 2, AND 3 (POND 1, SCENARIO 2)



Ponds 1, 2, and 3 - Reduced Capacity (Scen.2)

## Area Listing (all nodes)

	Area	CN	Description	
(a	cres)		(subcatchment-numbers)	
	2.410	79	<50% Grass cover, Poor, HSG B (DA-8)	
17	7.990	82	Dirt roads, HSG B (DA-1, DA-2, DA-4, DA-7, DA-8, DA-9)	
20	0.270	86	Fallow, bare soil, HSG B (DA-3, DA-4, DA-5, DA-6, DA-7, L1)	
2	4.410	98	Unconnected roofs, HSG B (DA-4, DA-7, DA-8)	
ę	9.560	98	Water Surface, HSG B (CP1, DA-1, DA-2, DA-5, DA-6, DA-7, DA-8, DA-9, L1)	
54	4.640	87	TOTAL AREA	

Ponds 1, 2, and 3 - Reduced Capacity (Scen.2)

## Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
54.640	HSG B	CP1, DA-1, DA-2, DA-3, DA-4, DA-5, DA-6, DA-7, DA-8, DA-9, L1
0.000	HSG C	
0.000	HSG D	
0.000	Other	
54.640		TOTAL AREA

	SG-A cres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0	0.000	2.410	0.000	0.000	0.000	2.410	<50% Grass cover, Poor	DA-8
0	0.000	17.990	0.000	0.000	0.000	17.990	Dirt roads	DA-1,
								DA-2,
								DA-4,
								DA-7,
								DA-8,
								DA-9
0	0.000	20.270	0.000	0.000	0.000	20.270	Fallow, bare soil	DA-3,
								DA-4,
								DA-5,
								DA-6,
								DA-7, L1
0	0.000	4.410	0.000	0.000	0.000	4.410	Unconnected roofs	DA-4,
								DA-7,
								DA-8
0	0.000	9.560	0.000	0.000	0.000	9.560	Water Surface	CP1,
								DA-1,
								DA-2,
								DA-5,
								DA-6,
								DA-7,
								DA-8,
								DA-9, L1
0	0.000	54.640	0.000	0.000	0.000	54.640	TOTAL AREA	

# Ground Covers (all nodes)

Ponds 1, 2, and 3 - Reduced Capacity (Scen.2)

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Line#	<sup>e</sup> Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	CP1	0.00	0.00	550.0	0.0200	0.010	6.0	0.0	0.0
2	2 L1	0.00	0.00	710.0	0.0200	0.010	8.0	0.0	0.0
3	AP1	89.00	88.00	280.0	0.0036	0.010	30.0	0.0	0.0
2	AP2	89.00	88.00	540.0	0.0019	0.025	16.0	0.0	0.0
5	AP3	88.00	87.00	100.0	0.0100	0.012	24.0	0.0	0.0
6	AP3	88.00	89.00	280.0	-0.0036	0.010	30.0	0.0	0.0
7	AP3	88.00	89.00	540.0	-0.0019	0.025	16.0	0.0	0.0
8	AP3	90.00	89.00	100.0	0.0100	0.025	24.0	0.0	0.0

# Pipe Listing (all nodes)

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Sim-Route method - Pond routing by Sim-Route method

SubcatchmentCP1: Concrete Pond Flow Length=550' Slope=0.0200 '/' Tc=1.7 min CN=98 Runoff=0.92 cfs 0.045 af
SubcatchmentDA-1: Area 1Runoff Area=1.930 ac34.20% ImperviousRunoff Depth=4.20"Flow Length=210'Slope=0.0100 '/'Tc=2.7 minCN=87Runoff=15.27 cfs0.676 af
SubcatchmentDA-2: Area 2Runoff Area=1.170 ac28.21% ImperviousRunoff Depth=4.20"Flow Length=65'Slope=0.3300 '/'Tc=0.3 minCN=87Runoff=9.87 cfs0.410 af
SubcatchmentDA-3: Area 3 Runoff Area=2.550 ac 0.00% Impervious Runoff Depth=4.10" Flow Length=210' Slope=0.0100 '/' Tc=2.7 min CN=86 Runoff=19.82 cfs 0.871 af
SubcatchmentDA-4: Area 4 Runoff Area=9.250 ac 4.00% Impervious Runoff Depth=4.10" Flow Length=590' Slope=0.0100 '/' Tc=6.7 min CN=86 Runoff=62.90 cfs 3.158 af
SubcatchmentDA-5: Area 5Runoff Area=4.710 ac 28.24% Impervious Runoff Depth=4.42"Flow Length=400' Tc=3.7 min CN=89 Runoff=37.28 cfs 1.733 af
SubcatchmentDA-6: Area 6Runoff Area=2.390 ac13.39% ImperviousRunoff Depth=4.31"Flow Length=510'Tc=5.3 minCN=88Runoff=17.66 cfs0.858 af
SubcatchmentDA-7: Area 7Runoff Area=19.590 ac 30.12% Impervious Runoff Depth=4.31"Flow Length=1,335'Slope=0.0100 '/' Tc=14.4 min CN=88Runoff=107.47 cfs 7.034 af
SubcatchmentDA-8: Area 8 Flow Length=475' Slope=0.0100 '/' Tc=16.7 min CN=87 Runoff=31.28 cfs 2.178 af
SubcatchmentDA-9: Area 9Runoff Area=5.140 ac 34.82% Impervious Runoff Depth=4.31"Flow Length=435'Slope=0.0100 '/' Tc=5.1 min CN=88 Runoff=38.23 cfs 1.846 af
SubcatchmentL1: Lagoon AreaRunoff Area=1.590 ac40.25% ImperviousRunoff Depth=4.63"Flow Length=710'Slope=0.0200 '/'Tc=1.9 minCN=91Runoff=13.71 cfs0.614 af
Pond AP1: Ash Pond 1         Peak Elev=93.85' Storage=9.435 af Inflow=230.02 cfs 15.979 af 30.0" Round Culvert n=0.010 L=280.0' S=0.0036 '/' Outflow=34.21 cfs 15.390 af
Pond AP2: Ash Pond 2         Peak Elev=91.84' Storage=3.032 af Inflow=33.68 cfs 4.424 af 16.0" Round Culvert x 2.00 n=0.025 L=540.0' S=0.0019 '/' Outflow=3.61 cfs 4.030 af
Pond AP3: Ash Pond 3         Peak Elev=91.31' Storage=4.601 af Inflow=67.47 cfs 21.264 af           Primary=28.51 cfs 21.610 af Secondary=0.00 cfs 0.000 af Tertiary=0.00 cfs 0.000 af Outflow=28.51 cfs 21.610 af
Total Bunoff Area = 54 640 as Bunoff Valuma = 10 422 af Avarage Bunoff Donth = 4.2

Total Runoff Area = 54.640 ac Runoff Volume = 19.422 af Average Runoff Depth = 4.27" 74.43% Pervious = 40.670 ac 25.57% Impervious = 13.970 ac

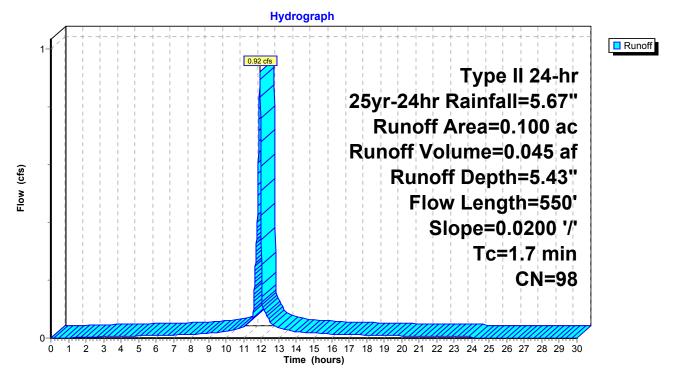
#### Summary for Subcatchment CP1: Concrete Pond

Runoff = 0.92 cfs @ 11.92 hrs, Volume= 0.045 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN De	escription		
_	0.100 98 Water Surface, H				e, HSG B	
0.100			10	0.00% Impe	ervious Area	
	Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description
_	1.7	550	0.020	0 5.25	1.03	<b>Pipe Channel,</b> 6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13' n= 0.010 PVC, smooth interior

#### Subcatchment CP1: Concrete Pond



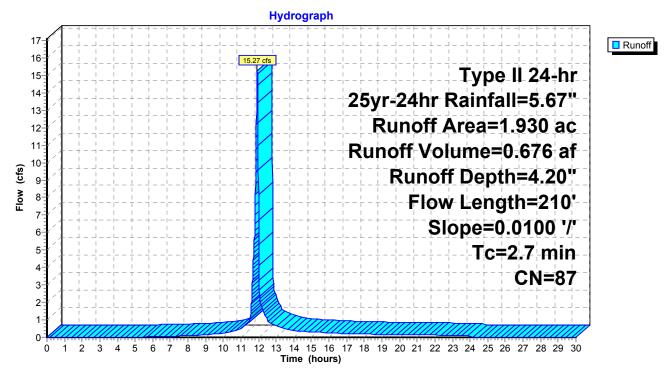
#### Summary for Subcatchment DA-1: Area 1

Runoff = 15.27 cfs @ 11.93 hrs, Volume= 0.676 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

	Area	(ac) C	N Des	cription		
	1.	270 8	32 Dirt	roads, HS	GВ	
	0.	660 9	98 Wat	er Surface	, HSG B	
	1.	930 8	37 Weig	ghted Aver	age	
	1.	270	65.8	0% Pervio	us Area	
	0.	660	34.2	0% Imperv	vious Area	
	Тс	Length	Slope	Velocity	Capacity	Description
(	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.6	100	0.0100	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
	1.1	110	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	2.7	210	Total			

#### Subcatchment DA-1: Area 1



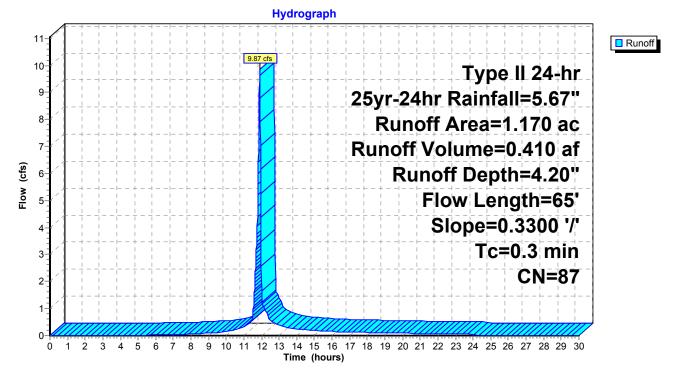
## Summary for Subcatchment DA-2: Area 2

Runoff = 9.87 cfs @ 11.90 hrs, Volume= 0.410 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac)	CN	Desc	cription					
0	.840	82	Dirt r	oads, HS	GВ				
0	.330	98	Wate	er Surface	, HSG B				
1.170 87 Weighted Average									
0.840 71.79% Pervious Area									
0	.330		28.2	1% Imperv	ious Area/				
Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
0.3	6	50	.3300	3.91		Sheet Flow, Smooth surfaces	n= 0.011	P2= 3.26"	





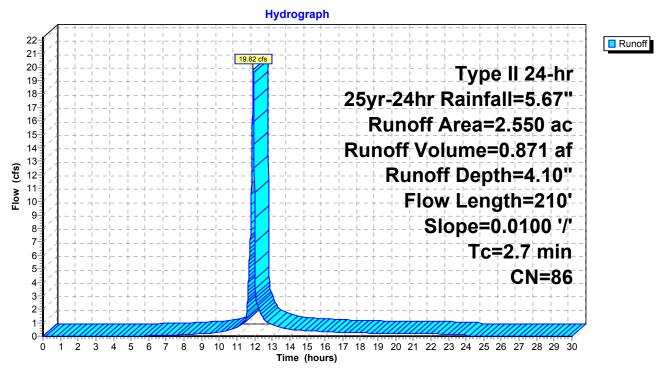
#### Summary for Subcatchment DA-3: Area 3

Runoff = 19.82 cfs @ 11.93 hrs, Volume= 0.871 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) C	N Des	cription						
	2.550 86 Fallow, bare soil, HSG B									
2.550 100.00% Pervious Area										
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
-	1.6	100	0.0100	1.05	· · ·	Sheet Flow,				
	1.1	110	0.0100	1.61		Smooth surfaces n= 0.011 P2= 3.26" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
	2.7	210	Total							

### Subcatchment DA-3: Area 3



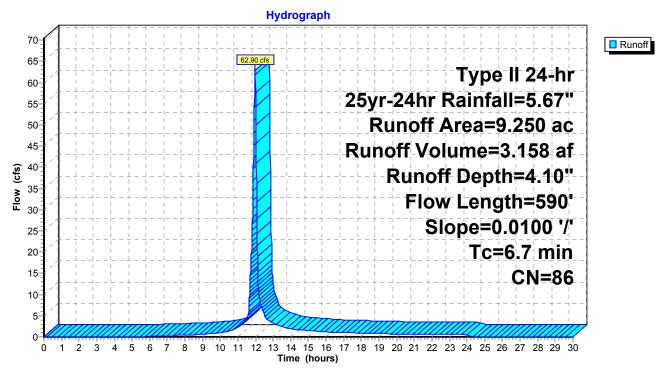
#### Summary for Subcatchment DA-4: Area 4

Runoff = 62.90 cfs @ 11.98 hrs, Volume= 3.158 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN D	escript	ion							
	1.	480	82 D	irt roads, HSG B								
	7.	400	86 F	allow, bare soil, HSG B								
	0.	370	98 U	8 Unconnected roofs, HSG B								
	9.250 86 Weighted Average											
	8.	880	9	6.00%	Pervio	us Area						
	0.	370	4.	.00% Ir	npervi	ous Area						
	0.	370	1	00.00%	6 Unco	nnected						
	Tc (min)	Length (feet)	•		locity t/sec)	Capacity (cfs)	Description					
_	1.6	100	0.010	00	1.05		Sheet Flow,					
	5.1	490	0.010	00	1.61		Smooth surfaces n= 0.011 P2= 3.26" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					
	6.7	590	Total									

#### Subcatchment DA-4: Area 4



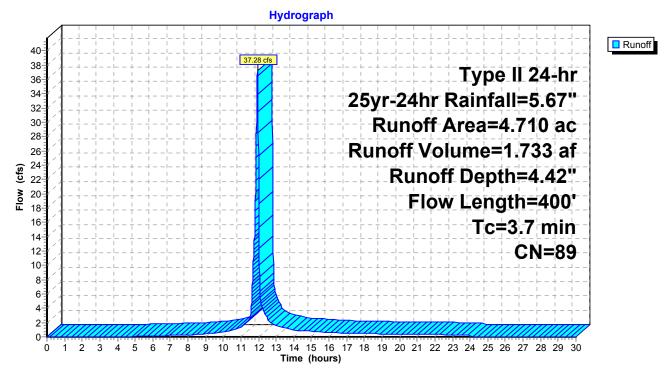
#### Summary for Subcatchment DA-5: Area 5

Runoff = 37.28 cfs @ 11.94 hrs, Volume= 1.733 af, Depth= 4.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

A	rea	(ac) C	N Desc	cription		
	3.	380 8	86 Fallo	w, bare so	oil, HSG B	
	1.	330 9	98 Wate	er Surface	, HSG B	
	4.	710 8	9 Weig	ghted Aver	age	
	3.	380	71.7	6% Pervio	us Area	
	1.	330	28.2	4% Imper	vious Area	
	_					
	Тс	Length	Slope	Velocity	Capacity	Description
(m	in)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.3	100	0.3300	1.27		Sheet Flow,
						Fallow n= 0.050 P2= 3.26"
(	0.1	80	0.3300	9.25		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
2	2.3 220 0.		0.0100 1.61			Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	3.7	400	Total			

#### Subcatchment DA-5: Area 5



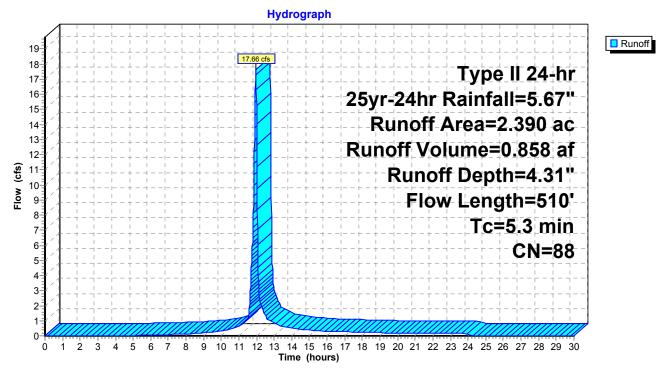
#### Summary for Subcatchment DA-6: Area 6

Runoff = 17.66 cfs @ 11.96 hrs, Volume= 0.858 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

 Area	(ac) C	N Dese	cription		
2.	070 8	86 Fallo	ow, bare so	oil, HSG B	
 0.	320 9	98 Wate	er Surface	, HSG B	
2.	390 E	88 Weig	ghted Aver	age	
2.	070	86.6	1% Pervio	us Area	
0.	320	13.3	9% Imperv	vious Area	
Тс	Length	Slope	Velocity	Capacity	Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.3	100	0.3300	1.27		Sheet Flow,
					Fallow n= 0.050 P2= 3.26"
0.1	30	0.3300	9.25		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
3.9 380 0.		0.0100 1.61			Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
5.3	510	Total			

### Subcatchment DA-6: Area 6



### Summary for Subcatchment DA-7: Area 7

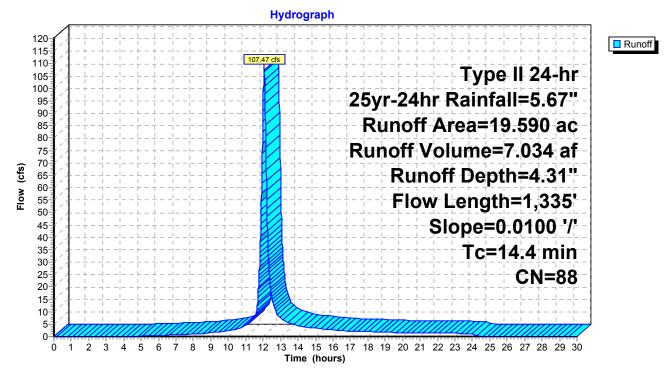
Runoff = 107.47 cfs @ 12.06 hrs, Volume= 7.034 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

_	Area	(ac) (	CN De	escription		
	1.	980	98 W	ater Surfac	e, HSG B	
	3.	920	86 Fa	allow, bare	soil, HSG B	
	3.	920	98 Ur	nconnected	roofs, HSG	В
	9.	770	82 Di	rt roads, H	SG B	
	19.	590	88 W	eighted Av	erage	
	13.	690	69	.88% Perv	ous Area	
	5.	900			rvious Area	
	3.	920	66	6.44% Unco	onnected	
	-		01		0 1	
	Tc	Length				Description
_	(min)	(feet)	(ft/f	t) (ft/sec)	) (cfs)	
	1.6	100	0.010	0 1.05	5	Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.26"
	12.8	1,235	0.010	0 1.61		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	444	4 005	Tatal			

14.4 1,335 Total

## Subcatchment DA-7: Area 7



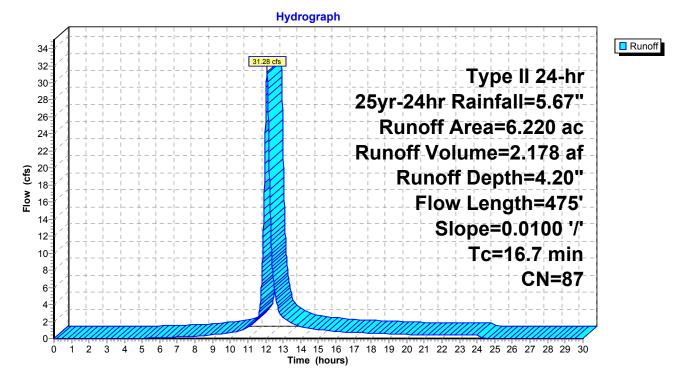
#### Summary for Subcatchment DA-8: Area 8

Runoff = 31.28 cfs @ 12.08 hrs, Volume= 2.178 af, Depth= 4.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	CN I	Desc	cription							
2.	410	98 \	Wate	er Surface	, HSG B						
2.410 79 <50% Grass cover, Poor, HSG B											
1.	1.280 82 Dirt roads, HSG B										
0.	120	98 I	Unco	onnected r	oofs, HSG	В					
6.	220	87 V	Weig	ghted Aver	age						
3.	690	į	59.3	2% Pervio	us Area						
2.	530	4	40.6	8% Imperv	ious Area						
0.	120	4	4.74	% Unconn	ected						
Тс	Length		эре	Velocity	Capacity	Description					
(min)	(feet)	) (f	t/ft)	(ft/sec)	(cfs)						
12.8	100	0.01	100	0.13		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.26"					
3.9	375	0.01	100	1.61		Shallow Concentrated Flow,					
						Unpaved Kv= 16.1 fps					
16.7	475	o Tota	al								

Subcatchment DA-8: Area 8



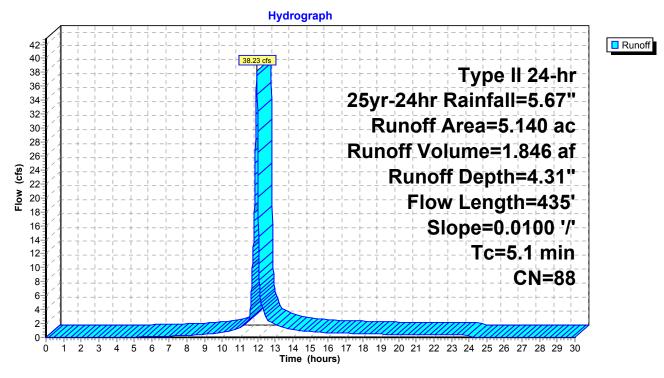
#### Summary for Subcatchment DA-9: Area 9

Runoff = 38.23 cfs @ 11.96 hrs, Volume= 1.846 af, Depth= 4.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Are	a (ac)	С	N Des	cription		
	1.790	9	8 Wat	er Surface	, HSG B	
	3.350	8	2 Dirt	roads, HS	ЭB	
	5.140	8	8 Weig	ghted Aver	age	
	3.350		65.1	8% Pervio	us Area	
	1.790		34.8	2% Imperv	ious Area	
Т	c Len	gth	Slope	Velocity	Capacity	Description
(min	) (fe	et)	(ft/ft)	(ft/sec)	(cfs)	
1.0	61	00	0.0100	1.05		Sheet Flow,
	3.5 335 0.0100 1.61					Smooth surfaces n= 0.011 P2= 3.26"
3.						Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
5.	1 4	135	Total			

#### Subcatchment DA-9: Area 9



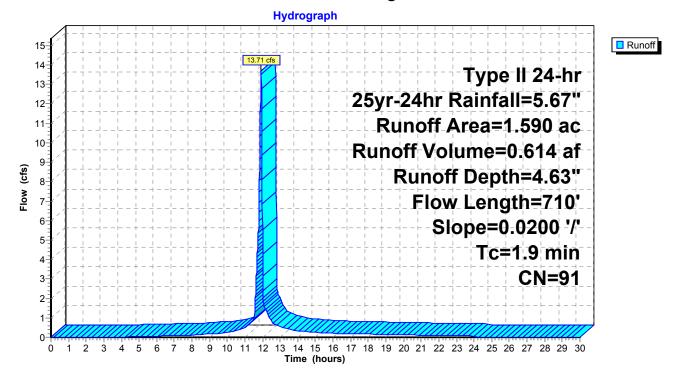
### Summary for Subcatchment L1: Lagoon Area

Runoff = 13.71 cfs @ 11.92 hrs, Volume= 0.614 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type II 24-hr 25yr-24hr Rainfall=5.67"

Area	(ac) (	N Des	scription		
0.	640	98 Wa	ter Surface	, HSG B	
0.	950	86 Fal	ow, bare se	oil, HSG B	
1.	590	91 We	ighted Ave	rage	
0.	950	59.	75% Pervic	ous Area	
0.	640	40.	25% Imper	vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
1.9	710	0.0200	6.36	2.22	<b>Pipe Channel,</b> 8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17' n= 0.010 PVC, smooth interior

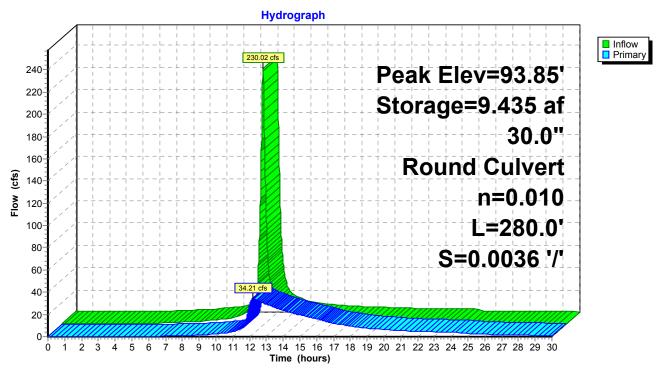
#### Subcatchment L1: Lagoon Area



## Summary for Pond AP1: Ash Pond 1

Inflow Outflow Primary	= = =	34.21 c	fs @ 1	,	af, Incl. 0.50 cfs Base Flow af, Atten= 85%, Lag= 15.6 min af						
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 2.200 af Peak Elev= 93.85' @ 12.44 hrs Surf.Area= 0.000 ac Storage= 9.435 af (7.235 af above start)											
	Plug-Flow detention time= 288.7 min calculated for 13.186 af (83% of inflow) Center-of-Mass det. time= 152.8 min ( 955.9 - 803.1 )										
Volume	I	nvert Av	ail.Stor	ge Storage Description							
#1	8	57.00'	11.50	af Custom Stage DataListed	below						
Elevatior (feet	)	Cum.Stor (acre-fee	<u>)</u>								
87.00	-	0.00	-								
89.00	-	2.20	-								
91.00	-	4.80	•								
93.00		7.90									
95.00	J	11.50	0								
Device	Routi	ng	Invert	Outlet Devices							
#1	Prima	iry	89.00'	<b>30.0" Round Culvert</b> L= 280.0' CPP, projecting, no I Inlet / Outlet Invert= 89.00' / 88. n= 0.010 PVC, smooth interior,	00' S= 0.0036 '/' Cc= 0.900						

Primary OutFlow Max=34.12 cfs @ 12.22 hrs HW=93.71' TW=90.37' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 34.12 cfs @ 6.95 fps) HydroCAD® 10.00-14 s/n 01006 © 2015 HydroCAD Software Solutions LLC



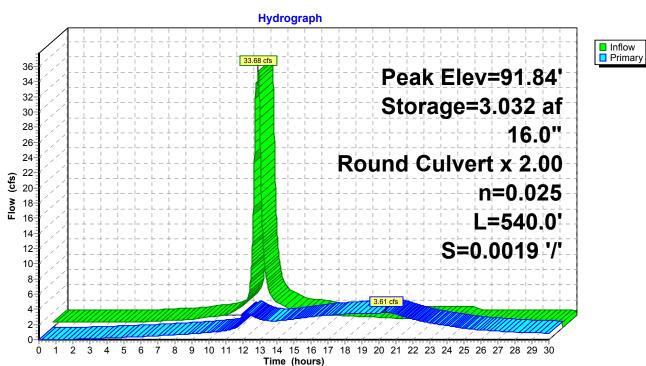
## Pond AP1: Ash Pond 1

## Summary for Pond AP2: Ash Pond 2

	= 3.61 d	:fs @ 2	2.08 hrs, Volume= 0.39 hrs, Volume= 0.39 hrs, Volume=	4.424 af, Incl. 0.64 cfs Base Flow 4.030 af, Atten= 89%, Lag= 498.3 min 4.030 af							
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 1.100 af Peak Elev= 91.84' @ 13.93 hrs Surf.Area= 0.000 ac Storage= 3.032 af (1.932 af above start)											
	Plug-Flow detention time= 599.8 min calculated for 2.929 af (66% of inflow) Center-of-Mass det. time= 250.5 min(1,083.9 - 833.4)										
Volume	Volume Invert Avail.Storage Storage Description										
#1	87.00'	5.60	0 af Custom Stage Da	taListed below							
#1       87.00'       5.600 af       Custom Stage DataListed below         Elevation       Cum.Store (feet)       (acre-feet)         87.00       0.000         89.00       1.100         91.00       2.400         93.00       3.900         95.00       5.600											
#1 Pri	mary	89.00'	L= 540.0' CMP, projec Inlet / Outlet Invert= 89	cting, no headwall, Ke= 0.900 .00' / 88.00' S= 0.0019 '/' Cc= 0.900							
			n= 0.025 Corrugated n	netal, Flow Area= 1.40 sf							

Primary OutFlow Max=3.62 cfs @ 20.39 hrs HW=90.71' TW=89.69' (Dynamic Tailwater) ☐ 1=Culvert (Outlet Controls 3.62 cfs @ 1.31 fps)

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## Pond AP2: Ash Pond 2

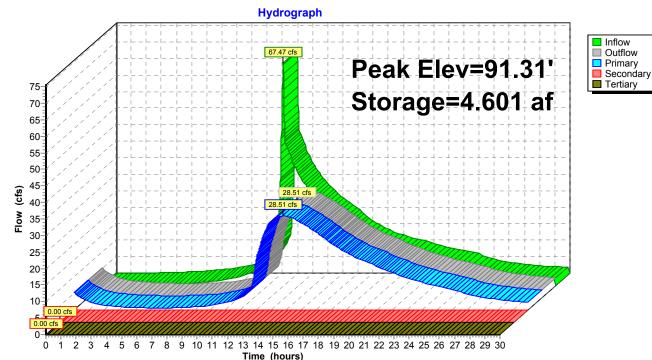
## Summary for Pond AP3: Ash Pond 3

Inflow Outflow Primary Seconda Tertiary	= 28.51 ( = 28.51 ( ary = 0.00 (	cfs @ 13 cfs @ 13 cfs @ 1	1.97 hrs, Volume=21.264 af3.79 hrs, Volume=21.610 af, Atten= 58%, Lag= 109.3 min3.79 hrs, Volume=21.610 af0.00 hrs, Volume=0.000 af0.00 hrs, Volume=0.000 af								
Routing by Sim-Route method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Starting Elev= 89.00' Surf.Area= 0.000 ac Storage= 1.900 af Peak Elev= 91.31' @ 13.79 hrs Surf.Area= 0.000 ac Storage= 4.601 af (2.701 af above start)											
Plug-Flow detention time= 150.8 min calculated for 19.710 af (93% of inflow) Center-of-Mass det. time= 45.3 min(1,010.9 - 965.6)											
Volume		vail.Stora	age Storage Description								
#1	87.00'	9.800	af Custom Stage DataListed below								
(fee 87.0	Elevation         Cum.Store           (feet)         (acre-feet)           87.00         0.000           89.00         1.900           91.00         4.200										
93.0	00 6.80	00									
95.0	9.80	00									
Device	Routing		Outlet Devices								
#1	Primary	88.00'	<b>24.0" Round Principal Spillway Culvert</b> L= 100.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 88.00' / 87.00' S= 0.0100 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 3.14 sf								
#2	Secondary	89.00'	<b>30.0"</b> Round Culvert to AP1 L= 280.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $88.00' / 89.00'$ S= -0.0036 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf								
#3	Tertiary 89.00		<b>16.0"</b> Round Culvert to AP2 X 2.00 L= 540.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $88.00' / 89.00'$ S= -0.0019 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.40 sf								
#4	Primary	90.00'	<b>24.0" Round Emergency Spillway Culvert</b> L= 100.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 90.00' / 89.00' S= 0.0100 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 3.14 sf								

Primary OutFlow Max=28.51 cfs @ 13.79 hrs HW=91.31' (Free Discharge) -1=Principal Spillway Culvert (Inlet Controls 22.98 cfs @ 7.32 fps) -4=Emergency Spillway Culvert (Barrel Controls 5.53 cfs @ 3.60 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=89.00' TW=89.00' (Dynamic Tailwater) 2=Culvert to AP1 (Controls 0.00 cfs)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=89.00' TW=89.00' (Dynamic Tailwater) -3=Culvert to AP2 (Controls 0.00 cfs)



# Pond AP3: Ash Pond 3

# ATTACHMENT 7

# STORAGE CAPACITY ABOVE POOL FOR VARYING POOL AREAS AND DEPTHS

## Owensboro Municipal Utilities Elmer Smith Station Ash Pond Hydrologic and Hydraulic Capacity Requirments (CCR Rule §257.82) Storage Capacity above Pool (Ac-Ft) for Varying Pool Areas (Ac) and Depths (feet)

	Pool Area	(Acres)																			
Depth to Pool (feet)	0.25	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	6.5	7	7.5	8	8.5	9	9.5	10
1	0.25	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	6.5	7	7.5	8	8.5	9	9.5	10
2	0.5	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
3	0.75	1.5	3	4.5	6	7.5	9	10.5	12	13.5	15	16.5	18	19.5	21	22.5	24	25.5	27	28.5	30
4	1	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
5	1.25	2.5	5	7.5	10	12.5	15	17.5	20	22.5	25	27.5	30	32.5	35	37.5	40	42.5	45	47.5	50
6	1.5	3	6	9	12	15	18	21	24	27	30	33	36	39	42	45	48	51	54	57	60

1. This tables shows the approximate storage capacity (ac-feet) for varying pool areas (ac) and depth to the pools (feet). This table can be used to estimate whether the required capacity is available in the pools based on the pool area and the depth to the pool (or freeboard).